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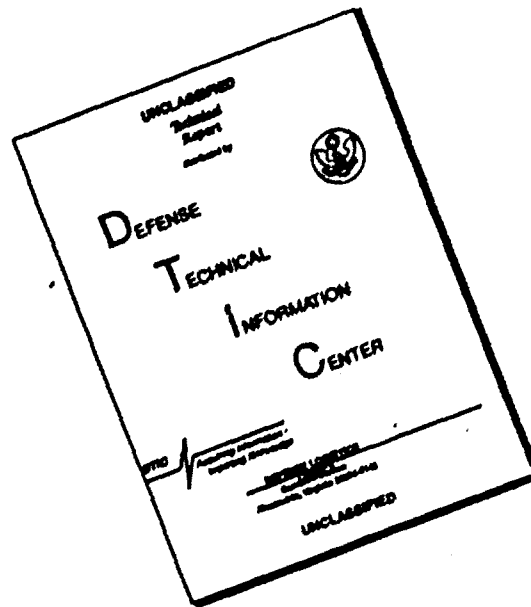
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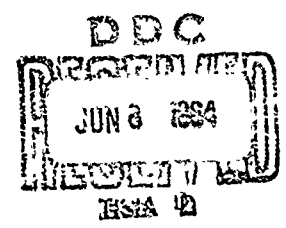
**CONFAC II  
A GENERAL COMPUTER PROGRAM FOR THE  
DETERMINATION OF RADIANT-INTERCHANGE  
CONFIGURATION AND FORM FACTORS**

TECHNICAL DOCUMENTARY REPORT No. FDL-TDR-64-43

APRIL 1964

AIR FORCE FLIGHT DYNAMICS LABORATORY  
RESEARCH AND TECHNOLOGY DIVISION  
AIR FORCE SYSTEMS COMMAND  
WRIGHT-PATTERSON AIR FORCE BASE, OHIO

Project No. 6146, Task No. 614618



(Prepared under Contract No. AF 33(657)-8953 by the  
Space and Information Systems Division of  
North American Aviation, Inc., Downey, California;  
Kempton A. Toups, author)

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300 - May 1964 - 162-39-786

#### FOREWORD

This computer program is one of a series of digital computer programs developed as in-house effort in support of the Space Vehicle Thermal and Atmospheric Control Study. The study is sponsored by the Flight Dynamics Laboratory of the Research and Technology Division under Contract AF33(657)-S255 and is under the direction of W. Uhl of the Environmental Control Branch. R. E. Sexton of S&ID served as Project Manager of the study program. H. L. Nordwall reviewed and edited the contractor's report for publication as an FDL TDR.

The program described in this report represents the second stage in the development of a general configuration factor computer program. This report partly incorporates SID 62-393 (ASD TN 61-101), which describes CONFAC I, the first program developed under the Space Vehicle Thermal and Atmospheric Control Study.

This report may also be identified by Contractor's Report No. SID 63-1397.

# ABSTRACT

A simple numerical method is derived for the determination of the geometric radiant-interchange factors used in radiant heat transfer and illumination. A FORTRAN II digital computer program utilizing this method is developed which provides a rapid and accurate means of computation of configuration and form factors. The source of flux may be any general plane polygon and the receiver may be any general plane or nonplanar polygon, the surface of an arbitrary polyhedron, or an arbitrary combination of such surfaces.

It is therefore possible to accurately determine configuration and form factors from a plane surface to another surface occluded by complex intervening surfaces. Form factors are computed rapidly -- averaging less than two seconds on the IBM 7094 for simple, unobstructed plane surfaces, and less than 30 seconds for simple polyhedra. Also, means are provided to internally generate a variety of regular polygons or polyhedra and to transform surface spatial coordinates for convenience of data entry and/or motion simulation. Simplicity of data entry, flexibility of application, and economy of operation are principal features of this program. Sample problems illustrating these important aspects are provided.

This report has been reviewed and is approved.



R. J. BAKER  
Asst. for R&T  
Vehicle Equipment Division  
AF Flight Dynamics Laboratory



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## NOMENCLATURE

$A$	Area
$e$	Exchange coefficient
$c$	Configuration factor (italicized)
$f$	Form factor (italicized)
$h, k, l$	Translation components
$i, j, k$	Unit vectors along the X-, Y-, Z-axis, respectively
$O$	Center of unit sphere, origin of coordinate system
$R$	Radius of sphere
$S$	Distance between two areas
$X, Y, Z$ or $x, y, z$	Spatial coordinates of a point relative to X, Y, Z axis
$\alpha, \beta, \gamma$	Direction angles of a line relative to X, Y, Z axis respectively
$\gamma$	Angle between Z axis and vector normal to plane
$\theta$	Angle between two vectors
$\pi$	Numerical constant = 3.14159 +
$\omega$	Solid angle

### Subscripts

$A, B, C$	Points on an area
$s$	Sector
$\Delta A$	Finite incremental area
$dA$	Differential area
$dA-A$	From a differential area to an area

NOMENCLATURE (cont'd)

Subscripts (cont'd)

- 1,2,     Areas 1,2,
- 12       Area 1 to area 2
- $\epsilon$        Elliptical

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## SECTION I

### INTRODUCTION

The geometric form factor,  $f_{12}$ , is defined as the fraction of radiant energy emanating from finite surface  $A_1$  which is intercepted by another surface  $A_2$ .

$$f_{12} = \frac{\text{Flux received by finite surface } A_2}{\text{Flux emitted by finite surface } A_1} \quad (1)$$

The geometric configuration factor,  $\epsilon_{12}$ , is defined in a similar manner, except that the emitting surface is infinitesimal, (sometimes referred to as the point configuration factor),

$$\epsilon_{12} = \frac{\text{Flux received by finite surface } A_2}{\text{Flux emitted by infinitesimal surface } dA_1} \quad (2)$$

The subscripts denote the direction of flow of net flux;  $\epsilon_{12}$  and  $f_{12}$  pertain respectively to the configuration and form factor from surface  $A_1$  to surface  $A_2$ . It is assumed that each surface is isothermal and radiates diffusely, i.e., follows Lambert's cosine distribution law.

The "closed-form" determination of the configuration or form factor by classical integration techniques is impossible or impractical in most situations. Experimental techniques and devices have been reported in the literature (Reference 1), and probably the most useful is Pleijel's Globoscope (Reference 4). Experimental techniques produce only the configuration factor, however. Nonetheless, they are useful for many applications where only one or just a few configuration factors are required and nominal accuracy is sufficient.

However, if a large number of form factors are required in a short period of time, experimental techniques are not practical. This report presents a numerical method and a computer program which enables rapid and accurate computation of configuration and form factors between plane surfaces, and plane or solid surfaces. The source (surface 1) may be any general plane polygon; the receiver (surface 2) may be any arbitrarily oriented general plane or nonplanar polygon, the surface of an arbitrary solid, or an arbitrary combination of planes, nonplanes, or solids. Form factors (which nominally are derived from 625 configuration factors) are computed rapidly, averaging less than 2 seconds by IBM 7094 time for simple plane surfaces, and less than 30 seconds from simple plane surfaces to simple solids. Table 1 compares solutions obtained by CONFAC II to those given in Reference 1.

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Table 1, Comparison of Configuration and Form Factors Computed by CONFACII to Those Given in Reference 1

Configuration	Reference 1	Computer (Trapezoidal Rule)	
		24 x 24 grid	60 x 60 grid
P-1, X = 1, Y = 1	0.13853	0.138532	0.138532
X = 0.1, Y = 0.1	0.00314	0.003141	0.003141
X = 1, Y = 4	0.17527	0.175270	0.175270
X = 0.1, Y = 0.4	0.01147	0.011471	0.011471
X = 1, Y = $\infty$ *	0.17678	0.176777	0.176777
X = 0.1, Y = $\infty$ *	0.02488	0.024876	0.024876
P-2, $\theta = 30^\circ$ , L = 0, N = 1	0.4665	0.466506	0.466506
$\theta = 30^\circ$ , L = 1, N = 1	0.1759	0.175923	0.175923
$\theta = 30^\circ$ , L = 0, N = 4	0.4665	0.466506	0.466506
$\theta = 30^\circ$ , L = 4, N = 4	0.0964	0.096447	0.096447
$\theta = 120^\circ$ , L = 0, N = 1	0.125	0.125000	0.125000
$\theta = 120^\circ$ , L = 1, N = 1	0.0236	0.023554	0.023554
$\theta = 120^\circ$ , L = 0, N = 4	0.125	0.125000	0.125000
$\theta = 120^\circ$ , L = 4, N = 4	0.0077	0.007683	0.007683
**P-6, E = 1, D = 1	0.276	0.275	---
E = 1, D = 2	0.438	0.436	---
E = 1, D = $\infty$	0.500	0.498	---
E = 2, D = 1	0.724	0.722	---
E = 2, D = $\infty$	0.800	0.799	---
**P-8, D = 4, L = 2	0.08074	0.08055	---
D = 2, L = 4	0.24774	0.2472	---
A-1, X = 1, Y = 1	0.19982	0.19972	0.19981
X = 0.1, Y = 0.1	0.00316	0.00316	0.00316
X = 1, Y = 4	0.34596	0.34559	0.34590
X = 0.1, Y = 0.4	0.01207	0.01207	0.01207
X = 1, Y = $\infty$ *	0.41421	0.40549	0.41075
X = 0.1, Y = $\infty$ *	0.04988	0.04884	0.04946
A-2, $\theta = 30^\circ$ , L = 1, N = 1	0.6202+	0.61769	0.61878
$\theta = 30^\circ$ , L = 4, N = 4	0.3961+	0.39431	0.39450
$\theta = 120^\circ$ , L = 1, N = 1	0.0870+	0.08665	0.08662
$\theta = 120^\circ$ , L = 4, N = 4	0.0433+	0.04272	0.04235

\*  $10^8$  was assumed to approximate  $\infty$  for computer run

\*\* 32 sided regular polygon used to simulate circular cross-section

+ These values were obtained by numerical integration across surface  $A_1$ , according to Reference 1

The FORTRAN II Computer Program described herein, CONFAC II, is a follow-on development of an earlier version, CONFAC I (Reference 5). The original program has been extensively modified and significant improvements in the flexibility of application have been achieved. CONFAC I was developed principally to compute geometric form factors between plane surfaces; no application to nonplanar surfaces or bodies was originally intended. However, because of the particular analytical approach utilized and the data handling techniques developed, it was possible to use the basic plane-to-plane program to compute factors to nonplanar surfaces, provided proper restrictions were observed.

The principal similarities and differences between CONFAC I and CONFAC II are as follows:

1. Both CONFAC I and CONFAC II require that Surface 1 be a plane polygon; it may be arbitrarily oriented in the coordinate system in which it is described (entered) in data.
2. Both CONFAC I and CONFAC II specify that if Surface 2 is a plane polygon, it may be arbitrarily oriented with respect to Surface 1 and within its own coordinate system.
3. Both CONFAC I and CONFAC II require that, if Surface 2 is a nonplanar surface, then the surface boundaries must present a valid silhouette from any point on the active side of Surface 1.
4. CONFAC I specifies that no part of nonplanar Surface 2 may lie below the "horizon" of Surface 1 when viewed from the active side of Surface 1. CONFAC II does not require that all of a nonplanar Surface 2 appear above the horizon of Surface 1. CONFAC II will automatically bisect a nonplanar Surface 2 and compute the factor to only the part which Surface 1 "sees."
5. CONFAC I cannot, in general, be used to compute the factor to a solid surface. CONFAC II will compute the factor to arbitrary solid surfaces or regular solids such as parallelepipeds, cylinders, cones, etc., with the restriction that all of the surface must appear above the horizon of Surface 1. CONFAC I cannot, in general, be used to compute factors to surfaces which are occluded or "shadowed" in a varying manner by intervening surfaces; on the other hand, the factor in such instances can be determined by CONFAC II with few restrictions.
6. CONFAC I has only two principal classes of data -- surface data and surface transformation data. No distinction of data entry is made between plane and nonplane surfaces. Surface data is distinguished from transformation data by the position of the data name on the data name card. CONFAC II, however, utilizes nine data classifications, as follows:



Class 1 - Plane polygon, silhouette developed directly from data

Class 2 - Nonplane polygon, silhouette developed directly from data

Class 3 - Internally generated disk, silhouette developed directly from generated data

Class 4 - Plane polygon, silhouette internally developed

Class 5 - Nonplane surface or solid, silhouette internally developed

Class 6 - Internally generated regular disk or solid, silhouette internally developed

Class 7 - Sphere

Class 8 - Multisurface, silhouette internally developed from all surfaces taken together

Class 9 - Transformation data

7. CONFAC II incorporates a silhouette generator subroutine which is utilized when the factor to solids or, in certain cases, to non-solids is requested. The silhouette generator computes the perspective of Surface(s) 2 from preselected positions on Surface 1 from which configuration factors are computed.
8. CONFAC II incorporates an internal automatic surface generator which computes the surface boundary coordinates of regular plane and solid surfaces from input data specifications. This feature enables the analyst to create surfaces such as circular or elliptical disks, parallelepipeds, pyramids, cones, truncated cones, cylinders, etc. An endless variety of regular surfaces can be created by CONFAC II.
9. CONFAC II incorporates extremely fast computation of factors to a sphere which is arbitrarily oriented with respect to Surface 1.

## SECTION II

### ANALYTICAL PROCEDURES

#### CONFIGURATION AND FORM FACTOR

The general equation that must be solved in the determination of the radiant-interchange form factor is (see Figure 1)

$$f_{12} = \frac{1}{A_1} \iint_{A_1} \iint_{A_2} \frac{\cos \theta_1 \cos \theta_2 dA_2 dA_1}{\pi S^2} \quad (1)$$

The following part of the integrand is the factor from the elemental surface  $dA_1$  to the total surface  $A_2$ , referred to as the configuration factor or plane point factor,  $c_{12}$ .

$$c_{12} = \iint_{A_2} \frac{\cos \theta_1 \cos \theta_2}{\pi S^2} dA_2 \quad (2)$$

Therefore,

$$f_{12} = \frac{1}{A_1} \iint_{A_1} c_{12} dA_1 \quad (3)$$

A very simple geometric interpretation of Equation 2 is given by Nusselt. The principal value of the Nusselt concept is that the computational procedure is simplified and made more accurate by the fact that no mathematical or numerical integration is required to compute the configuration factor. However, the Nusselt method yields only the configuration factor from the elemental area  $dA_1$ ; one must still integrate all such factors over surface  $A_1$  to yield the form factor  $f_{12}$  as given in Equation 3.

The Nusselt concept utilizes a hemisphere of radius  $R$  constructed over the incremental plane area  $dA_1$ , as shown in Figure 1. Every point defining the boundary of surface  $A_2$  is projected radially to the hemisphere surface and then vertically downward to the plane of  $dA_1$ , the equatorial plane of the hemisphere. The locus of all points thus projected encloses an area,  $A''_2$ , on the hemisphere base. This area  $A''_2$ , divided by the area of the base, is the configuration factor from  $dA_1$  to  $A_2$ .

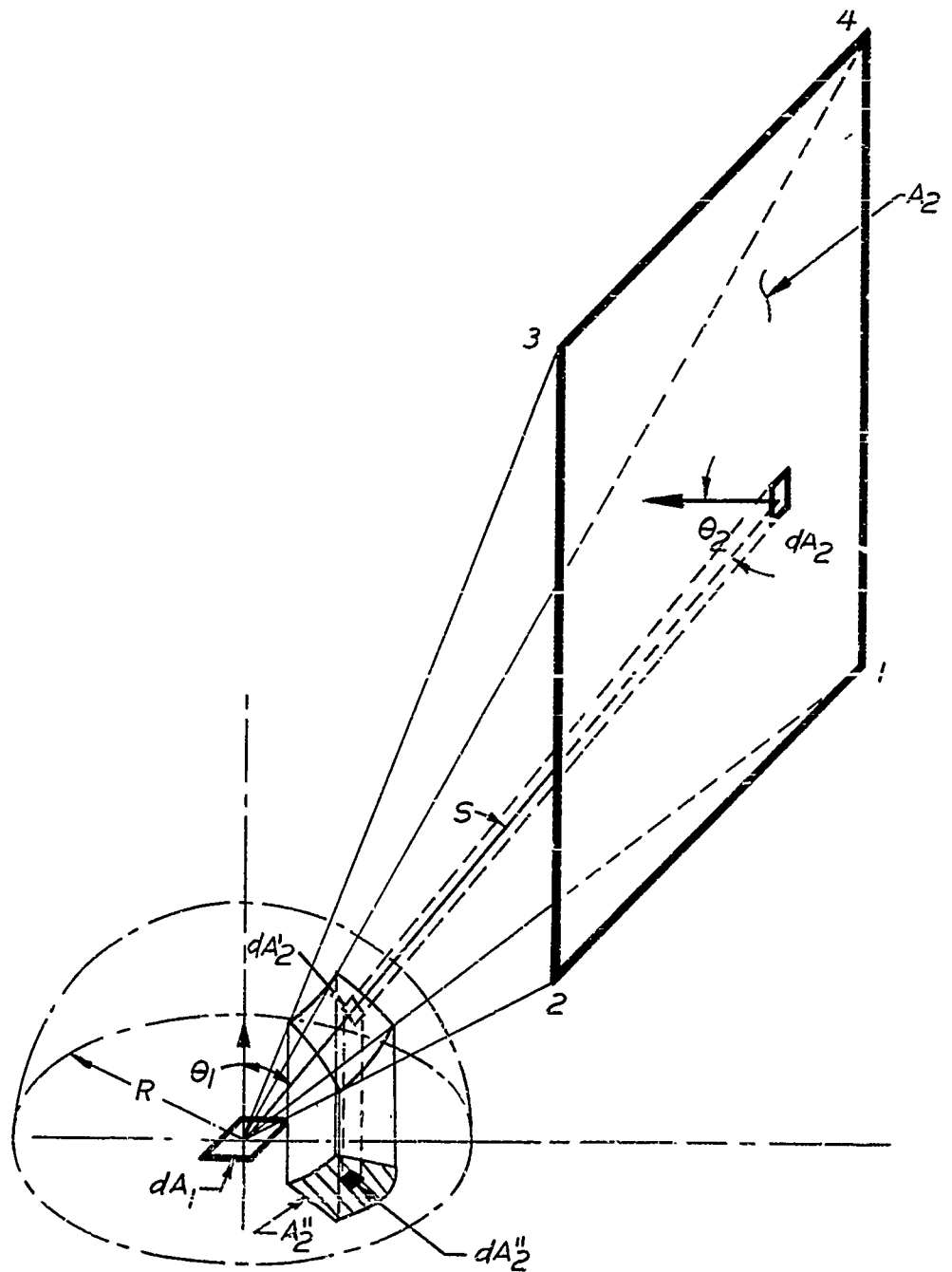


FIGURE 1. NUSSOLT GEOMETRICAL RELATIONSHIPS

The validity of this conclusion can be demonstrated as follows. Note that the elemental area  $dA_2$  is described in surface  $A_2$  by the elemental solid angle  $d\omega_1$ , or

$$d\omega_1 = \frac{\cos \theta_2 dA_2}{S^2} \quad (4)$$

Similarly, on the sphere having radius  $R$ ,

$$d\omega_1 = \frac{dA_2'}{R^2} \quad (5)$$

Because  $dA_2''$  is the projection of  $dA_2'$  on the hemisphere base,

$$dA_2' = \frac{dA_2''}{\cos \theta_1} \quad (6)$$

Inserting Equation 6 in Equation 5,

$$d\omega_1 = \frac{dA_2''}{R^2 \cos \theta_1} \quad (7)$$

The right side of Equation 4 appears explicitly in Equation 1 and, because Equation 7 is identical to Equation 4, Equation 2 becomes

$$c_{12} = \iint_{A_2} \frac{\cos \theta_1}{\pi} \left( \frac{dA_2''}{R^2 \cos \theta_1} \right) = \frac{\iint_{A_2} dA_2''}{\pi R^2} = \frac{A_2''}{\pi R^2}$$

For a sphere of unit radius (unit sphere),

$$c_{12} = \frac{A_2''}{\pi} \quad (8)$$

which completes the proof of Nusselt's method. By inserting Equation 8 in Equation 3, the original equation becomes greatly simplified; only one area integration is now required,

$$f_{12} = \frac{1}{A_1} \iint_{A_1} \frac{A_2''}{\pi} dA_1 \quad (9)$$

The computer program described herein solves Equation 9 numerically by successive algebraic evaluation of  $A_2''$  at preselected points on Surface  $A_1$ , with subsequent numerical integration to yield  $f_{12}$ , or

$$f_{12} = \frac{1}{A_1} \sum_{i=1}^N \sum_{j=1}^M \frac{A_2''}{\pi} \Delta A_1 \quad (10)$$

It should be emphasized that area  $A_2''$  is, in fact, formed by the doubly projected silhouette of surface  $A_2$  as it appears from  $dA_1$ .

The element  $dA_1$  is assumed to be oriented in the XY plane and at the origin of the coordinate system of Surface  $A_2$ . The area  $A_2''$  can be found from the line integral where  $y_1 = F(x_1)$  is the locus of the boundary of  $A_2$ ,

$$A_2'' = \frac{1}{2} \int_C (x_1 dy_1 - y_1 dx_1) \quad (11)$$

Let  $z = F(x,y)$  be the locus of the silhouette of  $A_2$ , and  $S$  the distance from  $dA_1$  to the point  $(x,y,z)$  on the silhouette of  $A_2$ .

$$S = \sqrt{x^2 + y^2 + z^2}$$

From similar triangles,

$$x_1 = \frac{x}{S}, \quad dx_1 = \frac{1}{S} dx + x d\left(\frac{1}{S}\right)$$

$$y_1 = \frac{y}{S}, \quad dy_1 = \frac{1}{S} dy + y d\left(\frac{1}{S}\right)$$

Inserting in Equation 11

$$A_2'' = \frac{1}{2} \int_C \frac{xdy - ydx}{S^2} \quad (12)$$

Equation 12 can be transposed to finite difference form by replacing the differentials with increments for numerical evaluation. Because of the problems of increment size control, it appears desirable to solve Equation 12 for a finite line segment in space and to allow the analyst to control accuracy of configuration factor computation by suitable selection of line segments describing Surface 2. If the surface is actually a polygon or polyhedra, the simulation is perfect; if the surface boundary is curved, like a disk, for example, the validity of the result is a function of the number of line segments used.

However, a much simpler and more easily understood geometric derivation, using the unit sphere, yields the result in superior computational form. Referring to Figure 2, note that the radial projection of line segment AB on the hemisphere surface forms the circular arc A'B'. Projection of A'B' to the base plane produces the elliptical arc A''B'', forming the elliptical section A''OB'' with the origin.

If all line segments describing Surface 2 are similarly projected, the area  $A_2''$  will be formed by a closed series of elliptical arcs. Surface  $A_2$  does not have to be a plane. Actually, the area  $A_2$  results from the geometry of a silhouette; any surface or object projecting an identical silhouette in the same spatial position on the hemisphere surface will produce the same area  $A_2$  and the same point factor.

Inspection reveals that the magnitude of area  $A_2''$  can be determined by computing the area of each elliptical sector, properly signed, followed by an algebraic summation.

In Figure 2, the area of elliptical sector  $A_E$  is the projected area of circular sector  $A_S$ . If the angle between the plane of the circular sector A'OB' and the XY plane is  $\gamma$ , then

$$\cos \gamma = \frac{A_E}{A_S} \quad (13)$$

The area  $A_S$  is computed from the usual polar equation, with  $\theta$  in radians,

$$A_S = \frac{1}{2} R^2 \theta$$

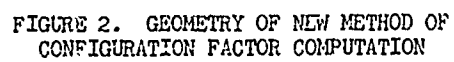
For the unit radius sphere,

$$A_S = \frac{\theta}{2} \quad (14)$$

Substituting Equation 14 in Equation 13, and solving for  $A_E$ ,

$$A_E = \frac{\theta}{2} \cos \gamma \quad (15)$$

For a polygon of N sides, the net area  $A_2''$  is found by algebraic summation of all computed  $A_E$ .



$$\Lambda_2'' = \frac{1}{2} \left| \sum_{n=1}^N \theta_n \cos \gamma_n \right| \quad (16)$$

Substituting in Equation 8, we have

$$\epsilon_{12} = \frac{i}{2\pi} \left| \sum_{n=1}^N \theta_n \cos \gamma_n \right| \quad (17)$$

A general analytical derivation of this equation is given in Reference 3, and is reported to be originally developed by Omoto in 1924.

The absolute value notation will be explained later. The use of vector algebra greatly facilitates the computation of  $\theta$  and  $\cos \gamma$ . Taking, for example, directed line segments of  $\vec{OA}$  and  $\vec{OB}$ , the vector dot product is

$$\vec{OA} \cdot \vec{OB} = x_A x_B + y_A y_B + z_A z_B \quad (18)$$

The cross product  $\vec{OA} \times \vec{OB}$  in determinant form is

$$\vec{OA} \times \vec{OB} = \begin{vmatrix} i & j & k \\ x_A & y_A & z_A \\ x_B & y_B & z_B \end{vmatrix}$$

which, upon expansion, becomes the normal vector  $\vec{V}_N$ ,

$$\vec{V}_N = \vec{OA} \times \vec{OB} = (y_A z_B - z_A y_B)i + (x_B z_A - z_B x_A)j + (x_A y_B - x_B y_A)k \quad (19)$$

where  $i$ ,  $j$ , and  $k$  are mutually orthogonal unit base vectors directed along the principal axes.

$\vec{V}_N$  is equal in magnitude to twice the area of the triangle AOB and is oriented normal to the plane of AOB so that the three vectors form a right-handed system. The magnitude is computed by the Pythagorean theorem,



$$|\vec{V}_N| = \sqrt{(y_A z_B - z_A y_B)^2 + (x_B z_A - x_A z_B)^2 + (x_A y_B - x_B y_A)^2} \quad (20)$$

The angle  $\theta$  may be evaluated from either the dot or the cross product by use of inverse functions, specifically

$$\theta = \cos^{-1} \left[ \frac{\vec{OA} \cdot \vec{OB}}{|\vec{OA}| |\vec{OB}|} \right] \text{ or } \sin^{-1} \left[ \frac{|\vec{V}_N|}{|\vec{OA}| |\vec{OB}|} \right]$$

However, an overall economy of computation results from the use of the arctan function,

$$\theta = \tan^{-1} \left[ \frac{|\vec{V}_N|}{\vec{OA} \cdot \vec{OB}} \right] \quad (21)$$

As noted earlier, the angle  $\gamma$  is defined as the angle between the plane of AOB and the XY plane. It is also the angle between the vector  $\vec{V}_N$  and the Z axis;  $\cos \gamma$  is therefore the direction cosine of  $\vec{V}_N$  with respect to the Z axis. Using the Z component in Equation 19,

$$\cos \gamma = \frac{x_A y_B - x_B y_A}{|\vec{V}_N|} \quad (22)$$

If the numerator and denominator are both divided by 2,

$$\cos \gamma = \frac{\frac{x_A y_B - x_B y_A}{2}}{\frac{|\vec{V}_N|}{2}}$$

This shows that  $\cos \gamma$  is also equal to the ratio of the signed projected area of triangle AOB on the XY plane and the plane area of triangle AOB.

In the right-handed system shown,  $\cos \gamma$  is positive when the order of computation of the vectors in the cross product causes the normal vector  $\vec{V}_N$  to point in the direction of the +Z axis ( $0 < \gamma < 90$ ). The order in which one proceeds from point to point on the boundary of Surface 2 will sign each elliptical sector accordingly; however, because the sectors are summed algebraically, the same absolute magnitude will result regardless of order. Because the point factor is always a positive number, the order is computationally unimportant. Nevertheless, the program requires that data be entered in counterclockwise order for other reasons. This will be discussed in more detail later.

The relative ease with which the point factor can be computed is best illustrated by an example. Using the triangle shown in Figure 2, and starting with line segment AB, from Equation 18

$$\vec{OA} \cdot \vec{OB} = 1 + 3 + 9 = 13$$

from Equation 20

$$|\vec{V}_{AB}| = |\vec{OA} \times \vec{OB}| = \sqrt{(-6)^2 + 0 + (2)^2} = \sqrt{40}$$

From Equation 21

$$\theta_{AB} = \tan^{-1} \left[ \frac{\sqrt{40}}{13} \right] \approx 0.453$$

From Equation 22

$$\cos \gamma_{AB} = \frac{2}{\sqrt{40}} = 0.316$$

Moving to BC,

$$\vec{OB} \cdot \vec{OC} = 3 + 3 + 9 = 15$$

$$|\vec{V}_{BC}| = \sqrt{6^2 + 6^2 + (-8)^2} = \sqrt{136}$$

$$\theta_{BC} = \tan^{-1} \left[ \frac{\sqrt{136}}{15} \right] \approx 0.661$$

$$\cos \gamma_{BC} = \frac{-8}{\sqrt{136}} = -0.686$$

Finally, line segment  $\vec{CA}$ ,

$$\vec{OC} \cdot \vec{OA} = 3 + 1 + 9 = 13$$

$$|\vec{VA}| = \sqrt{0^2 + 6^2 + (-2)^2} = \sqrt{40}$$

$$\theta_{CA} = \tan^{-1} \left( \frac{\sqrt{40}}{13} \right) \approx 0.453$$

$$\cos \gamma_{CA} = \frac{2}{\sqrt{40}} = 0.316$$

The configuration factor is, therefore, from Equation 17,

$$\begin{aligned} c_{12} &= \frac{1}{2\pi} \left| 2(0.453)(0.316) + (0.661)(-0.686) \right| \\ &= \frac{1}{2\pi} \left| -0.167 \right| \end{aligned}$$

$$c_{12} = 0.0266$$

Note the repetitive nature of the computation. Thus, all surfaces represented by straight line segments in space can be analyzed in the simple, direct manner shown.

#### COORDINATE TRANSFORMATION

The task of computing factors, even when simple "closed-form" solutions are available, is oftentimes laborious because the surfaces under consideration appear in difficult, skewed relative positions. A significant part of this effort has been eliminated by the program through the capability of general coordinate transformation (translation and/or rotation). Surface data may be entered for each surface using an individually convenient local origin. The surfaces may then be linked together by transforming one or both surfaces to a convenient third origin which is common to both surfaces. The fact that internally generated surfaces may also be transformed (excluding multisurfaces) makes this feature a very powerful tool.

Actually, two different types of coordinate transformation are used by the program. The transformation discussed in the prior paragraph is termed a "primary" transformation, and is under control of the user through transformation data entry. The second type of transformation is termed an "auxiliary" transformation, and is under internal program control only. An auxiliary transformation transforms the surface coordinates of both surfaces into a new coordinate system formed so that the XY plane of the coordinate system lies in the reference plane of one of the surfaces. The reference plane of a surface is the plane formed by the first, second and last point describing that surface. The origin of an auxiliary coordinate system is located at point 1 in the particular surface controlling the transformation. The X-axis is directed along the line segment formed by points 1 and 2. The surface unit orientation vector becomes the Z axis; the Y axis is computed orthogonal to the X and Z axes, thus locating the XY plane in the control surface reference plane.

The auxiliary transformation actually serves two purposes. First, it is utilized by Subroutine DOICU to facilitate reconstruction of the "seen" part of surfaces which are not entirely seen by the other surface. Secondly, the program requires that prior to computation of the configuration factors, Surface 1 must appear in the XY plane of the final coordinate system along with Surface 2 in its proper relative position. This is necessary to enable Subroutine MAP to select points on Surface 1 from which factors to Surface 2 may be directly computed, or from which silhouettes of Surface 2 may be generated and factors computed.

For example, suppose Figure 3 represents the surfaces of various items of equipment appearing in a compartment. The unprimed coordinate system shown may be conveniently chosen at a corner or axis of symmetry, perhaps as shown on a mechanical drawing. This system may not be convenient for data entry of the disk, however. The primed coordinate system with the origin at the center of the disk is the more logical choice in this case. The previously described surface generator will generate the disk about this origin. The disk data can then be transformed from the primed to the unprimed system by a primary transformation. The choice of generating the cube and transforming, or directly entering data from the unprimed system, is left to the user as it requires about equal effort both ways. The plate coordinates can be easily entered from the unprimed system. Now, suppose we desire the form factor from the disk to the plate. If the data are entered as discussed above (including the transformation data), the program will generate the disk and then primary transform disk coordinates to the unprimed system. Since the disk is bisected by the plate, an auxiliary transformation of all coordinates, both disk and plate, will be made from the unprimed to the quad-primed system. Now, that portion of the disk appearing above the active side of the plate will be determined, and an auxiliary transformation of the plate and the truncated disk will be made to the double primed coordinate system, i.e., the reference plane of the disk. The disk is now in a position for mapping, and the plate coordinates are proper for obtaining the configuration factors. A similar manipulation of surface data would be made to obtain the form factor to the cube with one exception - no truncation of the disk would occur and the auxiliary



transformation to the double-primed system would occur immediately after primary transformation.

The transformation technique utilized for a primary transformation differs from the customary method whereby "old" coordinates plus translation data and direction cosines or Euler angles are supplied, from which a "new" set of coordinates are derived. The program requires the coordinates of any three points (not in a line) measured from the new origin. These data are then used to derive direction cosines and translation terms, by which the old coordinates are then transformed to the new origin.

The reader may find it easier to visualize transformation in terms of the movement of the surfaces instead of the origins. In the case of the disk, again referring to Figure 3, we may say we generated the disk with its center at the origin of the unprimed system and in its XY plane, and then moved the surface to the position indicated by the primed system. This viewpoint appears more realistic when motion is simulated by transforming a surface along a particular path.

The mathematical treatment of primary and auxiliary transformation is presented in Appendix C.

#### SILHOUETTE GENERATOR

As noted in the introduction, CONFAC I cannot, in general, be used to compute the form factor to solid surfaces. Subroutine FACTOR requires a single array be made available containing the surface boundary points, and only those points, which, when taken in numerical sequence, form a valid silhouette of Surface 2 from a particular point in Surface 1. It is impossible to generally satisfy this requirement with a single input array if Surface 1 is finite and Surface 2 is arbitrarily nonplanar or solid. It is the function of the silhouette generator to determine which points in a given set of Surface 2 data form the silhouette from preselected viewpoints on Surface 1.

The silhouette generator computes the silhouette from the perspective of Surface 2 developed on the Z-unity ( $Z = +1$ ) plane. The perspective on the Z-unity plane is the locus formed in the plane by the boundary of the solid angle subtended by Surface 2.

For example, the view of a cube from two positions on the XY plane is shown in Figure 4. The coordinates of each point in the Z-unity plane are derived in the following manner from the coordinates of its corresponding point on the cube. Note the triangle formed by the origin, point 2 in the cube, and point Q, the vertical projection of point 2 on the XY plane. A similar triangle is constructed from point 2' to point N. From similar triangles,

$$\frac{ON}{OQ} = \frac{Z_2}{Z_2'} \quad (22)$$

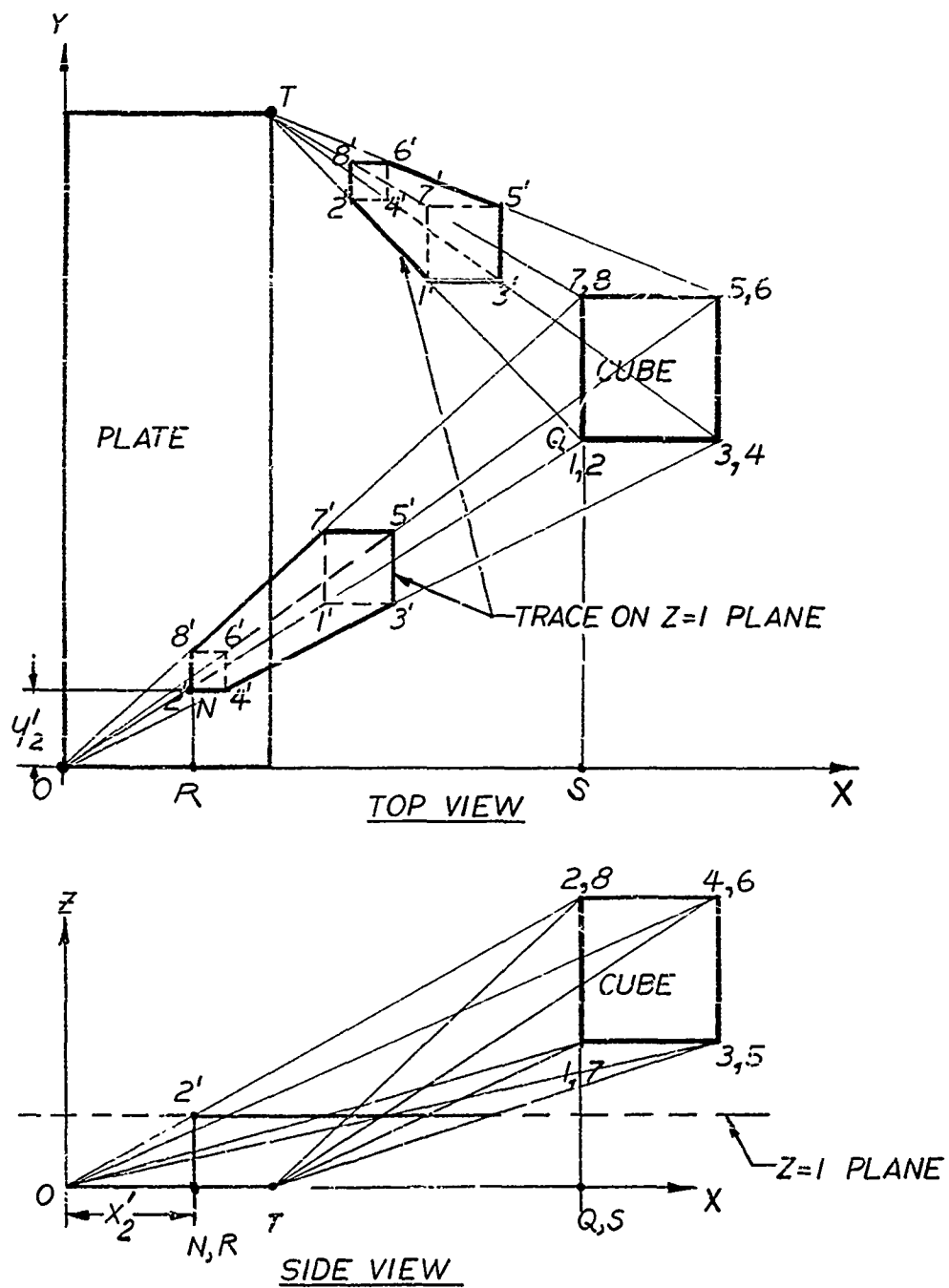


FIGURE 4. SIMPLE SILHOUETTE GEOMETRY

In like manner, using triangles RON and SOQ in the top view,

$$\frac{ON}{OO} = \frac{OR}{OS} = \frac{NR}{QS}$$

but  $OR = X_2'$ ,  $OS = X_2$ ,  $NR = Y_2'$ ,  $QS = Y_2$  and  $Z_2' = 1$ .

Therefore,

$$\frac{X_2'}{X_2} = \frac{Z_2'}{Z_2} = \frac{1}{Z_2}$$

$$X_2' = \frac{X_2}{Z_2} \quad (23)$$

and similarly,

$$Y_2' = \frac{Y_2}{Z_2} \quad (24)$$

This reduction to two dimensions results in considerable simplification. Given the coordinates (X, Y) and point connections data, it is possible to determine the line segments forming the silhouette by application of a simple criterion. At each point on the silhouette, those line segments forming the largest included angle define the silhouette. For example, at point 2' in the lower silhouette in Figure 4, vectors 2' - 3', 2' - 1' and 2' - 4' emerge from the point. Vectors 2' - 3' and 2' - 4' obviously form the silhouette, and can be numerically selected by applying the criterion.

Figure 5 shows the development of the Z-unity plane silhouette of a multisurface. In contrast to point D, Surfaces S2 and S3 appear separated in the silhouette when viewed from C.

Note the line connecting 4 to 7. This artifice - a "bridge" line - is utilized to cause the silhouette generator to include both surfaces in the silhouette, otherwise surface S3 would be ignored. Because the line has no width, it has no effect on the factor computation, but the silhouette generator follows the line as if it were a boundary of the multisurface S2 plus S3.

The distinguishing difference between the silhouettes shown in Figure 4 and Figure 5 is the fact that "crossover" occurs in Figure 5. The silhouette at a crossover is formed by intersecting line segments at a point between line segment extremities. The detection of such intersections, and the computation of the coordinates of the intersection, requires considerable analysis with resultant increased computer time. Because of this, silhouette analysis is termed "simple" if no investigation is made by the silhouette generator to detect crossovers, and "complex" when such is made. Only multisurface data (class 8) are run in the complex mode. All other surface data requiring the silhouette generator (classes 4, 5 and 6) are run in the simple mode.



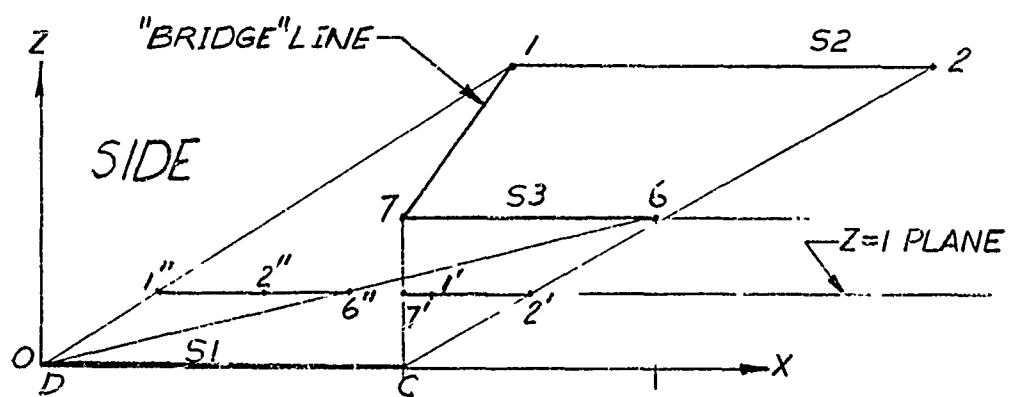
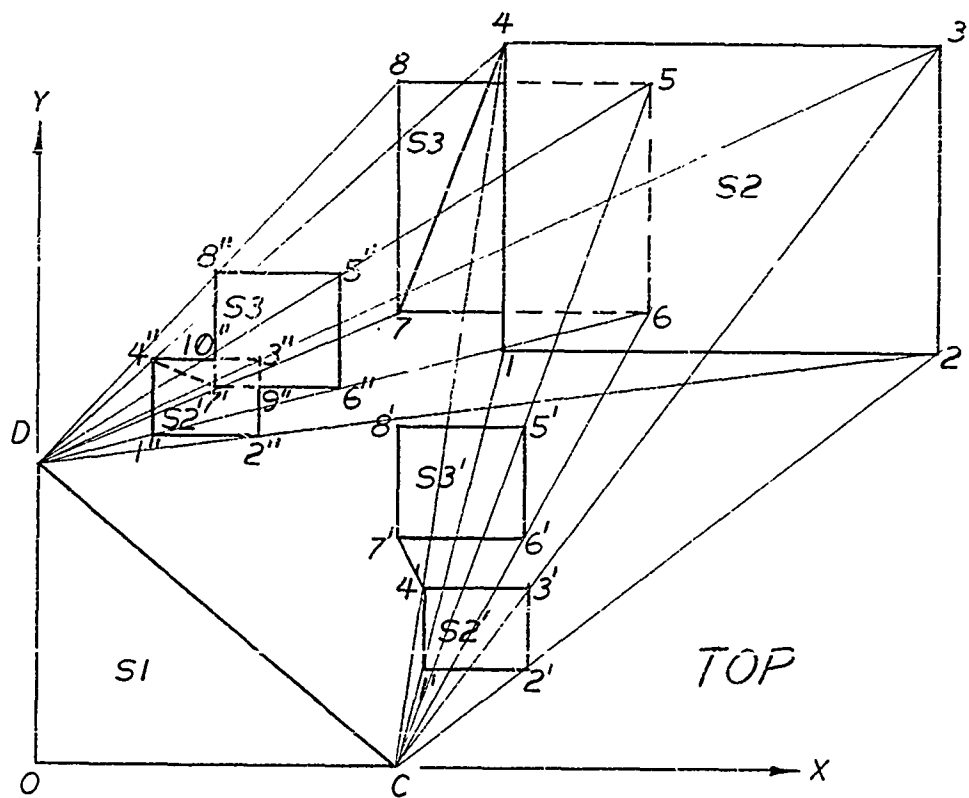


FIGURE 5. COMPLEX (MULTISURFACE) SILHQUETTE GEOMETRY

## SURFACE GENERATOR

The program cannot directly compute factors to curved surfaces or boundaries such as disks, cylinders, etc. A series of line segments must be substituted for a curved line. In general, the more line segments used, the more accurate the simulation. Because every surface point requires 3 coordinates (and connecting points data, when the silhouette must be computed), preparation and entry of data for even a modest simulation of a cylinder can involve a considerable amount of effort. The internal surface generator eliminates practically all of this effort.

The surface generator is used to create surfaces entered under data classes 3 or 6. Regular plane polygons are created under Class 3, but no connections data are generated. A regular plane polygon or solid surface, including connections data, is created under a class 6 entry.

The surface generator "creates" a surface in accordance with cross section specifications. The following information is required to create a class 3 surface:

1. Number of cross section division (sides)  $\geq 3$
2. Coordinates (X, Y, Z) of center of polygon
3. X-axis Radius
4. Y-axis Radius

Because a class 6 surface may have one or more cross sections, the following data are required:

1. Number of cross section division (sides)  $\geq 3$
2. Number of cross sections
3. Coordinates (X, Y, Z) of first cross section
4. X-axis Radius of first cross section
5. Y-axis Radius of first cross section

If more than one cross section is specified, the following data are required for each additional cross section: X-axis radius, Y-axis radius and Z-coordinate. All cross sections are created parallel to the XY plane of the generator coordinate system, and must be specified above the XY plane. Note that X, Y coordinates are required to locate the first cross section only. If more than one is specified, all are oriented along the same vertical centerline to the position specified by the respective Z coordinate.

The basic generating element is the ellipse. Because only complete polygons are generated, the total angle of  $2\pi$  radians about the vertical centerline is divided by the number of sides specified to yield the unit parametric angle  $\phi$  in the equations of the ellipse:

$$\phi = \frac{2\pi}{N}$$

$$X = (XR) \cos \phi$$

$$Y = (YR) \sin \phi$$

Instead of the conventional semi-major and semi-minor expressions, the terms "X-Radius" and "Y-Radius" are utilized - the larger of the two becomes the semi-major axis as shown in Figures 6 (a), (b), and (c). When  $XR = YR$ , the generating figure is circular and a regular polygon of  $N$  sides results. Notice that the generating figure always circumscribes the generated polygon. The radius vector always starts in the same relative position parallel to X-axis and moves counterclockwise about the vertical centerline of the generated cross section. Considerable computing time is saved by using  $\sin(\phi + \beta)$ ,  $\cos(\phi + \beta)$  trigonometric formulae for computation of  $X$ ,  $Y$  after unit values are obtained by use of computer library functions.

Figure 6 (d) shows an eight-sided polygon elevated above the XY plane. Figure 6 (e) indicates the order in which point numbers are assigned to a solid surface. The first point is always assigned to the first coordinates in the first cross section. Numbers are assigned in numerical sequence vertically until the last cross section is numbered, for a particular value of  $\phi$ ; the sequence is continued in similar manner with the first cross section and the next value of  $\phi$ , until all points are defined.

Point connections data are also computed for each point for Class 6 surfaces. For example, in Figure 6 (e), points 2, 3 and 15 are computed for point 1; points 1, 4 and 16 are computed for point 2, etc. This information is used by the silhouette generator.

An example of the variety of objects which may be created by a few cards of specifications are shown in Figure 6 (f). The cone vertex is generated merely by specifying zero X-radius and Y-radius.

The internal surface generator also computes the surface area of the generated solid, if the cross sections are similar. Because the silhouette generator analyzes the solid figure, the total surface area is computed. For instance, the area of the prismatic cylinder shown in Figure 6 (c) would include the top and bottom polygons. The surface area computation analytical development is given in Appendix D.

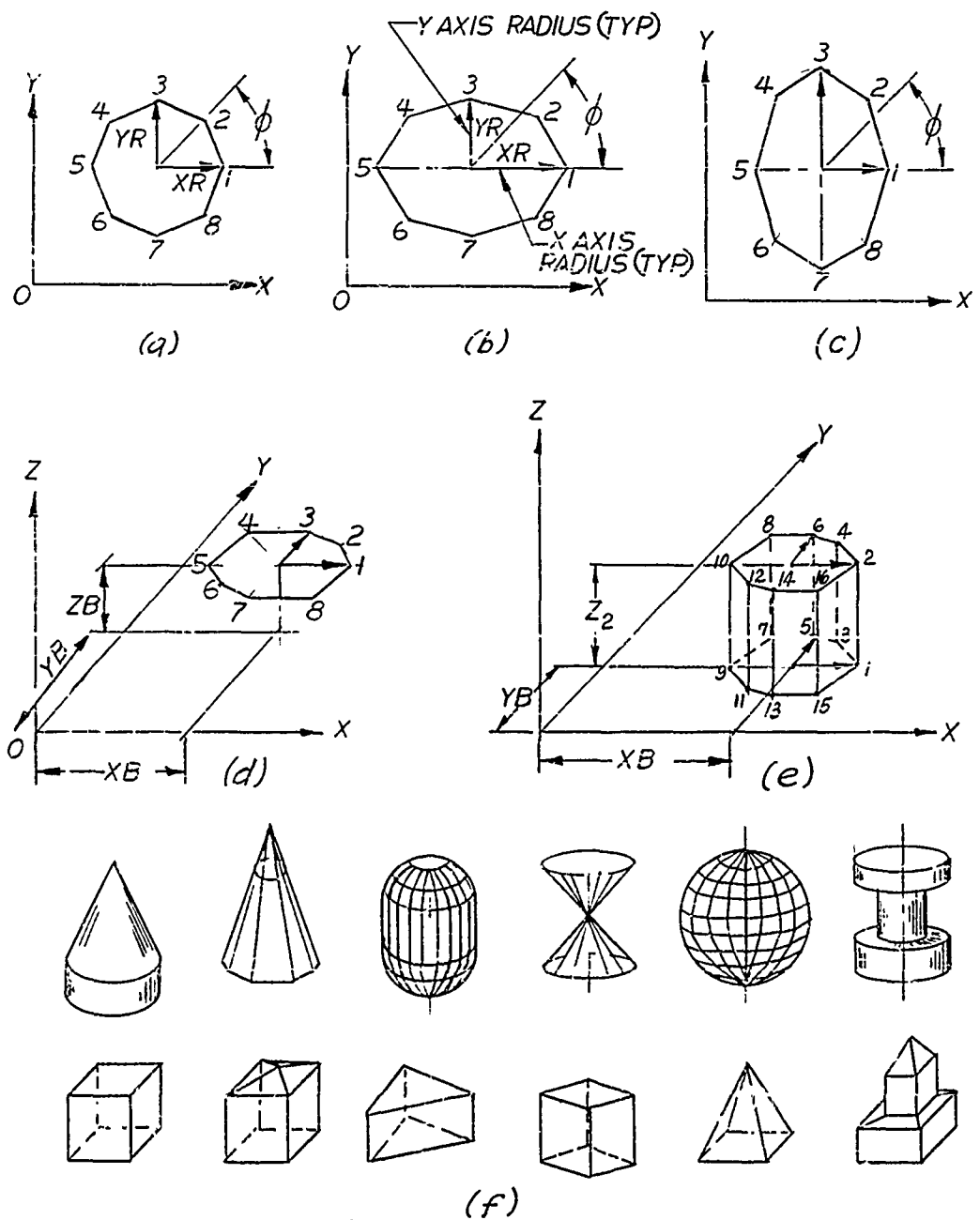


FIGURE 6. CONFAC II SURFACE GENERATOR

## SECTION III

### COMPUTER PROGRAM CONTENTS

#### PROGRAM DESCRIPTION

The program is written in IBM 7090 FORTRAN II source language. The source deck consists of the Main Program and Subroutines UNIVFC, TXFRM, COICU, MAP, SILFAC and FACTOR. An input-output tape compatibility Subroutine written in IBM 7090 (FAP) machine language is included. Algebraic routines required from library tape are SQRT (Square Root), ARCTAN (Inverse tangent trigonometric function), COS (Cosine trigonometric function), and SIN (Sine trigonometric function). The source programs are presently dimensioned so that a 32 K core size is required. NAA Library Subroutines COUNTV and TIMEV are also used by Subroutine SILFAC when operating in the NAA 7094 system.

#### Main Program

The functions performed by the Main Program are as follows:

1. Reads in surface, transformation and run data.
2. Processes input surface data and prints immediately upon completion. Run instruction data are read in and processed one card at a time and processed at once. No printout of the complete run instructions is given, as was in CONFAC I.
3. Selects the proper data for processing according to the run instructions.
4. Examines each run instruction and calls in proper subroutines for processing.
5. Prints diagnostic error indications when possible.
6. Prints standard or detailed output as indicated by run instructions.

#### Subroutine UNIVFC

This subroutine computes the components of a unit orientation vector normal to the reference plane formed by the first, second and last point in surface data classes 1, 3, 4 and plane 6. The cross product of vectors 1-2 and 1-last is computed and normalized. The vector is formed normal to point 1, and is located on the active side of the surface, thus orienting the surface.

It also computes a new fourth point normal to the new three points submitted in transformation data and an old fourth point normal to the old three points in the surface data to be transformed.

#### Subroutine TXFRM

The first section performs the auxiliary transformation. This transformation is used to reconstruct a surface which is bisected by the second surface. It also tests Surface 1 to determine if the reference plane is substantially in the XY plane of its coordinate system. If it is not, an auxiliary transformation is effected to move the surfaces to fulfill this requirement prior to computation of silhouettes or factors.

This subroutine also performs a primary transformation as indicated by P.U. instructions and transformation data. This transformation, if indicated for a surface, is accomplished prior to entry to subroutine DOICU so that tests of the surface "view" of each other occur in their transformed position(s).

#### Subroutine DOICU

The function of this subroutine is conveyed literally by its name DO-I-C-U. Given surfaces A1 and A2 with the "active" side of each surface identified by the surface orientation unit vector, the question is asked; Is all, part, or none of surface A1 "seen" by A2? Conversely, does A2 see all, none, or part of A1? This is accomplished by computing the vector dot product formed by the unit vector in one surface with the vector formed by point 1 in the first surface and each point in the other surface (See Figure 7). The sign of the dot product indicates whether the angle between the vectors is less than or greater than 90°, which reveals the position of the point relative to the plane of the viewing surface. In Figure 7 (a) the dot products from surface A1 to A2 are all positive, and conversely, all from A2 to A1 are likewise positive: A1 sees all of A2; A2 sees all of A1. However, in Figure 7 (b) all dot products from A2 to A1 are positive, but all from A1 to A2 are negative. Hence, in general, if all dot products from one surface to another are all negative, then the surfaces do not see each other, even though the converse products may be positive. There is also the trivial case where all products are zero, in which case the surfaces are in the same plane, and obviously again cannot see each other.

Figure 7 (c) shows a surface A2 bisecting surface A1. In this case, some of the dot products from A2 and A1 are positive and some negative. In Figure 7 (d) both A1 and A2 are bisected. Nonplanar surface A3 was added to show how it would be bisected by A1. Surface A3 has no orientation vector and thus no test is made of the view from this surface. The vertical dashed line in A2 represents how the plane 1-2-5-6 in A3 might bisect A2. DOICU will not detect this condition. If the configuration factor,  $C_{23}$ , were required, DOICU would properly bisect A3. However, if the factor to the concave side only is desired, an error would result because part of A2 sees the convex side of A3. This represents one of the limitations of CONFAC I which is carried over to CONFAC II.

If a surface is bisected, DOICU reconstructs the surface data to exclude the area not seen by the other surface. If point 1 in the original surface is

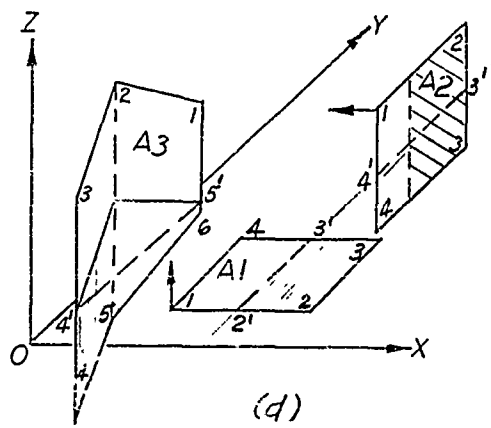
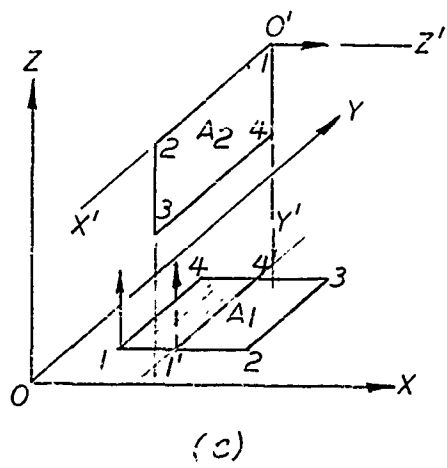
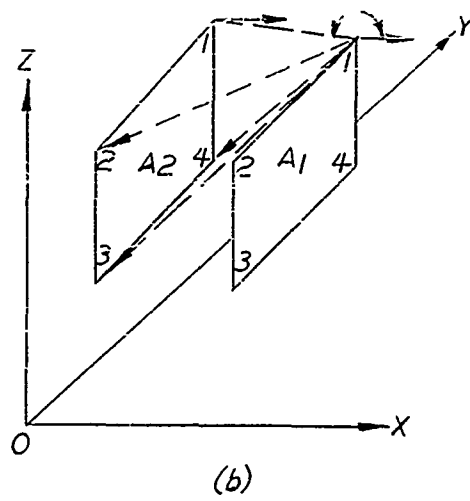
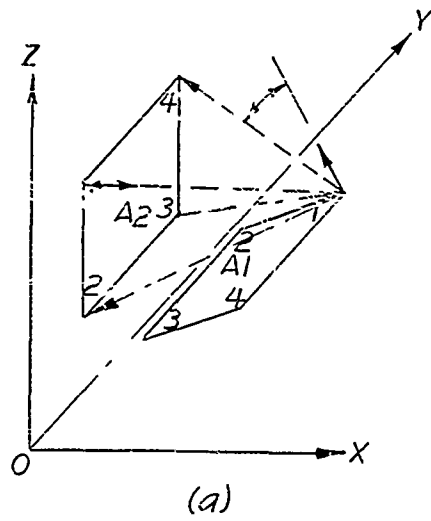


FIGURE 7. DOICU SURFACE ANALYSIS

removed as a result, a new orientation vector is created over the new point 1 as shown in Figure 7 (c). Notice that in reconstructing A3 [Figure 7 (d)], DOICU created the new array 1, 2, 3, 4', 5'. This "surface" is identical to the actual surface seen by A1 insofar as factor computation from A1 is concerned.

The bisection of a surface is done in a simple manner, with the aid of the auxiliary transformation capability. For example, in Figure 7 (c), the coordinates of both surfaces are transformed so that A2 lies in the XY plane of the auxiliary (primed) coordinate system. Each point in A1 is tested, in numerical order, until a change in the sign of the Z-coordinate occurs. The coordinates of the new points where the transition line segment crosses the X' Y' plane ( $Z' = 0$ ) are obtained by computing X and Y intercepts of traces projected on X' Z', Y' Z' principal planes.

#### Subroutine MAP

The double integral in Equation (9) and its numerical counterpart in Equation (10) mathematically represent the volume under a surface defined by the configuration factor  $c_{12} = f(X,Y)$ . Subroutine MAP decides the location (X,Y) from which each factor to Surface 2 will be computed.

It is assumed that Surface 1, being classed as a plane, is a plane surface throughout. The program insures only that the reference plane of Surface 1 is in the XY plane of the final coordinate system. MAP will use the X,Y coordinates of all points, and assumes a value of 0 for all Z coordinates. This procedure cannot properly map a nonplanar surface.

Subroutine MAP determines the maximum Y coordinate and the minimum Y coordinate from among the points defining Surface 1 (Figure 8). The total vertical distance between  $Y_{max}$  and  $Y_{min}$  is divided into equal vertical increments, as specified by the run instructions. Then, horizontal lines are scribed across (parallel to X-axis) the surface at each vertical increment position, including  $Y_{max}$  and  $Y_{min}$ . The point at which a horizontal line intersects the left (toward the negative X direction) boundary of Surface 1 is termed "X-left" and the intersection on the right, "X-right". Each horizontal line segment thus created is termed a "mapping line". Each mapping line segment is also divided into an equal number of increments as specified by the run instructions. All mapping lines are divided into the same number of increments, not necessarily the same size of increment. Obviously, if Surface 1 converges to a point instead of a line at  $Y_{max}$  or  $Y_{min}$ , the horizontal increment is 0. A configuration factor is computed at each increment point along a mapping line, including X-left and X-right, which means the number of factors per line is one greater than the number of increments.

The number of increments is automatically set to 24 horizontal and 24 vertical, but can be separately specified by input data to 3, 6, 18, 24, 30, 36, 42, 48, 54, or 60. The details are discussed in Section IV.



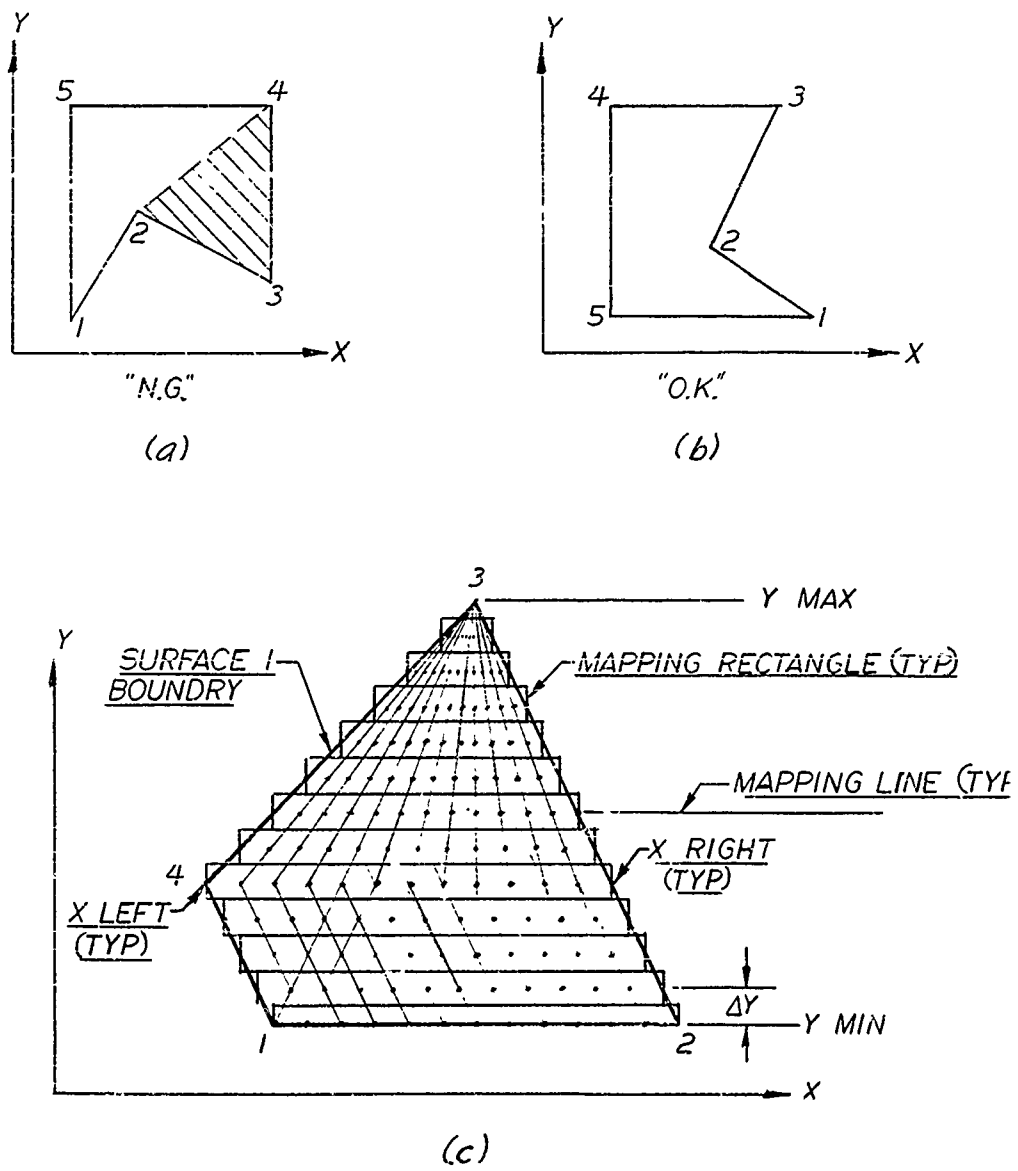


FIGURE 8. MAPPING PROCEDURE

A typical example of Surface 1 manning using a standard (24 x 24) increment is shown in Figure 8 (c). The manning area is also computed by Subroutine MAP, it is the sum of the rectangular areas formed by each manning line. A measure of form factor accuracy is the degree with which the manning area approximates the actual surface area.

Figure 8 (a) illustrates a Surface 1 orientation which cannot be satisfactorily manned because the crosshatched area is ignored. The program does not detect more than one left and one right intersection between a manning line and the surface boundary; therefore, point 3 is ignored. The same surface rotated sufficiently may be acceptable, however, clearing this restriction, as shown in Figure 8 (b).

#### Subroutine SILFAC

This subroutine computes the silhouette of Surface 2 which appears from the points selected on Surface 1 by Subroutine MAP, and then computes the configuration factor from this silhouette. After all configuration factors have been determined, the form factor is computed by numerical integration.

Surface data entered as Class 4, 5, 6, 7 or 8 is processed by SILFAC. Class 7 data, a sphere, is processed in this routine, but the silhouette generator is not utilized; a closed form solution is used instead (see Appendix E).

Classes 4, 5 and 6 are processed by the silhouette generator in the 'simple' mode; only those points given in connections data are analyzed to select the next point on the silhouette. Surfaces such as planes, cylinders, parallelpiped, etc. may be processed in the 'simple' mode.

Class 8, a multisurface, is the only class processed in the 'complex' mode. One or more (limitations on data are given at the end of this section and in Section IV) surfaces may be processed as a multisurface. Processing in the 'complex' mode is complicated because the computer must test all line segments in all surfaces (including the surface in which the segment appears) in order to select the next point forming the silhouette, or to compute the next point on the silhouette. This analysis is further complicated by ambiguities resulting from normal imprecision in input data and internal arithmetic roundoff, necessitating the use of numerous time consuming tolerance tests. Consequently, a factor computation in the 'complex' mode takes considerably longer than the 'simple' mode.

If a surface is processed as 'simple' when it should be 'complex', a wrong silhouette will be computed whenever a 'crossover' (an intersection of two line segments) occurs. The configuration factor computed from that silhouette will be wrong.

It is possible to detect certain kinds of trouble in the silhouette generator from the detailed silhouette output which lists the points forming the

silhouette. Normally, the silhouette will start at the lowest leftmost point in the Z-unit plane perspective developed for the noted point in Surface 1, and move progressively from point to point in a counterclockwise manner, keeping the perspective area to the left. When a crossover occurs, the point is computed and assigned the next highest number in the silhouette array. For example, from point "n" in Figure 5, the silhouette derived in the convex mode would appear in the detailed silhouette output as "Line No., Point No., 1" 2" 9" 6" 5" 8" 10" 4" 1." However, if this problem were run as simple (both surfaces entered together as Class 4) instead, Surface 93 would be ignored because the crossover at point 9 would not be computed. The silhouette would appear normal, but actually be wrong, as follows:

Line No., Point No., 1" 2" 3" 4" 1"

A bad silhouette can sometimes be detected by the presence of internal "looming". Normally, a silhouette is completed by a return to the starting point. But, if, for some reason, a wrong path is chosen, it may loop a polygon within the perspective. Looming is characterized by the repeated appearance of the same sequence of numbers. No internal pattern recognition is attempted, the only detection is visual examination of the detailed output.

The coordinates of the silhouette on the  $Z = 1$  plane are used directly for factor computation instead of the actual points on the surface in space. Because the  $Z$  - coordinate of each point is 1, the configuration factor equations for this special case can be simplified, and computing time reduced. SIMFAC, therefore, contains its own equations for configuration factor computation and numerical integration across Surface 1. The integration process is similar to the procedure given in Subroutine FACTOR. Subroutine FACTOR has been retained from COMFAC I for factor computations not utilizing the silhouette generator.

#### Subroutine FACTOR

This subroutine computes configuration factors from each point on Surface 1 selected by MAP to Surface 2. The exchange coefficient is computed by numerical integration of configuration factors across Surface 1, from which the form factor is finally derived as the area-weighted mean of all configuration factors.

Factors are computed for each point along each mapping line, moving from X-left to X-right, by translating the origin of the Surface 2 coordinate system in X. The analysis and equations are organized for minimum computational time; constants at each loop level are computed once prior to loop entry. Because the usual output desired is only the form factor, configuration factors never are not computed unless a detailed output is requested. A numerical integration of computed point function with respect to X is performed before proceeding to the next line. After all horizontal integrations are completed, these products are integrated with respect to Y, and divided by the mapping area computed in subroutine MAP.

A standard 24 X 24 grid results in 625 configuration factors to be computed. The question naturally arises as to whether this many configuration factors are actually required. If the configuration factor changes very little across Surface 1, then it is probably too many; but if there are sharp changes in the factor, and third place accuracy is desired, then it is probably sufficient. Contrary to off-hand expectations, a more sophisticated integration rule such as Simpson's or Weddle's is not as accurate as the trapezoidal rule for standard increments if the factor function alone changes rapidly. Weddle's rule was initially used which explains why the program increment control is in groups of six (except the initial 3 which is not in ONFAC I). If the factor varies smoothly, a 6 x 6 weddle's rule integration (49 factors) is probably as accurate as the standard 625 factors presently used by the trapezoidal rule. The time saved is appreciable when running many factors. If desired, Weddle's rule may be inserted in the source deck and compiled with no other changes required.

The form factor computed by the above is from that part of Surface 1 which "sees" Surface 2. If Surface 1 is bisected, then the computed factor must be reduced in proportion to the area reduction. This is required because the total active side of Surface 1 entered in data is considered the radiant surface.

#### GENERAL RULES AND RESTRICTIONS

The following general rules and restrictions must be observed for normal program operation:

1. All data must be derived from right-handed rectangular coordinate systems.
2. Points 1, 2 and the last point in plane surface input data (Class 1 and 4) must not form a straight line in space.
3. The active side of a plane or nonplanar surface is established by entering the boundary points in counterclockwise order, as they appear when facing the active side.
4. If the factor to a Class 2 (nonplanar) surface is required, only the active surfaces should be seen from any point on Surface 1, and they must also be seen from every point on Surface 1.
5. All surfaces used as Surface 2 which utilizes the silhouette generator (Classes 5, 6, 8, or 4 if included in Class 8) must appear above the plane of Surface 1, i.e., all Z - coordinates must be nonzero and positive, prior to factor computation.
6. A primary transformation of Class 8 data is not permitted. Also, no auxiliary transformation is permitted; Surface 1 must be in the XY plane of the Multisurface coordinate system as entered in data.
7. Detailed restrictions and limitations upon input data are given in Section IV.

## SECTION IV

### INPUT DATA

#### DATA SPECIFICATIONS AND SPECIFIC RESTRICTIONS

Input data consists of externally computed surface data, specifications for internally created surfaces, transformation data and run instructions (operator requests). Also title and comments cards may be entered as required.

Data type is classified by the use of an integer from 1 to 9 placed in column 1 of the data name card, followed by a 1 to 5 FORTRAN character name to provide data identity within each class. The classes of data are described below.

##### Class 1 - Plane Polygon

The X, Y, and Z coordinates of each point defining the surface boundary are required. Only one side of a single plane surface can be made active i.e., may interchange radiant flux with another surface. The active side is established in the following manner: Face or look at the desired active side, and select any point on the surface boundary as point number one. Proceeding in a counterclockwise direction about the boundary of the surface, select the remaining points in sequence. If this rule is followed, the surface will always be on the left when moving along the boundary.

The X, Y, and Z coordinates of each point are entered on the data cards in the above sequence, and each point is numbered internally according to its position in the data.

It is assumed that a Class 1 surface is a plane surface. No internal check is made to verify this (in contrast to CONFAC 1). If a substantially nonplanar surface is classed as a plane surface, serious errors in naming could result if used as Surface 1, or wrong factors computed if used as Surface 2.

No point connections data are entered under Class 1; the silhouette generator is not used.

##### Class 2 - Nonplanar Surface

Two or more plane surfaces, not in the same plane, adjoining or connected, and entered as one package is termed a nonplanar surface.

A Class 2 surface can be used as Surface 2 if the side of each facet selected as the active side, and only those sides, are seen from everywhere on the active side of Surface 1. The counterclockwise order of data

entry establishing the active side is also required as in Class 1, but no orientation vector is generated.

No connection data is required because the silhouette generator is not used.

#### Class 3 - Internally Generated Plane Polygon, No Connections Data

The internal surface generator will compute the coordinates of each point defining a plane polygon, parallel to the XY plane, with an orientation vector erected over point 1 and directed toward the +Z axis. A detailed description of the internal surface generator is given in Section II.

The data required for a Class 3 surface is:

No. of sides,  $3 \leq N \leq 100$

X - Axis Radius

Y - Axis Radius

X, Y, and Z coordinates to center of polygon

A Class 3 surface is used in the same manner as a Class 1 surface. The same rules and restrictions apply.

#### Class 4 - Plane Polygon with Connections Data and Class 5 - Nonplanar Polygon or Solid Surface with Connections Data

A Class 4 surface is actually a Class 1 surface with connections data added making it possible for it to be processed with the silhouette generator. But, in general, no useful purpose is gained by the use of the silhouette generator to process a plane surface, unless combined with other surfaces. Therefore, a Class 4 surface is processed as a Class 1 surface, unless it is listed under a Class 8 entry.

A Class 5 surface is always processed in the simple mode by SILEAC unless listed under a Class 8 entry.

A maximum of 100 boundary points may be entered describing a Class 4 or 5 surface. Up to 4 connecting points for each boundary point may be entered. If more than four connecting points are required, one may enter more boundary data points having the same coordinates and connecting to each other, using the surplus (3) connections to satisfy the additional connections requirement. However, if more than two such identical boundary points are used, the surface cannot be processed in the simple mode. This restriction in most practical situations can be circumvented by separating the points slightly with little effect on the final form factor computed. If this cannot be done, the surface must be listed under a Class 8 name and processed in the complex mode.

#### Class 6 - Internally Generated Polygon or Polyhedron, Including Connections Data

A detailed description of the internal surface generator is given in Section II. A class 6 surface is always processed by SILFAC - in the simple mode if used directly, and complex if listed under Class 8. The data required to create a Class 6 surface are:

1. No. of cross sections
2. No. of cross sections divisions (sides)
3. Coordinates and generating radii of first cross section.
4. Z-coordinate and generating radii of additional cross sections, if any.

Attention is directed to general restrictions 4 and 5 in Section III.

#### Class 7 - Sphere

The radius and the X, Y, and Z coordinates of the sphere are required. A primary transformation of a sphere is pointless and therefore not permitted. Arbitrary orientation of both Surface 1 and sphere is allowed. One peculiarity exists which differs from the usual treatment of bisected surfaces. If the plane of Surface 1 bisects the sphere, the area of the spherical surface above the horizon of Surface 1 will be computed. Now the sphere cannot bisect Surface 1 in the usual sense, but it is possible a bisected sphere may be partly or totally inside the boundaries of Surface 1 - embedded in the surface. In this case, the program will merely assign a zero for the configuration factor when the viewpoint from Surface 1 is inside the sphere. This zero will be integrated as usual with the other factors computed along each scanning line. No computation of the Surface 1 area seeing the sphere is made, however, even though part of Surface 1 is not seen by the sphere.

#### Class 8 - Multisurface

A Multisurface consists of from one to eleven Class 4, 5, or 6 surfaces. A Class 8 surface, and only a Class 8 surface, is processed in the complex mode. The only data entry necessary to indicate the surfaces which comprise a Multisurface are the names assigned each surface.

#### Class 9 - Transformation Data

Transformation Data consists of the coordinates of three points in a surface, not in a straight line, derived from the "new" position of a surface which has been moved in its coordinate system. One may, with equal validity, interpret the transformation to mean that the origin of the coordinate system is being moved to a different position, and the data are the coordinates of

each point taken from the new origin. The three points selected need not be chosen or entered in any particular order, nor must the same points be used if more than one different primary transformation of the same surface is desired.

#### Run Instructions

Run instructions specify, for each factor desired, the following:

1. The name of Surface 1 (emitter)
2. The name of Surface 2 (receiver)
3. Transformation data name(s) for Surface 1 and/or 2, if required.
4. Whether a standard or detailed output is desired, by inserting code letter "D" for detailed output.
5. The horizontal and/or vertical divisions to be used in mapping surface 1. The major divisions which may be used are 6, 12, 18, 24, 30, 36, 42, 48, 54 and 60, but in run instructions these divisions are specified, respectively, by the integers 1, 2, 3, 4, 5, 6, 7, 8, 9 and 10. A special division of 7 may be specified by the integer 11.

#### DATA DIMENSION RESTRICTIONS

1. A maximum of 100 boundary points (300 coordinates) for each surface entered as Class 1, 2, 4, and 5.
2. A maximum of 100 points, equivalent to 100 sides, generated by Class 3 data.
3. For Class 6 data, the number of sides plus one, times the number of cross sections, must not exceed 101 if plane, and 102 if non-planar.
4. The grand total of surfaces entered or generated by Class 4, 5 and 6 must not exceed 11.
5. The grand total of surfaces entered or generated by Classes 1, 2, 3, 4, 5 and 6 must not exceed 26. If a detailed silhouette output is requested, the grand total must not exceed 16.
6. The total number of Class 7 data must not exceed 9.
7. The total number of Class 8 data must not exceed 12.
8. The total number of Class 9 data must not exceed 10.



#### PROGRAM CONTROL

The program deck setup is shown in Figure 36. Note the presence of a "T" card immediately following the \* DATA Card and the variable format. A "T" card has a "T" in column 1, and serves two purposes. Columns 2 - 72 may contain job title, name of programmer, etc. and will be printed in the output of input data and each factor result. The "T" card also initializes data storage locations, so that new input data can be read in. This means, however, that the old data is effectively wiped out, and is no longer available for fac or commutations, unless re-entered as input data. It is obviously unnecessary to use the "T" card unless all available locations are used up.

Actually, a "T" card does not necessarily have to follow the variable format unless one desires the title to be printed, because the data location counters are automatically initialized at the start of the program. But subsequent re-initialization can be accomplished only by a card with a "T" in column 1.

It appears desirable to have separate identification of the various factors commut<sup>1</sup>, and a comments card has been provided for that purpose. The comments card has a "C" in column 1, and a comment may appear in columns 2 - 72. A comments card may be inserted between run instruction cards, and the line of comment given on the card will be printed below the title on all output thereafter, unless superseded by another comments card.

Comments output may be entirely suppressed by using another comments card containing blanks in columns 2 - 72.

#### FORMAT

All data may be entered on NAA FORTRAN Fixed 10 Decimal Data sheets. Each line represents 12 card columns with six lines per card, making a total of 72 card columns available for data entry. Columns 73 - 80 are used for card identification and/or numerical sequencing for sorting purposes.

##### Title Card

A title card is characterized by an alphabetical "T" placed in column 1. Columns 2 - 72 available for job identification, as shown on Figure 9.

##### Comments Card

A comments card is characterized by an alphabetical "C" placed in column 1. Columns 2 - 72 are available for run comments, as shown on Figure 9.

##### Surface and Transformation Data

All surface and transformation data is preceded by a name card uniquely identifying the data. A name consists of six FORTRAN characters (a computer "word") and always occupies the first six columns of the name card. The data

FORTRAN FIXED 10 DIGIT DECIMAL DATA			
DECK NO.	JOINT	PROGRAMMER'S I & TOPS	DATE 8/1/51 PAGE 1 OF 1 JOB NO.
1	2	3	4
5	6	7	8
9	10	11	12
13	14	15	16
17	18	19	20
21	22	23	24
25	26	27	28
29	30	31	32
33	34	35	36
37	38	39	40
41	42	43	44
45	46	47	48
49	50	51	52
53	54	55	56
57	58	59	60
61	62	63	64
65	66	67	68
69	70	71	72
73	74	75	76
77	78	79	80
81	82	83	84
85	86	87	88
89	90	91	92
93	94	95	96
97	98	99	100
101	102	103	104
105	106	107	108
109	110	111	112
113	114	115	116
117	118	119	120
121	122	123	124
125	126	127	128
129	130	131	132
133	134	135	136
137	138	139	140
141	142	143	144
145	146	147	148
149	150	151	152
153	154	155	156
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217	218	219	220
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237	238	239	240
241	242	243	244
245	246	247	248
249	250	251	252
253	254	255	256
257	258	259	260
261	262	263	264
265	266	267	268
269	270	271	272
273	274	275	276
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525	526	527	528
529	530	531	532
533	534	535	536
537	538	539	540
541	542	543	544
545	546	547	548
549	550	551	552
553	554	555	556
557	558	559	560
561	562	563	564
565	566	567	568
569	570	571	572
573	574	575	576
577	578	579	580
581	582	583	584
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617	618	619	620
621	622	623	624
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685	686	687	688
689	690	691	692
693	694	695	696
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705	706	707	708
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713	714	715	716
717	718	719	720
721	722	723	724
725	726	727	728
729	730	731	732
733	734	735	736
737	738	739	740
741	742	743	744
745	746	747	748
749	750	751	752
753	754	755	756
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765	766	767	768
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785	786	787	788
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797	798	799	800
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805	806	807	808
809	810	811	812
813	814	815	816
817	818	819	820
821	822	823	824
825	826	827	828
829	830	831	832
833	834	835	836
837	838	839	840
841	842	843	844
845	846	847	848
849	850	851	852
853	854	855	856
857	858	859	860
861	862	863	864
865	866	867	868
869	870	871	872
873	874	875	876
877	878	879	880
881	882	883	884
885	886	887	888
889	890	891	892
893	894	895	896
897	898	899	900
901	902	903	904
905	906	907	908
909	910	911	912
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921	922	923	924
925	926	927	928
929	930	931	932
933	934	935	936
937	938	939	940
941	942	943	944
945	946	947	948
949	950	951	952
953	954	955	956
957	958	959	960
961	962	963	964
965	966	967	968
969	970	971	972
973	974	975	976
977	978	979	980
981	982	983	984
985	986	987	988
989	990	991	992
993	994	995	996
997	998	999	1000

FIGURE 9. "T" and "C" Control Card Format

class, an integer from 1 to 9, must always be placed in column 1. The remainder of the name occupies columns 2 - 6, and it is important to note that a blank space is considered a character and a part of the name. For example, the name 1S1 is not the same as 1\_S1 or 1\_\_S1.

The next word on the name card, columns 7 - 12 must be left blank. The remainder of the name card, (columns 13 - 72) may be left blank or contents written to further identify the data, and will be printed out along with the name of the surface as part of the "Input Data" print out.

The data identified by the name card must follow the name card. There are seven different formats which must be adhered to in entering data.

#### Class 1 and 2

The number of points to be entered describing the surface appears on the first line, Figure 10, followed by the X, Y, and Z coordinates of each point in sequence. The order in which the points are selected in the surface is explained in detail in Section IV.

#### Class 3

The number of sides are entered on the first line, followed by the X, Y, and Z coordinates of the center of the internally generated polygon, the X-axis radius and the Y-axis radius as shown in Figure 11.

#### Class 4

The total number of points describing the surface are entered on the first line as shown in Figure 12. The X, Y, and Z coordinates of the first point follow on the next three lines. The fourth line, representing 12 columns, is divided into four equal parts of 3 columns each. Each point in the surface connecting to point 1 is entered, up to a maximum of four. The pattern is repeated for the remaining points describing the surfaces.

#### Class 6

The numbers of surface cross section boundary divisions (sides) is given on the first line as shown in Figure 13. The number of cross sections desired is specified on the second line, followed by the X, Y, and Z coordinates of the base (1st) cross section. The X-axis radius of the base cross section is given on the last line of the first card. The Y-axis radius is entered on the first line of the second card, followed by, if more than one cross section is specified, the following, repeated for each cross section. The height (Z-coordinate) of the cross section above the XY plane, the X-axis radius and the Y-axis.

**FORTRAN FIXED 10 DIGIT DECIMAL DATA**

DECK NO.	FORM	PROGRAMMER	DATE	NAME	JOB NO.
1	1	1	1	1	1
2	2	2	2	2	2
3	3	3	3	3	3
4	4	4	4	4	4
5	5	5	5	5	5
6	6	6	6	6	6
7	7	7	7	7	7
8	8	8	8	8	8
9	9	9	9	9	9
10	10	10	10	10	10
11	11	11	11	11	11
12	12	12	12	12	12
13	13	13	13	13	13
14	14	14	14	14	14
15	15	15	15	15	15
16	16	16	16	16	16
17	17	17	17	17	17
18	18	18	18	18	18
19	19	19	19	19	19
20	20	20	20	20	20
21	21	21	21	21	21
22	22	22	22	22	22
23	23	23	23	23	23
24	24	24	24	24	24
25	25	25	25	25	25
26	26	26	26	26	26
27	27	27	27	27	27
28	28	28	28	28	28
29	29	29	29	29	29
30	30	30	30	30	30
31	31	31	31	31	31
32	32	32	32	32	32
33	33	33	33	33	33
34	34	34	34	34	34
35	35	35	35	35	35
36	36	36	36	36	36
37	37	37	37	37	37
38	38	38	38	38	38
39	39	39	39	39	39
40	40	40	40	40	40
41	41	41	41	41	41
42	42	42	42	42	42
43	43	43	43	43	43
44	44	44	44	44	44
45	45	45	45	45	45
46	46	46	46	46	46
47	47	47	47	47	47
48	48	48	48	48	48
49	49	49	49	49	49
50	50	50	50	50	50
51	51	51	51	51	51
52	52	52	52	52	52
53	53	53	53	53	53
54	54	54	54	54	54
55	55	55	55	55	55
56	56	56	56	56	56
57	57	57	57	57	57
58	58	58	58	58	58
59	59	59	59	59	59
60	60	60	60	60	60
61	61	61	61	61	61
62	62	62	62	62	62
63	63	63	63	63	63
64	64	64	64	64	64
65	65	65	65	65	65
66	66	66	66	66	66
67	67	67	67	67	67
68	68	68	68	68	68
69	69	69	69	69	69
70	70	70	70	70	70
71	71	71	71	71	71
72	72	72	72	72	72
73	73	73	73	73	73
74	74	74	74	74	74
75	75	75	75	75	75
76	76	76	76	76	76
77	77	77	77	77	77
78	78	78	78	78	78
79	79	79	79	79	79
80	80	80	80	80	80
81	81	81	81	81	81
82	82	82	82	82	82
83	83	83	83	83	83
84	84	84	84	84	84
85	85	85	85	85	85
86	86	86	86	86	86
87	87	87	87	87	87
88	88	88	88	88	88
89	89	89	89	89	89
90	90	90	90	90	90
91	91	91	91	91	91
92	92	92	92	92	92
93	93	93	93	93	93
94	94	94	94	94	94
95	95	95	95	95	95
96	96	96	96	96	96
97	97	97	97	97	97
98	98	98	98	98	98
99	99	99	99	99	99
100	100	100	100	100	100

NOTE: 1) ALL DATA MUST BE ENTERED IN DECIMAL POINTS.  
 2) DATA MUST BE ENTERED IN DECIMAL POINTS.  
 3) DATA MUST BE ENTERED IN DECIMAL POINTS.

FIGURE 10. Class 1 and 2 Surface Input Data Format

FORTRAN F'XSD 10 DIGIT DECIMAL DATA				
DECK NO.	FORMAT	PROGRAMMER	DATE	JOB NO.
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1	F X S D I	NAME OF CLASS 3 SURFACE CODE 1-4		
2		USE "1" TO CODE 1 TO CREATE AS		
3		INTERNALLY GENERATED PLANE NUMBER		
4		NUMBER OF CODE "1" IS PLANE NO. 1-10		
5		THE CODE "1" IS PLANE NO. 1-10		
6		USE CODE "1" TO CODE TO USE CODE		
7		NO. OF ACTION STOPS = 1		
8		COORDINATES OF CENTER		
9		1 = AFTER EASTING		
10		2 = AFTER EASTING		
11				
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FIGURE 11. Class 3 Surface Specifications Input Data Format

**FORTTRAN FIXED 10 DIGIT DECIMAL DATA**

DECK NO. 10001 PROGRAMMER E. A. TOOP DATE 4/11/53 PAGE 1 OF 1 JOB NO.         

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	1	NAME OF CLASS 4 OF 5 SURFACE, CODE 1 - 6	
2	2	CLASS 4 - PLATE NUMBER, USE "X" IN COL. 1	
3	3	CLASS 5 - ROUTE OR LOCATION OF WELD, DIV. 1 OR 2	
4	4	WELDMENT CODE, WILL BE REAPPLIED	
5	5	THE CODE IS TO BE REAPPLIED TO THE WELDMENT	
6	6	USE COLS 7-10 FOR CARD 19, ALL CARDS	
7	7	NO. OF POINTS SURFACE 4 SURFACE	
8	8	COORDINATES OF FIRST SURFACE POINT	
9	9	COORDINATES OF SECOND SURFACE POINT	
10	10	COORDINATES OF THIRD SURFACE POINT	
11	11	COORDINATES OF FOURTH SURFACE POINT	
12	12	COORDINATES OF FIFTH SURFACE POINT	
13	13	COORDINATES OF SIXTH SURFACE POINT	
14	14	COORDINATES OF SEVENTH SURFACE POINT	
15	15	COORDINATES OF EIGHTH SURFACE POINT	
16	16	COORDINATES OF NINTH SURFACE POINT	
17	17	COORDINATES OF TENTH SURFACE POINT	
18	18	COORDINATES OF ELEVENTH SURFACE POINT	
19	19	COORDINATES OF TWELFTH SURFACE POINT	
20	20	COORDINATES OF THIRTEENTH SURFACE POINT	
21	21	COORDINATES OF FOURTEENTH SURFACE POINT	
22	22	COORDINATES OF FIFTEENTH SURFACE POINT	
23	23	COORDINATES OF SIXTEENTH SURFACE POINT	
24	24	COORDINATES OF SEVENTEENTH SURFACE POINT	
25	25	COORDINATES OF EIGHTEENTH SURFACE POINT	
26	26	COORDINATES OF NINETEENTH SURFACE POINT	
27	27	COORDINATES OF TWENTIETH SURFACE POINT	
28	28	COORDINATES OF TWENTY-FIRST SURFACE POINT	
29	29	COORDINATES OF TWENTY-SECOND SURFACE POINT	
30	30	COORDINATES OF TWENTY-THIRD SURFACE POINT	
31	31	COORDINATES OF TWENTY-FOURTH SURFACE POINT	
32	32	COORDINATES OF TWENTY-FIFTH SURFACE POINT	
33	33	COORDINATES OF TWENTY-SIXTH SURFACE POINT	
34	34	COORDINATES OF TWENTY-SEVENTH SURFACE POINT	
35	35	COORDINATES OF TWENTY-EIGHTH SURFACE POINT	
36	36	COORDINATES OF TWENTY-NINTH SURFACE POINT	
37	37	COORDINATES OF THIRTIETH SURFACE POINT	
38	38	COORDINATES OF THIRTY-FIRST SURFACE POINT	
39	39	COORDINATES OF THIRTY-SECOND SURFACE POINT	
40	40	COORDINATES OF THIRTY-THIRD SURFACE POINT	
41	41	COORDINATES OF THIRTY-FOURTH SURFACE POINT	
42	42	COORDINATES OF THIRTY-FIFTH SURFACE POINT	
43	43	COORDINATES OF THIRTY-SIXTH SURFACE POINT	
44	44	COORDINATES OF THIRTY-SEVENTH SURFACE POINT	
45	45	COORDINATES OF THIRTY-EIGHTH SURFACE POINT	
46	46	COORDINATES OF THIRTY-NINTH SURFACE POINT	
47	47	COORDINATES OF FORTY SURFACE POINT	
48	48	COORDINATES OF FORTY-FIRST SURFACE POINT	
49	49	COORDINATES OF FORTY-SECOND SURFACE POINT	
50	50	COORDINATES OF FORTY-THIRD SURFACE POINT	
51	51	COORDINATES OF FORTY-FOURTH SURFACE POINT	
52	52	COORDINATES OF FORTY-FIFTH SURFACE POINT	
53	53	COORDINATES OF FORTY-SIXTH SURFACE POINT	
54	54	COORDINATES OF FORTY-SEVENTH SURFACE POINT	
55	55	COORDINATES OF FORTY-EIGHTH SURFACE POINT	
56	56	COORDINATES OF FORTY-NINTH SURFACE POINT	
57	57	COORDINATES OF FIFTY SURFACE POINT	
58	58	COORDINATES OF FIFTY-FIRST SURFACE POINT	
59	59	COORDINATES OF FIFTY-SECOND SURFACE POINT	
60	60	COORDINATES OF FIFTY-THIRD SURFACE POINT	
61	61	COORDINATES OF FIFTY-FOURTH SURFACE POINT	
62	62	COORDINATES OF FIFTY-FIFTH SURFACE POINT	
63	63	COORDINATES OF FIFTY-SIXTH SURFACE POINT	
64	64	COORDINATES OF FIFTY-SEVENTH SURFACE POINT	
65	65	COORDINATES OF FIFTY-EIGHTH SURFACE POINT	
66	66	COORDINATES OF FIFTY-NINTH SURFACE POINT	
67	67	COORDINATES OF SIXTY SURFACE POINT	
68	68	COORDINATES OF SIXTY-FIRST SURFACE POINT	
69	69	COORDINATES OF SIXTY-SECOND SURFACE POINT	
70	70	COORDINATES OF SIXTY-THIRD SURFACE POINT	
71	71	COORDINATES OF SIXTY-FOURTH SURFACE POINT	
72	72	COORDINATES OF SIXTY-FIFTH SURFACE POINT	
73	73	COORDINATES OF SIXTY-SIXTH SURFACE POINT	
74	74	COORDINATES OF SIXTY-SEVENTH SURFACE POINT	
75	75	COORDINATES OF SIXTY-EIGHTH SURFACE POINT	
76	76	COORDINATES OF SIXTY-NINTH SURFACE POINT	
77	77	COORDINATES OF SEVENTY SURFACE POINT	
78	78	COORDINATES OF SEVENTY-FIRST SURFACE POINT	
79	79	COORDINATES OF SEVENTY-SECOND SURFACE POINT	
80	80	COORDINATES OF SEVENTY-THIRD SURFACE POINT	
81	81	COORDINATES OF SEVENTY-FOURTH SURFACE POINT	
82	82	COORDINATES OF SEVENTY-FIFTH SURFACE POINT	
83	83	COORDINATES OF SEVENTY-SIXTH SURFACE POINT	
84	84	COORDINATES OF SEVENTY-SEVENTH SURFACE POINT	
85	85	COORDINATES OF SEVENTY-EIGHTH SURFACE POINT	
86	86	COORDINATES OF SEVENTY-NINTH SURFACE POINT	
87	87	COORDINATES OF EIGHTY SURFACE POINT	
88	88	COORDINATES OF EIGHTY-FIRST SURFACE POINT	
89	89	COORDINATES OF EIGHTY-SECOND SURFACE POINT	
90	90	COORDINATES OF EIGHTY-THIRD SURFACE POINT	
91	91	COORDINATES OF EIGHTY-FOURTH SURFACE POINT	
92	92	COORDINATES OF EIGHTY-FIFTH SURFACE POINT	
93	93	COORDINATES OF EIGHTY-SIXTH SURFACE POINT	
94	94	COORDINATES OF EIGHTY-SEVENTH SURFACE POINT	
95	95	COORDINATES OF EIGHTY-EIGHTH SURFACE POINT	
96	96	COORDINATES OF EIGHTY-NINTH SURFACE POINT	
97	97	COORDINATES OF NINETY SURFACE POINT	
98	98	COORDINATES OF NINETY-FIRST SURFACE POINT	
99	99	COORDINATES OF NINETY-SECOND SURFACE POINT	
100	100	COORDINATES OF NINETY-THIRD SURFACE POINT	
101	101	COORDINATES OF NINETY-FOURTH SURFACE POINT	
102	102	COORDINATES OF NINETY-FIFTH SURFACE POINT	
103	103	COORDINATES OF NINETY-SIXTH SURFACE POINT	
104	104	COORDINATES OF NINETY-SEVENTH SURFACE POINT	
105	105	COORDINATES OF NINETY-EIGHTH SURFACE POINT	
106	106	COORDINATES OF NINETY-NINTH SURFACE POINT	
107	107	COORDINATES OF ONE HUNDRED SURFACE POINT	
108	108	COORDINATES OF ONE HUNDRED AND ONE SURFACE POINT	
109	109	COORDINATES OF ONE HUNDRED AND TWO SURFACE POINT	
110	110	COORDINATES OF ONE HUNDRED AND THREE SURFACE POINT	
111	111	COORDINATES OF ONE HUNDRED AND FOUR SURFACE POINT	
112	112	COORDINATES OF ONE HUNDRED AND FIVE SURFACE POINT	
113	113	COORDINATES OF ONE HUNDRED AND SIX SURFACE POINT	
114	114	COORDINATES OF ONE HUNDRED AND SEVEN SURFACE POINT	
115	115	COORDINATES OF ONE HUNDRED AND EIGHT SURFACE POINT	
116	116	COORDINATES OF ONE HUNDRED AND NINE SURFACE POINT	
117	117	COORDINATES OF ONE HUNDRED AND TEN SURFACE POINT	
118	118	COORDINATES OF ONE HUNDRED AND ELEVEN SURFACE POINT	
119	119	COORDINATES OF ONE HUNDRED AND TWELVE SURFACE POINT	
120	120	COORDINATES OF ONE HUNDRED AND THIRTEEN SURFACE POINT	
121	121	COORDINATES OF ONE HUNDRED AND FOURTEEN SURFACE POINT	
122	122	COORDINATES OF ONE HUNDRED AND FIFTEEN SURFACE POINT	
123	123	COORDINATES OF ONE HUNDRED AND SIXTEEN SURFACE POINT	
124	124	COORDINATES OF ONE HUNDRED AND SEVENTEEN SURFACE POINT	
125	125	COORDINATES OF ONE HUNDRED AND EIGHTEEN SURFACE POINT	
126	126	COORDINATES OF ONE HUNDRED AND NINETEEN SURFACE POINT	
127	127	COORDINATES OF ONE HUNDRED AND TWENTY SURFACE POINT	
128	128	COORDINATES OF ONE HUNDRED AND TWENTY-ONE SURFACE POINT	
129	129	COORDINATES OF ONE HUNDRED AND TWENTY-TWO SURFACE POINT	
130	130	COORDINATES OF ONE HUNDRED AND TWENTY-THREE SURFACE POINT	
131	131	COORDINATES OF ONE HUNDRED AND TWENTY-FOUR SURFACE POINT	
132	132	COORDINATES OF ONE HUNDRED AND TWENTY-FIVE SURFACE POINT	
133	133	COORDINATES OF ONE HUNDRED AND TWENTY-SIX SURFACE POINT	
134	134	COORDINATES OF ONE HUNDRED AND TWENTY-SEVEN SURFACE POINT	
135	135	COORDINATES OF ONE HUNDRED AND TWENTY-EIGHT SURFACE POINT	
136	136	COORDINATES OF ONE HUNDRED AND TWENTY-NINE SURFACE POINT	
137	137	COORDINATES OF ONE HUNDRED AND THIRTY SURFACE POINT	
138	138	COORDINATES OF ONE HUNDRED AND THIRTY-ONE SURFACE POINT	
139	139	COORDINATES OF ONE HUNDRED AND THIRTY-TWO SURFACE POINT	
140	140	COORDINATES OF ONE HUNDRED AND THIRTY-THREE SURFACE POINT	
141	141	COORDINATES OF ONE HUNDRED AND THIRTY-FOUR SURFACE POINT	
142	142	COORDINATES OF ONE HUNDRED AND THIRTY-FIVE SURFACE POINT	
143	143	COORDINATES OF ONE HUNDRED AND THIRTY-SIX SURFACE POINT	
144	144	COORDINATES OF ONE HUNDRED AND THIRTY-SEVEN SURFACE POINT	
145	145	COORDINATES OF ONE HUNDRED AND THIRTY-EIGHT SURFACE POINT	
146	146	COORDINATES OF ONE HUNDRED AND THIRTY-NINE SURFACE POINT	
147	147	COORDINATES OF ONE HUNDRED AND FORTY SURFACE POINT	
148	148	COORDINATES OF ONE HUNDRED AND FORTY-ONE SURFACE POINT	
149	149	COORDINATES OF ONE HUNDRED AND FORTY-TWO SURFACE POINT	
150	150	COORDINATES OF ONE HUNDRED AND FORTY-THREE SURFACE POINT	
151	151	COORDINATES OF ONE HUNDRED AND FORTY-FOUR SURFACE POINT	
152	152	COORDINATES OF ONE HUNDRED AND FORTY-FIVE SURFACE POINT	
153	153	COORDINATES OF ONE HUNDRED AND FORTY-SIX SURFACE POINT	
154	154	COORDINATES OF ONE HUNDRED AND FORTY-SEVEN SURFACE POINT	
155	155	COORDINATES OF ONE HUNDRED AND FORTY-EIGHT SURFACE POINT	
156	156	COORDINATES OF ONE HUNDRED AND FORTY-NINE SURFACE POINT	
157	157	COORDINATES OF ONE HUNDRED AND FIFTY SURFACE POINT	
158	158	COORDINATES OF ONE HUNDRED AND FIFTY-ONE SURFACE POINT	
159	159	COORDINATES OF ONE HUNDRED AND FIFTY-TWO SURFACE POINT	
160	160	COORDINATES OF ONE HUNDRED AND FIFTY-THREE SURFACE POINT	
161	161	COORDINATES OF ONE HUNDRED AND FIFTY-FOUR SURFACE POINT	
162	162	COORDINATES OF ONE HUNDRED AND FIFTY-FIVE SURFACE POINT	
163	163	COORDINATES OF ONE HUNDRED AND FIFTY-SIX SURFACE POINT	
164	164	COORDINATES OF ONE HUNDRED AND FIFTY-SEVEN SURFACE POINT	
165	165	COORDINATES OF ONE HUNDRED AND FIFTY-EIGHT SURFACE POINT	
166	166	COORDINATES OF ONE HUNDRED AND FIFTY-NINE SURFACE POINT	
167	167	COORDINATES OF ONE HUNDRED AND SIXTY SURFACE POINT	
168	168	COORDINATES OF ONE HUNDRED AND SIXTY-ONE SURFACE POINT	
169	169	COORDINATES OF ONE HUNDRED AND SIXTY-TWO SURFACE POINT	
170	170	COORDINATES OF ONE HUNDRED AND SIXTY-THREE SURFACE POINT	
171	171	COORDINATES OF ONE HUNDRED AND SIXTY-FOUR SURFACE POINT	
172	172	COORDINATES OF ONE HUNDRED AND SIXTY-FIVE SURFACE POINT	
173	173	COORDINATES OF ONE HUNDRED AND SIXTY-SIX SURFACE POINT	
174	174	COORDINATES OF ONE HUNDRED AND SIXTY-SEVEN SURFACE POINT	
175	175	COORDINATES OF ONE HUNDRED AND SIXTY-EIGHT SURFACE POINT	
176	176	COORDINATES OF ONE HUNDRED AND SIXTY-NINE SURFACE POINT	
177	177	COORDINATES OF ONE HUNDRED AND SEVENTY SURFACE POINT	
178	178	COORDINATES OF ONE HUNDRED AND SEVENTY-ONE SURFACE POINT	
179	179	COORDINATES OF ONE HUNDRED AND SEVENTY-TWO SURFACE POINT	
180	180	COORDINATES OF ONE HUNDRED AND SEVENTY-THREE SURFACE POINT	
181	181	COORDINATES OF ONE HUNDRED AND SEVENTY-FOUR SURFACE POINT	
182	182	COORDINATES OF ONE HUNDRED AND SEVENTY-FIVE SURFACE POINT	
183	183	COORDINATES OF ONE HUNDRED AND SEVENTY-SIX SURFACE POINT	
184	184	COORDINATES OF ONE HUNDRED AND SEVENTY-SEVEN SURFACE POINT	
185	185	COORDINATES OF ONE HUNDRED AND SEVENTY-EIGHT SURFACE POINT	
186	186	COORDINATES OF ONE HUNDRED AND SEVENTY-NINE SURFACE POINT	
187	187	COORDINATES OF ONE HUNDRED AND EIGHTY SURFACE POINT	
188	188	COORDINATES OF ONE HUNDRED AND EIGHTY-ONE SURFACE POINT	
189	189	COORDINATES OF ONE HUNDRED AND EIGHTY-TWO SURFACE POINT	
190	190	COORDINATES OF ONE HUNDRED AND EIGHTY-THREE SURFACE POINT	
191	191	COORDINATES OF ONE HUNDRED AND EIGHTY-FOUR SURFACE POINT	
192	192	COORDINATES OF ONE HUNDRED AND EIGHTY-FIVE SURFACE POINT	
193	193	COORDINATES OF ONE HUNDRED AND EIGHTY-SIX SURFACE POINT	
194	194	COORDINATES OF ONE HUNDRED AND EIGHTY-SEVEN SURFACE POINT	
195	195	COORDINATES OF ONE HUNDRED AND EIGHTY-EIGHT SURFACE POINT	
196	196	COORDINATES OF ONE HUNDRED AND EIGHTY-NINE SURFACE POINT	
197	197	COORDINATES OF ONE HUNDRED AND NINETY SURFACE POINT	
198	198	COORDINATES OF ONE HUNDRED AND NINETY-ONE SURFACE POINT	
199	199	COORDINATES OF ONE HUNDRED AND NINETY-TWO SURFACE POINT	
200	200	COORDINATES OF ONE HUNDRED AND NINETY-THREE SURFACE POINT	
201	201	COORDINATES OF ONE HUNDRED AND NINETY-FOUR SURFACE POINT	
202	202	COORDINATES OF ONE HUNDRED AND NINETY-FIVE SURFACE POINT	
203	203	COORDINATES OF ONE HUNDRED AND NINETY-SIX SURFACE POINT	
204	204	COORDINATES OF ONE HUNDRED AND NINETY-SEVEN SURFACE POINT	
205	205	COORDINATES OF ONE HUNDRED AND NINETY-EIGHT SURFACE POINT	
206	206	COORDINATES OF ONE HUNDRED AND NINETY-NINE SURFACE POINT	
207	207	COORDINATES OF TWO HUNDRED SURFACE POINT	
208	208	COORDINATES OF TWO HUNDRED AND ONE SURFACE POINT	
209	209	COORDINATES OF TWO HUNDRED AND TWO SURFACE POINT	
210	210	COORDINATES OF TWO HUNDRED AND THREE SURFACE POINT	
211	211	COORDINATES OF TWO HUNDRED AND FOUR SURFACE POINT	
212	212	COORDINATES OF TWO HUNDRED AND FIVE SURFACE POINT	
213	213	COORDINATES OF TWO HUNDRED AND SIX SURFACE POINT	
214	214	COORDINATES OF TWO HUNDRED AND SEVEN SURFACE POINT	
215	215	COORDINATES OF TWO HUNDRED AND EIGHT SURFACE POINT	
216	216	COORDINATES OF TWO HUNDRED AND NINE SURFACE POINT	
217	217	COORDINATES OF TWO HUNDRED AND TEN SURFACE POINT	
218	218	COORDINATES OF TWO HUNDRED AND ELEVEN SURFACE POINT	
219	219	COORDINATES OF TWO HUNDRED AND TWELVE SURFACE POINT	
220	220	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
221	221	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
222	222	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
223	223	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
224	224	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
225	225	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
226	226	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
227	227	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
228	228	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
229	229	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
230	230	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
231	231	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
232	232	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
233	233	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
234	234	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
235	235	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
236	236	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
237	237	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
238	238	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
239	239	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
240	240	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
241	241	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
242	242	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
243	243	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
244	244	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
245	245	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
246	246	COORDINATES OF TWO HUNDRED AND THIRTEEN SURFACE POINT	
247	2		

**FORTRAN    FIXED 10 DIGIT DECIMAL DATA**

[illegible]

FIGURE 13. Class 6 Surface Specifications Input Data Format

#### Class 7

The sphere radius is entered on the first line, followed by the X, Y, and Z coordinates locating the center of the sphere as shown in Figure 14.

#### Class 8

The names of the surface (s) which are to be entered under this class are entered together on one card, without regard to order as shown in Figure 15. The card is usually divided into 12 words of six columns each. Each name to be entered must appear identically in a word-space as it appears in the word-space on the data name card.

#### Class 9

The first point to be transformed is entered on the first line, followed by the X, Y and Z coordinates of the "new" position of the point as shown in Figure 16. The second point to be transformed immediately follows on the fifth line followed by the X-coordinate of the new position of the second point, thus completing the first card. The Y and Z coordinates of the new position of the second point are entered on the first two lines of the second card, followed by the number of the third point to be transformed and its new X, Y, and Z coordinates.

All of the numbers entered in the above data may be entered as fixed or floating point numbers except connections data, which must be entered as decimal integers. If a decimal point is given (fractional numbers must have decimal points given), the floating number may be located anywhere in the field (line); if no decimal point is given, the number must be located to the extreme right of the field (no blanks to the right of the number).

#### Run Instructions

Six FORTRAN words comprise a set of run instructions; two sets may be entered on one card as shown in Figure 17. The first set starts at column 1 and the second set starts at column 37. Two words (12 columns) comprise one line on the data sheet. The name of the Surface 1 data is entered in the first word (columns 1 - 6) precisely as it appears in the first word of the surface data name card. The name of the Surface 2 data is entered in the second word (columns 8 - 12) precisely as it appears in the first word of the surface data name card. If a primary transformation of Surface 1 is desired, the desired transformation data name is entered in columns 13 - 18, otherwise, it is left blank. If a primary transformation of Surface 2 is desired, the name of the transformation data is entered in the fourth word, columns 19 - 24. If a detailed output is desired, the alphabetical character "D" is entered in column 27, or in column 31. If the "D" appears in either or both locations, a detailed output will result; if a blank is in both locations, a standard output will result. The horizontal naming division "integer" appears in column 30, unless the integer 10 or 11 is used, in which case columns 29 and 30 are utilized. The vertical naming division "integer" appears in column 36, un-



FORTRAN FIXED 10 DIGIT DECIMAL DATA			
DECK NO.	PROGRAM	DATE	PAGE
NO. 1	NO. 1	NO. 1	NO. 1
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	1	1	1
2	2	2	2
3	3	3	3
4	4	4	4
5	5	5	5
6	6	6	6
7	7	7	7
8	8	8	8
9	9	9	9
10	10	10	10
11	11	11	11
12	12	12	12
13	13	13	13
14	14	14	14
15	15	15	15
16	16	16	16
17	17	17	17
18	18	18	18
19	19	19	19
20	20	20	20
21	21	21	21
22	22	22	22
23	23	23	23
24	24	24	24
25	25	25	25
26	26	26	26
27	27	27	27
28	28	28	28
29	29	29	29
30	30	30	30
31	31	31	31
32	32	32	32
33	33	33	33
34	34	34	34
35	35	35	35
36	36	36	36
37	37	37	37
38	38	38	38
39	39	39	39
40	40	40	40
41	41	41	41
42	42	42	42
43	43	43	43
44	44	44	44
45	45	45	45
46	46	46	46
47	47	47	47
48	48	48	48
49	49	49	49
50	50	50	50
51	51	51	51
52	52	52	52
53	53	53	53
54	54	54	54
55	55	55	55
56	56	56	56
57	57	57	57
58	58	58	58
59	59	59	59
60	60	60	60
61	61	61	61
62	62	62	62
63	63	63	63
64	64	64	64
65	65	65	65
66	66	66	66
67	67	67	67
68	68	68	68
69	69	69	69
70	70	70	70
71	71	71	71
72	72	72	72
73	73	73	73
74	74	74	74
75	75	75	75
76	76	76	76
77	77	77	77
78	78	78	78
79	79	79	79
80	80	80	80
81	81	81	81
82	82	82	82
83	83	83	83
84	84	84	84
85	85	85	85
86	86	86	86
87	87	87	87
88	88	88	88
89	89	89	89
90	90	90	90
91	91	91	91
92	92	92	92
93	93	93	93
94	94	94	94
95	95	95	95
96	96	96	96
97	97	97	97
98	98	98	98
99	99	99	99
100	100	100	100

FIGURE 14. Class 7 Sphere Specification Input Data Format

**FORTRAN FIXED 10 DIGIT DECIMAL DATA**

DECK NO. 00001 PROGRAMMER E. J. Topp DATE 12/11/52 PAGE 1 OF 1 JOB NO.         

NUMBER	IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
1	1	1
2	2	2
3	3	3
4	4	4
5	5	5
6	6	6
7	7	7
8	8	8
9	9	9
10	10	10
11	11	11
12	12	12
13	13	13
14	14	14
15	15	15
16	16	16
17	17	17
18	18	18
19	19	19
20	20	20
21	21	21
22	22	22
23	23	23
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25	25	25
26	26	26
27	27	27
28	28	28
29	29	29
30	30	30
31	31	31
32	32	32
33	33	33
34	34	34
35	35	35
36	36	36
37	37	37
38	38	38
39	39	39
40	40	40
41	41	41
42	42	42
43	43	43
44	44	44
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63	63	63
64	64	64
65	65	65
66	66	66
67	67	67
68	68	68
69	69	69
70	70	70
71	71	71
72	72	72
73	73	73
74	74	74
75	75	75
76	76	76
77	77	77
78	78	78
79	79	79
80	80	80
81	81	81
82	82	82
83	83	83
84	84	84
85	85	85
86	86	86
87	87	87
88	88	88
89	89	89
90	90	90
91	91	91
92	92	92
93	93	93
94	94	94
95	95	95
96	96	96
97	97	97
98	98	98
99	99	99
100	100	100

FIGURE 15. Class 8 Multisurface Specifications Input Data Format

FORTRAN FIXED 10 DIGIT DECIMAL DATA			
FORM NO. 10011	PROGRAMMER J. E. TERRY	DATE 12/1/53	PAGE 1 OF 1
JOE NO.			
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	1	TYPE OF CLASS 9 DATA CODE A - 6	
2	2	EXP. NO. BY A. I. 3 FOR TRANSFORMATION	
3	3	DATA	
4	4	IS POINTS CODE 7-32 MUST BE MARKED	
5	5	EXP. CODE 12-31 FOR AMPLITUDE RESPONSE	
6	6	EXP. CODE 12-31 FOR AMPLITUDE RESPONSE	
7	7	FIRST POINT TO BE TRANSFORMED	
8	8	COORDINATES OF FIRST POINT FROM	
9	9	FROM POINT	
10	10	SECOND POINT TO BE TRANSFORMED	
11	11	COORDINATES OF SECOND POINT FROM REV. OF 10	
12	12	FROM POINT, etc.	
13	13	COORDINATES, etc.	
14	14	EXP. 12-31 DATA POINT FOR INITIAL POINT IN SET	
15	15	INITIAL POINT MAY BE OBTAINED BY EXP. 12-31	
16	16	TYPE OF POINT	
17	17	DATA POINT AS OBTAINED FROM A POINT-MARKED	
18	18	AMPLITUDE COORDINATE SYSTEM	

FIGURE 16. Class 9 Transformation Data Input Data Format

**FORTTRAN FIXED 10 DIGIT DECIMAL DATA**

DECK NO.	FOUNT	PROGRAMMER	DATE	CLASS	PAGE	OF	TOTAL
1	1	1	1	1	1	1	1
2	2	2	2	2	2	2	2
3	3	3	3	3	3	3	3
4	4	4	4	4	4	4	4
5	5	5	5	5	5	5	5
6	6	6	6	6	6	6	6
7	7	7	7	7	7	7	7
8	8	8	8	8	8	8	8
9	9	9	9	9	9	9	9
10	10	10	10	10	10	10	10
11	11	11	11	11	11	11	11
12	12	12	12	12	12	12	12
13	13	13	13	13	13	13	13
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16	16	16	16	16	16	16	16
17	17	17	17	17	17	17	17
18	18	18	18	18	18	18	18
19	19	19	19	19	19	19	19
20	20	20	20	20	20	20	20
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22	22	22	22	22	22	22	22
23	23	23	23	23	23	23	23
24	24	24	24	24	24	24	24
25	25	25	25	25	25	25	25
26	26	26	26	26	26	26	26
27	27	27	27	27	27	27	27
28	28	28	28	28	28	28	28
29	29	29	29	29	29	29	29
30	30	30	30	30	30	30	30
31	31	31	31	31	31	31	31
32	32	32	32	32	32	32	32
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34	34	34	34	34	34	34	34
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36	36	36	36	36	36	36	36
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42	42	42	42	42	42	42	42
43	43	43	43	43	43	43	43
44	44	44	44	44	44	44	44
45	45	45	45	45	45	45	45
46	46	46	46	46	46	46	46
47	47	47	47	47	47	47	47
48	48	48	48	48	48	48	48
49	49	49	49	49	49	49	49
50	50	50	50	50	50	50	50
51	51	51	51	51	51	51	51
52	52	52	52	52	52	52	52
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54	54	54	54	54	54	54	54
55	55	55	55	55	55	55	55
56	56	56	56	56	56	56	56
57	57	57	57	57	57	57	57
58	58	58	58	58	58	58	58
59	59	59	59	59	59	59	59
60	60	60	60	60	60	60	60
61	61	61	61	61	61	61	61
62	62	62	62	62	62	62	62
63	63	63	63	63	63	63	63
64	64	64	64	64	64	64	64
65	65	65	65	65	65	65	65
66	66	66	66	66	66	66	66
67	67	67	67	67	67	67	67
68	68	68	68	68	68	68	68
69	69	69	69	69	69	69	69
70	70	70	70	70	70	70	70
71	71	71	71	71	71	71	71
72	72	72	72	72	72	72	72
73	73	73	73	73	73	73	73
74	74	74	74	74	74	74	74
75	75	75	75	75	75	75	75
76	76	76	76	76	76	76	76
77	77	77	77	77	77	77	77
78	78	78	78	78	78	78	78
79	79	79	79	79	79	79	79
80	80	80	80	80	80	80	80
81	81	81	81	81	81	81	81
82	82	82	82	82	82	82	82
83	83	83	83	83	83	83	83
84	84	84	84	84	84	84	84
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86	86	86	86	86	86	86	86
87	87	87	87	87	87	87	87
88	88	88	88	88	88	88	88
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90	90	90	90	90	90	90	90
91	91	91	91	91	91	91	91
92	92	92	92	92	92	92	92
93	93	93	93	93	93	93	93
94	94	94	94	94	94	94	94
95	95	95	95	95	95	95	95
96	96	96	96	96	96	96	96
97	97	97	97	97	97	97	97
98	98	98	98	98	98	98	98
99	99	99	99	99	99	99	99
100	100	100	100	100	100	100	100

FIGURE 17. Run Instructions Input Data Format

less the integer 10 or 11 is used, in which case columns 35 and 36 are utilized. If columns 29 and 30 are both blank, a standard integer 4 meaning 24 horizontal divisions of each naming line is used. If 35 and 36 are both blank, a standard vertical division of 24 will be used. The above format is repeated in the same manner, starting from column 37 on the fourth line, for the second set of run instructions on the card. There is no numerical limit to the number of run instructions which may be entered. The only requirement is, of course, that the data called for has been loaded in under the names used.

## SECTION V

### PROGRAM OUTPUT

Input data is processed and printed out prior to its use in factor computations for programmer verification. The orientation vector head end is also printed out for all plane surfaces, so that the "active" side used by the program is clearly shown. Class 3 and 6 specifications as read in are printed, along with the surface data generated by the specifications.

A standard "minimum" output is given when the code letter "D" does not appear in the run instructions, consisting of the following:

1. Run number
2. Run instructions
3. The computed form factor
4. The Surface 1 mapping area
5. The exchange coefficient ( $fA$  product)
6. The total area of Surface 1
7. If Surface 1 is bisected, the area seen by Surface 2
8. The total area of Surface 2, if Surface 2 area can be computed
9. If Surface 2 is bisected, the area seen by Surface 1, if that area can be computed
10. The time in seconds spent in Subroutine SHIFAC, if utilized

If a detailed output is requested, the minimum output plus the following is printed:

1. The final coordinates of Surface 1 and Surface 2 prior to computation of configuration factors.
2. The X-Left and X-Right coordinates for each Y division of Surface 1 mapping, including horizontal and vertical divisions used.
3. Each configuration factor computed. The output is given in groups of factors easily identified because the last factor in a group occupies a line by itself. Each group contains the configuration factors computed on a mapping line. The first factor in the group is that computed at Y-left and the last factor in the group is that

computed at X-right. The first group represents the first mapping line, the second group the second mapping line, etc.

4. If the silhouette generator was used, the silhouette computed for points selected on each mapping line is printed out. The first numeral given is the mapping line, the second is the point on the mapping line, moving from X-left to X-right. The numbers following represent the silhouette.

## SECTION VI

### REFERENCES

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3. Moon, Parry. The Scientific Basis of Illuminating Engineering. New York: Dover Publications, Inc., (1961), pp. 312-318.
4. O'Brien, F. F. "Pictiel's Globoscone for Lighting Design;" Illuminating Engineering, Vol. LVIII, No. 3 (3 March 1963).
5. Towns, Kempton A. A General Computer Program for the Determination of Radiant-Interchange Configuration Factors. NAA S&ID, SID 62-393, ASD Technical Note ASD-TN-61-101 (ASTIA No. 403027), (March 1963).



## APPENDIX A

### SAMPLE PROBLEMS

A number of sample problems have been devised to illustrate the capabilities and limitations of CONFAC II. The examples are arranged roughly in order of complexity, beginning with simple plane surfaces and concluding with a complicated "intervening surface" problem involving plane and solid surfaces.

The surface configurations upon which the example problems are based are shown in accompanying illustrations. Each illustration is conveniently grouped separately with the problem description pertaining to the surfaces shown in the illustration, along with the input data sheets, run instructions, program output and a short discussion.

#### SAMPLE PROBLEM GROUP A

The surfaces shown in Figure 18 are similar to the examples given in CONFAC I. The added CONFAC II capability of bisecting a nonplanar surface is demonstrated. The data sheets are shown in Figure 19 and the results are presented in Figure 20.

##### Problem 1A

In Figure 18 (A1), the factor between the floor of a rectangular room (1FLOOR) and an adjacent wall (1WALL) is computed, using standard horizontal and vertical mapping divisions (24 x 24) on Surface 1. A detailed output is requested.

Note that because no primary or auxiliary transformation occurred, the floor coordinate system is the same as the input data (unprimed) coordinate system. The first mapping line starts at the origin and extends to point 1 in 1FLOOR.

##### Problem 2A

In Figure 18 (A1), any plane surface may be used as Surface 1 providing it has been properly entered in data prior to the factor request. To demonstrate, the wall (1WALL) now acts as Surface 1, and the factor to the floor (1FLOOR) is requested.

Note that Surface 1WALL is not in the X-Y plane of its input (unprimed) coordinate system. The program, therefore, had to perform an auxiliary transformation of both surfaces to the primed system shown, prior to factor computation, to get Surface 1 in the XY plane.

##### Problem 3A

In Figure 18 (A2), the factor from the floor (1FLOOR) to two adjacent walls taken together (2WALLS) is requested. This is a valid request because the boundary data describing 2WALLS form a valid silhouette of 2WALLS from any point on 1FLOOR. The factor should be twice that to one wall alone.

##### Problem 4A

The program cannot validly compute the factor from a nonplanar surface. A Class 2 surface is assumed nonplanar. The factor from 2WALLS to 1FLOOR is requested in order to elicit the diagnostic, warning the user of this error.

The program does not test the surface, as in CONFAC I. If a nonplanar surface is erroneously entered as a Class 1 surface, it will not be rejected if used as Surface 1 - the responsibility lay with the user to insure that Surface 1 is planar.

#### Problem 5A

In Figure 18 (A3), the necessity for proper order in data entry is emphasized. The wall data are deliberately entered in a clockwise direction (IWALLR) looking at the active surface, instead of counterclockwise. Hence, the orientation vector points in the wrong direction. The factor from IFLOOR to IWALLR is requested in order to elicit the diagnostic which alerts the user to a possible error.

#### Problem 6A

In Figure 15 (A4), CONFAC II has the capability of bisecting a nonplanar (Class 2) surface. The factor from IFLOOR to 2WALLZ, is requested, with a detailed output, to demonstrate this capability.

Subroutine LOGIC bisected 2WALLZ at the XY plane, and reconstructed the surface by eliminating points 2, 3, and 4, as shown, and creating new points 2', 3', 4' and 5'. The dashed line 2' 3' divides Surface 1 (IFLOOR) into triangular parts, designated A and B. The view of the reconstructed 2WALLZ from anywhere in area B reflects a valid silhouette in the proper counterclockwise order. When reconstructed 2WALLZ is viewed from area A, the points still form a valid silhouette, but the order is reversed. This means the computed configuration factor will be to the hemispherical space not occupied by 2WALLZ, and will be negative. So, subroutine FACTOR subtracts this factor from 1.0 to yield the correct factor to 2WALLZ.

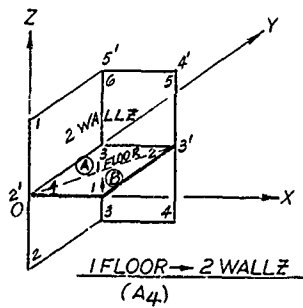
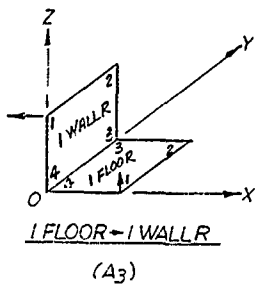
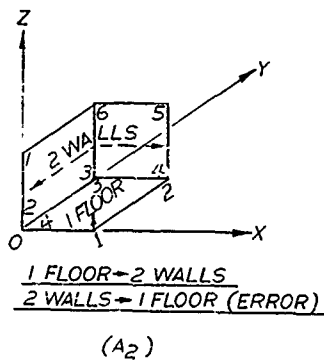
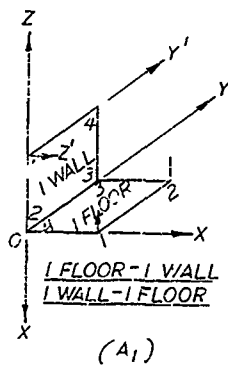


FIGURE 18. SAMPLE PROBLEMS - GROUP A

**FORTRAN FIXED 10 DIGIT DECIMAL DATA**

FORM NO. 570 PROGRAMMER E. T. 1021 DATE 11/1/53 PAGE 3 of 4 JOB NO. 2023-30

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
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3	0		
4	0		
5	0		
6	0		
7	0		
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10	0		
11	0		
12	0		
13	0		
14	0		
15	0		
16	0		
17	0		
18	0		
19	0		
20	0		
21	0		
22	0		
23	0		
24	0		
25	0		
26	0		
27	0		
28	0		
29	0		
30	0		
31	0		
32	0		
33	0		
34	0		
35	0		
36	0		
37	0		
38	0		
39	0		
40	0		
41	0		
42	0		
43	0		
44	0		
45	0		
46	0		
47	0		
48	0		
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56	0		
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58	0		
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62	0		
63	0		
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66	0		
67	0		
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69	0		
70	0		
71	0		
72	0		
73	0		
74	0		
75	0		
76	0		
77	0		
78	0		
79	0		
80	0		
81	0		
82	0		
83	0		
84	0		
85	0		
86	0		
87	0		
88	0		
89	0		
90	0		
91	0		
92	0		
93	0		
94	0		
95	0		
96	0		
97	0		
98	0		
99	0		
100	0		

**FORTRAN FIXED 10 DIGIT DECIMAL DATA**

FORM NO. 570 PROGRAMMER E. T. 1021 DATE 11/1/53 PAGE 4 of 4 JOB NO. 2023-30

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
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5	0		
6	0		
7	0		
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16	0		
17	0		
18	0		
19	0		
20	0		
21	0		
22	0		
23	0		
24	0		
25	0		
26	0		
27	0		
28	0		
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30	0		
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36	0		
37	0		
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39	0		
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63	0		
64	0		
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67	0		
68	0		
69	0		
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71	0		
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75	0		
76	0		
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78	0		
79	0		
80	0		
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98	0		
99	0		
100	0		

FIGURE 19. Group A Sample Problems Input Data Code Sheets

FORTRAN FIXED 10 DIGIT DECIMAL DATA			
DECK NO.	PROGRAMMER	DATE	PAGE 1 of 25 JOB NO. 200-30
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	0		
2	0		
3	0		
4	0		
5	0		
6	0		
7	0		
8	0		
9	0		
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99	0		
100	0		

FORTRAN FIXED 10 DIGIT DECIMAL DATA			
DECK NO.	PROGRAMMER	DATE	PAGE 2 of 25 JOB NO. 200-30
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	0		
2	0		
3	0		
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FIGURE 19. Group A Sample Problems Input Data Code Sheets  
(continued)

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE 1 of 31	JOB NO. 225-10
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1				
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FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE 2 of 31	JOB NO. 225-10
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
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FIGURE 19. Group A Sample Problems Input Data Code Sheets  
(continued)

**FORTRAN FIXED 10 DIGIT DECIMAL DATA**

DECK NO. PROGRAMMER DATE PAGE 2 OF 26 JOB NO. 2107-2

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
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**FORTRAN FIXED 10 DIGIT DECIMAL DATA**

DECK NO. PROGRAMMER DATE PAGE 3 OF 26 JOB NO. 2107-2

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
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FIGURE 19. Group A Sample Problems Input Data Code Sheets  
(continued)



NAA SPACE AND INFORMATION SYSTEMS DIVISION  
T-1 PROJECT ADJUNCT-INTERCHANGE CONFIGURATION FACILITY PROGRAM

C O N F A C I I

NAA COM-AC II REPORT SAMPLE PROBLEMS FROM FIG. 1A3--L.A.T.O.U.S. 11/1/63

I N P U T O A T A

```

***** DATA NAME= *IFLOOR * 1X1 SQUARE
POINT X Y Z POINT X Y Z
1 0.1000000E 01 0. 0.1000000E 01----(INTERNALLY GENERATED ORIENTATION VECTOR) Z
3 0. 0.1000000E 01 0. 0.1000000E 01 0. 0.1000000E 01 0. 0.1000000E 01 0.

***** DATA NAME= *SMALL * 1X1 SQUARE TOUCHING IN WALL
POINT X Y Z POINT X Y Z
1 0.1000000E 01 0. 0.1000000E 01----(INTERNALLY GENERATED ORIENTATION VECTOR) Z
3 0. 0.1000000E 01 0. 0.1000000E 01 0. 0.1000000E 01 0.1000000E 01 0.1000000E 01

***** DATA NAME= *SMALLER * SAME AS SMALL, BUT WITH DATA ENTERED CLOCKWISE
POINT X Y Z POINT X Y Z
1 0.1000000E 01 0. 0.1000000E 01----(INTERNALLY GENERATED ORIENTATION VECTOR) Z
3 0. 0.1000000E 01 0. 0.1000000E 01 0. 0.1000000E 01 0.1000000E 01 0.1000000E 01

***** DATA NAME= *SMALLS * SIDE AND BACK WALL TAKEN TOGETHER
POINT X Y Z POINT X Y Z
1 0. 0. 0.1000000E 01 0. 0.1000000E 01 0.1000000E 01 0.1000000E 01 0.
3 0.1000000E 01 0.1000000E 01 0.1000000E 01 0. 0.1000000E 01 0.1000000E 01 0.1000000E 01

```

FIGURE 20. Group A Sample Problems Program Results  
(24 pages)



# VIA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (A)-K-A-T UPS, 11/1/63

RUN NO. 1 DATA USED FOR THIS RUN= \*IFLOOR\*SMALL  
 \*D  
 \*D  
 \*

THE FORM FACTOR FROM SURFACE \*IFLOOR \* 10 SURFACE \*SMALL \* = 0.19996

THE EXCHANGE COEFFICIENT (FA)= 0.19996-00 50 UNITS

THE MAPPING AREA = 1.0000000 00 50 UNITS

THE 1/24 OF SURFACE \*IFLOOR \* = 0.1000000 01 50 UNITS.

THE AREA OF SURFACE \*SMALL \* = 0.1000000 01 50 UNITS.

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION=

\*\*\*\*\* DATA NAME= \*IFLOOR \*

POINT X Y Z POINT X Y Z  
 1 0.1000000E 01 0. 0. 0.1000000E 01 0. 0. 0.1000000E 01 0. 0. 0.  
 3 0. 0. 0.1000000E 01 0. 0. 0. 0. 0. 0. 0. 0.

\*\*\*\*\* DATA NAME= \*SMALL \*

POINT X Y Z POINT X Y Z  
 1 0.1000000E 01 0. 0. 0.1000000E 01 0. 0. 0.1000000E 01 0. 0. 0.  
 3 0. 0. 0.1000000E 01 0. 0. 0. 0. 0. 0. 0. 0.  
 COORDINATES OF POINTS ON BOUNDARY OF SURF \*IFLOOR \* FOR EACH Y INTERVAL  
 X-LEFT X-RIGHT Y X-LEFT X-RIGHT Y  
 0. 0.1000000E 01 0. 0. 0.1000000E 01 0. 0.1000000E 01 0.1000000E 01 0.1000000E 01 0.  
 0. 0.1000000E 01 0. 0.1000000E 01 0.1000000E 01 0.1000000E 01 0.1000000E 01 0.1000000E 01 0.

FIGURE 20. Group A Sample Problems Program Results  
 (continued)

0.	0.1000000E-01	0.1666667E-00	0.	0.1000000E-01	0.5893333E-00
0.	0.1000000E-01	0.2500000E-00	0.	0.1000000E-01	0.3986667E-00
0.	0.1000000E-01	0.3333333E-00	0.	0.1000000E-01	0.3750000E-00
0.	0.1000000E-01	0.4166667E-00	0.	0.1000000E-01	0.4583333E-00
0.	0.1000000E-01	0.5000000E-00	0.	0.1000000E-01	0.5416667E-00
0.	0.1000000E-01	0.5833333E-00	0.	0.1000000E-01	0.6250000E-00
0.	0.1000000E-01	0.6666667E-00	0.	0.1000000E-01	0.7083333E-00
0.	0.1000000E-01	0.7500000E-00	0.	0.1000000E-01	0.7916667E-00
0.	0.1000000E-01	0.8333333E-00	0.	0.1000000E-01	0.8750000E-00
0.	0.1000000E-01	0.9166667E-00	0.	0.1000000E-01	0.9583333E-00
0.	0.1000000E-01	0.1000000E-01	0.	0.1000000E-01	0.9583333E-00

NO. OF HORIZONTAL INCREMENTS: 24 NO. OF VERTICAL INCREMENTS: 24

THE FOLLOWING ARE PLANE ORIENT COMPRESSION FACTORS COMPUTED FOR THIS RUN  
LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

0.2500000E-00	0.238174E-00	0.2244698E-00	0.2147803E-00	0.2033431E-00	0.1921609E-00
0.1812784E-00	0.170741E-00	0.1605884E-00	0.1508443E-00	0.1412374E-00	0.1321677E-00
0.1371681E-00	0.1163181E-00	0.1068213E-00	0.1017688E-00	0.9316960E-01	0.8894905E-01
0.357342E-01	0.1773592E-01	0.7268371E-01	0.6769038E-01	0.6337979E-01	0.5952419E-01
0.5000000E-00	0.3627443E-00	0.2993818E-00	0.2647437E-00	0.2406935E-00	0.2156495E-00
0.5000000E-00	0.8750000E-00	0.1773888E-00	0.1652006E-00	0.1530019E-00	0.1433944E-00
0.1936074E-00	0.1244870E-00	0.1159889E-00	0.1068122E-00	0.9816192E-01	0.909088E-01
0.5000000E-00	0.4135154E-00	0.3469833E-00	0.3098146E-00	0.2792845E-00	0.2496071E-00
0.2276412E-00	0.2091476E-00	0.1934455E-00	0.1798108E-00	0.1682784E-00	0.1589071E-00
0.4748498E-00	0.1323835E-00	0.1291622E-00	0.1145711E-00	0.1060798E-00	0.9860433E-01
0.598712E-01	0.4930941E-01	0.7949021E-01	0.7395829E-01	0.6892252E-01	0.6427036E-01
0.5000000E-00	0.4396345E-00	0.3801883E-00	0.3358659E-00	0.3006194E-00	0.2713642E-00
0.1511731E-00	0.1396425E-00	0.1294811E-00	0.1189902E-00	0.1170340E-00	0.1051941E-00
0.956517E-01	0.8882340E-01	0.8223385E-01	0.7672328E-01	0.7137948E-01	0.6645781E-01
0.5000000E-00	0.4472467E-00	0.3900101E-00	0.3578012E-00	0.3213116E-00	0.2872934E-00
0.2447633E-00	0.2415963E-00	0.2216719E-00	0.2023584E-00	0.1827261E-00	0.1729325E-00
0.1468093E-00	0.1468093E-00	0.1355933E-00	0.1253344E-00	0.1159110E-00	0.1072811E-00
0.4739312E-01	0.4707955E-01	0.8542170E-01	0.7929282E-01	0.7366185E-01	0.6848631E-01

FIGURE 20. Group A Sample Problems Program Results  
(continued)





0.1426349E-00	0.1313825E-00	0.12-316E-00	0.1145371E-00	0.1040789E-00	0.9860414E-01
0.9169544E-01	0.851021E-01	0.7945921E-01	0.739589E-01	0.689225E-01	0.6447518E-01
0.500500E-00	0.367490E-00	0.299119E-00	0.264741E-00	0.236095E-00	0.211959E-00
0.203195E-00	0.190635E-00	0.177329E-00	0.165200E-00	0.153701E-00	0.142719E-00
0.872544E-01	0.81970E-00	0.773394E-00	0.730076E-00	0.687129E-00	0.636609E-01
0.370281E-01	0.483982E-01	0.761163E-01	0.710274E-01	0.663152E-01	0.619509E-01
0.161204E-00	0.43017E-00	0.226098E-00	0.214780E-00	0.203342E-00	0.192160E-00
0.124284E-00	0.116318E-00	0.10831E-00	0.100608E-00	0.93374E-00	0.86737E-00
0.431308E-01	0.777359E-01	0.726377E-01	0.678038E-01	0.635597E-01	0.592849E-01
0.333940E-01					

FIGURE 20. Group A Sample Problems Program Results  
(continued)

NAA CO-FAC II REPORT SAMPLE PROBLEMS FROM FIG. 1A3-K-A.TOWNS, 11/1/63

```

RUN NO. 2 DATA USED FOR THIS RUN: *WALL *FLOOR.
      *D * *
THE FORM FACTOR FROM SURFACE *WALL * TO SURFACE *FLOOR * = 0.19936
THE EXCHANGE COEFFICIENT (FA) = 0.19936E-00 SQ UNITS
      * *
THE MAPPING AREA = 1.000000E 00 SQ UNITS
THE AREA OF SURFACE *WALL * = 0.100000E 01 SQ UNITS.
THE AREA OF SURFACE *FLOOR * = 0.100000E 01 SQ UNITS.
THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

**** DATA NAME= *WALL *
POINT X Y Z PRINT X Y Z
1 -0. 0.100000E 01 0.100000E 01 0. 0.100000E 01 0.
3 0.100000E 01 0.100000E 01 0. 0.100000E 01 0.

**** DATA NAME= *FLOOR *
POINT X Y Z PRINT X Y Z
1 -0. 0.100000E 01 0.100000E 01 0. 0.100000E 01 0.
3 0.100000E 01 0.100000E 01 0. 0.100000E 01 0.

COORDINATES OF POINTS ON BOUNDARY OF SURF *WALL * FOR EACH Y INTERVAL
X-LEFT X-LEFT Y X-LEFT X-RIGHT Y
-0. 0.100000E 01 -0. 0.833333E-01 -0. 0.100000E 01 0.455667E-01
-0. 0.100000E 01 0.100000E 01 0.833333E-01 -0. 0.100000E 01 0.100000E 01

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FIGURE 20. Group A Sample Problems Program Results  
(continued)







0.318800E-00	0.344449E-00	0.375035E-00	0.403360E-00	0.436675E-00	0.467226E-00
0.308000E-00	0.325535E-00	0.342374E-00	0.359114E-00	0.375855E-00	0.392596E-00
0.298000E-00	0.316035E-00	0.332874E-00	0.349614E-00	0.366355E-00	0.383096E-00
0.288000E-00	0.306535E-00	0.323374E-00	0.340114E-00	0.356855E-00	0.373596E-00
0.278000E-00	0.297035E-00	0.313874E-00	0.330614E-00	0.347355E-00	0.364096E-00
0.268000E-00	0.287535E-00	0.304374E-00	0.321114E-00	0.337855E-00	0.354596E-00
0.258000E-00	0.278035E-00	0.294874E-00	0.311614E-00	0.328355E-00	0.345096E-00
0.248000E-00	0.268535E-00	0.285374E-00	0.302114E-00	0.318855E-00	0.335596E-00
0.238000E-00	0.259035E-00	0.275874E-00	0.292614E-00	0.309355E-00	0.326096E-00
0.228000E-00	0.249535E-00	0.266374E-00	0.283114E-00	0.299855E-00	0.316596E-00
0.218000E-00	0.240035E-00	0.256874E-00	0.273614E-00	0.290355E-00	0.307096E-00
0.208000E-00	0.230535E-00	0.247374E-00	0.264114E-00	0.280855E-00	0.297596E-00
0.198000E-00	0.221035E-00	0.237874E-00	0.254614E-00	0.271355E-00	0.288096E-00
0.188000E-00	0.211535E-00	0.228374E-00	0.245114E-00	0.261855E-00	0.278596E-00
0.178000E-00	0.202035E-00	0.218874E-00	0.235614E-00	0.252355E-00	0.269096E-00
0.168000E-00	0.192535E-00	0.209374E-00	0.226114E-00	0.242855E-00	0.259596E-00
0.158000E-00	0.183035E-00	0.199874E-00	0.216614E-00	0.233355E-00	0.250096E-00
0.148000E-00	0.173535E-00	0.190374E-00	0.207114E-00	0.223855E-00	0.240596E-00
0.138000E-00	0.164035E-00	0.180874E-00	0.197614E-00	0.214355E-00	0.231096E-00
0.128000E-00	0.154535E-00	0.171374E-00	0.188114E-00	0.204855E-00	0.221596E-00
0.118000E-00	0.145035E-00	0.161874E-00	0.178614E-00	0.195355E-00	0.212096E-00
0.108000E-00	0.135535E-00	0.152374E-00	0.169114E-00	0.185855E-00	0.202596E-00
0.098000E-00	0.126035E-00	0.142874E-00	0.159614E-00	0.176355E-00	0.193096E-00
0.088000E-00	0.116535E-00	0.133374E-00	0.150114E-00	0.166855E-00	0.183596E-00
0.078000E-00	0.107035E-00	0.123874E-00	0.140614E-00	0.157355E-00	0.174096E-00
0.068000E-00	0.097535E-00	0.114374E-00	0.131114E-00	0.147855E-00	0.164596E-00
0.058000E-00	0.088035E-00	0.104874E-00	0.121614E-00	0.138355E-00	0.155096E-00
0.048000E-00	0.078535E-00	0.095374E-00	0.112114E-00	0.128855E-00	0.145596E-00
0.038000E-00	0.069035E-00	0.085874E-00	0.102614E-00	0.119355E-00	0.136096E-00
0.028000E-00	0.059535E-00	0.076374E-00	0.093114E-00	0.109855E-00	0.126596E-00
0.018000E-00	0.050035E-00	0.066874E-00	0.083614E-00	0.100355E-00	0.117096E-00
0.008000E-00	0.040535E-00	0.057374E-00	0.074114E-00	0.090855E-00	0.107596E-00
0.000000E-00	0.031035E-00	0.047874E-00	0.064614E-00	0.081355E-00	0.098096E-00
0.000000E-00	0.021535E-00	0.038374E-00	0.055114E-00	0.071855E-00	0.088596E-00
0.000000E-00	0.012035E-00	0.028874E-00	0.045614E-00	0.062355E-00	0.079096E-00
0.000000E-00	0.002535E-00	0.019374E-00	0.036114E-00	0.052855E-00	0.069596E-00
0.000000E-00	0.000000E-00	0.000000E-00	0.000000E-00	0.000000E-00	0.000000E-00

FIGURE 20. Group A Sample Problems Program Results  
(continued)

0.14283492-C0	0.45316995-C0	0.1658290E-00	0.1700103-C0	0.3364848E-00	0.2064476E-00
0.2250505E-C0	0.2485091E-00	0.2737869E-00	0.1058147E-00	0.1426924E-00	0.4131378E-00
0.5700201E-C0	0.6195098E-01	0.663191E-01	0.710372E-01	0.741163E-01	0.8197921E-01
0.8705442E-C1	0.9736602E-01	0.1007149E-00	0.1080744E-00	0.115874E-00	0.123875E-00
0.1150318E-00	0.1233369E-00	0.1519020E-00	0.165208E-00	0.177394E-03	0.1906391E-00
0.2231992E-C0	0.2274442E-00	0.4760079E-00	0.4267418E-00	0.2993620E-03	0.3627491E-00
0.5000000E-C0	0.5000000E-00	0.6510938E-01	0.6798038E-01	0.7236572E-01	0.7773592E-01
0.8151061E-01	0.8724607E-01	0.915068E-00	0.95068E-00	0.98623E-00	0.102197E-00
0.1224662E-C0	0.1258571E-00	0.141179E-00	0.150768E-00	0.15623E-03	0.162197E-00
0.4818160E-00	0.1121608E-00	0.2033451E-00	0.2147893E-00	0.226409E-03	0.2381744E-00
0.8330000E-C0					

FIGURE 20. Group A Sample Problems Program Results  
(continued)

FIGURE 20. Group A Sample Problems Program Results  
(continued)









0.57844E-00	0.417350E-00	0.456784E-00	0.566174E-00	0.531204E-00	0.536320E-00
0.511642E-00	0.4765240E-00	0.478470E-00	0.700373E-00	0.680044E-00	0.675987E-00
0.28381E-00	0.316400E-00	0.718771E-00	0.700373E-00	0.680044E-00	0.675987E-00
0.604109E-00	0.327473E-00	0.718771E-00	0.700373E-00	0.680044E-00	0.675987E-00
0.601033E-00	0.5117073E-00	0.566667E-00	0.373762E-00	0.514933E-00	0.426997E-00
0.285374E-00	0.5160184E-00	0.5234621E-00	0.506666E-00	0.476834E-00	0.426997E-00
0.500000E-00	0.733714E-00	0.724639E-00	0.714780E-00	0.7031451E-00	0.632160E-00
0.621278E-00	0.6707421E-00	0.660584E-00	0.550844E-00	0.6415274E-00	0.632077E-00
0.581180E-00	0.660721E-00	0.660584E-00	0.550844E-00	0.6415274E-00	0.632077E-00
0.581180E-00	0.577735E-00	0.576688E-00	0.576688E-00	0.5691498E-00	0.588944E-00
0.305734E-00			0.576688E-00	0.5691498E-00	0.588944E-00

FIGURE 20. Group A Sample Problems Program Results  
(continued)

NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. 1A) K<sub>A</sub> TOUPS=1.1/03

RUN NO. 4 DATA USED FOR THIS RUN= \*2MALLS\*IFLOOR\*  
 \*  
 \*  
 \*

A NONPLANAR SURFACE CANNOT BE USED AS SURFACE 1-THIS RUN ABORTED.

FIGURE 20. Group A Sample Problems Program Results  
 (continued)

NAA COMPAC II REPORT SAMPLE PROBLEMS FROM FIG. (A)X-A-TOUPE:11/1/03

RUN NO. 5 DATA USED FOR THIS RUN- \*IFLOOS\*+HALL\*  
 \* \* \*  
 \* \* \*

NOV. OF SURFACE \*IFLOUP \* IS SEEN BY SURFACE \*HALL\*  
 IF THE ABOVE RESULT IS UNEXPECTED, OR NOT BECOME ALARMED- IT HAPPENS TO THE BEST OF CM- JUST CHECK YOUR  
 DATA- ESPECIALLY BE SURE THAT YOU ENTERED ALL POINTS IN COUNTERCLOCKWISE ORDER, AS THEY APPEAR WHEN  
 FACING THE ACTIVE SIDE OF THE SURFACE, AND DERIVED FROM A RIGHT-HANDED COORDINATE SYSTEM.

FIGURE 20. Group A Sample Problems Program Results  
 (continued)

MIA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. 1A1-KA-17/P5,11/1/63

```

RIV NO- 6 DATA USED FOR THIS RUN- *IFLOOR*2WALLZ*
      *D *
      *
THE FORM FACTOR FROM SURFACE *IFLOOR * TO SURF/CE *2WALLZ * = 0.39932
THE EXCHANGE COEFFICIENT (FA)- 0.39932E-00 SO UNITS
      *
THE AREA OF SURFACE *IFLOOR * = 0.1000000E 01 SO UNITS.
      *
ONLY A PART OF SURFACE *2WALLZ * SEES SURFACE *IFLOOR *
      *
THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTA-ION-

```

```

***** DATA NAME- *IFLOOR *
POINT X Y Z POINT X Y Z
1 0.1000000E 01 0. 0.1000000E 01 0. 0.1000000E 01 0.1000000E 01 0.
2 0. 0.1000000E 01 0. 0.1000000E 01 0. 0.1000000E 01 0.
3 0. 0.1000000E 01 0. 0.1000000E 01 0. 0.1000000E 01 0.
4 0. 0.1000000E 01 0. 0.1000000E 01 0. 0.1000000E 01 0.

***** DATA NAME- *2WALLZ *
POINT X Y Z POINT X Y Z
1 0. 0.1000000E 01 0.1000000E 01 0. 0.1000000E 01 0.1000000E 01
2 0.1000000E 01 0.1000000E 01 0.1000000E 01 0.1000000E 01 0.1000000E 01
3 0.1000000E 01 0.1000000E 01 0.1000000E 01 0.1000000E 01 0.1000000E 01
4 0.1000000E 01 0.1000000E 01 0.1000000E 01 0.1000000E 01 0.1000000E 01
COORDINATES OF POINTS ON BOUNDARY OF SURF *IFLOOR * FOR EACH Y INTERVAL
X-LEFT X-RIGHT Y X-LEFT X-RIGHT Y

```

FIGURE 20. Group A Sample Problems Program Results  
(continued)





0.632637E+00	0.610144E+00	0.386625E+00	0.366885E+00	0.545552E+00	0.524742E+00
0.394453E+00	0.380728E+00	0.364866E+00	0.340149E+00	0.334827E+00	0.317765E+00
0.301914E+00	0.282558E+00	0.269607E+00	0.253157E+00	0.236581E+00	0.220027E+00
0.203547E+00	0.182640E+00	0.173946E+00	0.167893E+00	0.159559E+00	0.150621E+00
0.119172E+00	0.100330E+00	0.936037E+00	0.864330E+00	0.771448E+00	0.670225E+00
0.411090E+00	0.396037E+00	0.382123E+00	0.366316E+00	0.350388E+00	0.334281E+00
0.311843E+00	0.301030E+00	0.283768E+00	0.268168E+00	0.246849E+00	0.220122E+00
0.058463E+00	0.630707E+00	0.611024E+00	0.591283E+00	0.574803E+00	0.532228E+00
0.319792E+00	0.312507E+00	0.298714E+00	0.284406E+00	0.268387E+00	0.251451E+00
0.334981E+00	0.317391E+00	0.299112E+00	0.280149E+00	0.260419E+00	0.240744E+00
0.220847E+00	0.143456E+00	0.146271E+00	0.140190E+00	0.135344E+00	0.126717E+00
0.455236E+00	0.314631E+00	0.314421E+00	0.498241E+00	0.442064E+00	0.466165E+00
0.450223E+00	0.434954E+00	0.419440E+00	0.403705E+00	0.387608E+00	0.370531E+00
0.323747E+00	0.333227E+00	0.315651E+00	0.295416E+00	0.274034E+00	0.251958E+00
0.670744E+00	2.65747E+00	0.134723E+00	0.616879E+00	0.599212E+00	0.581824E+00
0.564788E+00	0.544014E+00	0.531823E+00	0.515909E+00	0.500310E+00	0.485018E+00
0.371882E+00	0.354335E+00	0.338181E+00	0.323177E+00	0.308458E+00	0.294048E+00
0.371807E+00	0.356360E+00	0.338175E+00	0.321217E+00	0.298745E+00	0.284648E+00
0.237950E+00	0.644596E+00	0.643190E+00	0.630145E+00	0.613388E+00	0.594646E+00
0.590513E+00	0.575767E+00	0.564232E+00	0.551029E+00	0.510194E+00	0.504443E+00
0.492518E+00	0.475551E+00	0.460049E+00	0.445932E+00	0.430141E+00	0.413421E+00
0.632168E+00	0.672747E+00	0.654823E+00	0.644376E+00	0.627834E+00	0.612225E+00
0.590652E+00	0.581608E+00	0.567117E+00	0.552728E+00	0.538023E+00	0.524425E+00
0.422658E+00	0.404715E+00	0.388458E+00	0.373502E+00	0.358458E+00	0.344281E+00
0.257532E+00	2.421151E+00	0.376027E+00	0.353502E+00	0.334320E+00	0.291907E+00
0.703331E+00	0.694012E+00	0.675796E+00	0.657180E+00	0.645659E+00	0.629731E+00
0.447810E+00	0.437842E+00	0.426676E+00	0.415507E+00	0.404359E+00	0.393205E+00
0.717684E+00	0.702373E+00	0.686002E+00	0.671717E+00	0.657631E+00	0.643760E+00
0.632165E+00	0.616677E+00	0.603910E+00	0.591283E+00	0.578533E+00	0.566058E+00
0.552316E+00	0.544221E+00	0.534522E+00	0.521308E+00	0.507758E+00	0.494781E+00
0.478131E+00	0.466760E+00	0.454568E+00	0.441350E+00	0.427194E+00	0.413194E+00

FIGURE 20. Group A Sample Problems Program Results  
(continued)





#### SYNTH. PROBLEM GROUP B

The geometrical relationships used in this example are presented in Figure 21. The data sheets are shown in Figure 22 with results in Figure 23.

##### Problem 1B

The use of the surface generator and double bisection of surfaces is demonstrated. The plane Surface 1PLAT1 is entered as usual in the data, but the octagonal disk 3DISK is created by specifications to the surface generator. Note that no connections data are created for a Class 3 surface, but would be if the disk were named CDISK.

The double bisection is easily seen in side view of 1PLAT1 and 3DISK. The results of the factor request from 1PLAT1 and 3DISK is shown in Run #1 output, indicating the areas in each surface seen by the other. The number of points defining 3DISK has been reduced to 7 and reorganized because of the bisection, as seen along the dotted line.

##### Problem 2B

The converse factor, 3DISK to 1PLAT1, is requested as Run #2. Because the disk is now Surface 1, the final coordinate system in 3DISK is aligned so that the XY plane is the plane of the disk. Point 1 becomes the origin, and line segment 1-2 the X axis. Note that the exchange coefficients (FA) are very nearly equal, as they should be because of the reciprocity theorem.

Notice that the factor from one surface to the other along the line of bisection is, in reality, zero, but the output is, in some cases, non-zero though quite small ( $10^{-8}$  order of magnitude). This is caused by accumulated internal truncation error, and is not significant enough to warrant concern here. (This is not the case, however, with some silhouette generator computations).

##### Problem 3B

The capability of coordinate transformation is illustrated. Run #3 requests the factor from 1PLAT1 to 3DISK transformed to the position shown by the transformation data 9TDISK. The program detected, after transforming 3DISK, that it bisected 1PLAT1. As the output shows, the part of 1PLAT1 actually named was the trapezoid indicated in the top view, and in the output final coordinate data.

##### Problem 4B

It is quite feasible to generate or manually input a surface, transform the surface to a different location, and then ask for the factor between the original surface and the transformed surface. This is shown by Run #4, where 3DISK is used as Surface 1, and 3DISK transformed by 9TDISK is used as

Surface 2. The output shows a bisection of 3DISK, removing the 4th boundary point, and therefore adding a point to the final 3DISK surface boundaries, making it 9 instead of 8.

#### Problem 5B

The factor from the transformed disk, 3DISK9TDICK, to 1PLAT1 is requested as Run #5, demonstrating program flexibility in that Surface 1 is now transformed. The resulting exchange coefficient is very nearly equal to Run #3, as it should be.

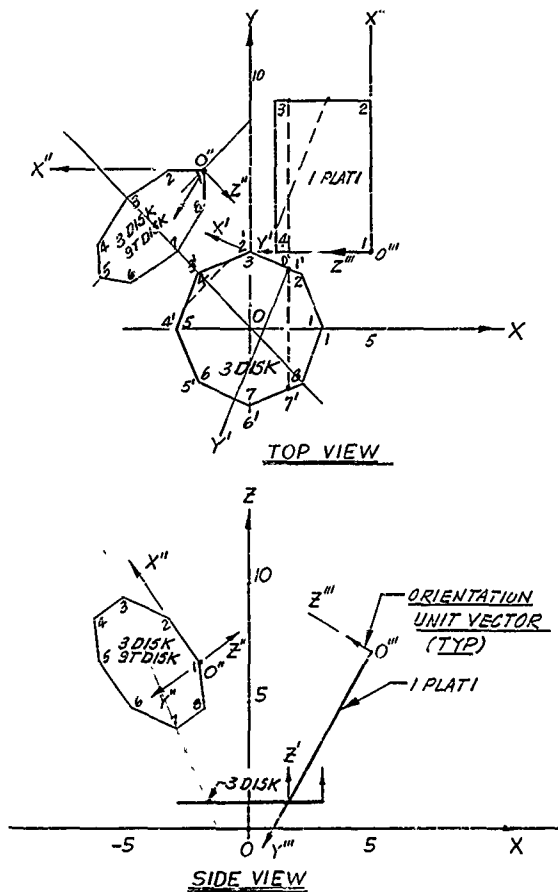


FIGURE 21. GROUP B SAMPLE PROBLEMS GEOMETRY

**FORTRAN FIXED 10 DIGIT DECIMAL DATA**

DECK NO. \_\_\_\_\_ PROGRAMMER \_\_\_\_\_ DATE \_\_\_\_\_ PAGE 3 of 3 JOB NO. 252-20

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	0.00000000		
2	0.00000000		
3	0.00000000		
4	0.00000000		
5	0.00000000		
6	0.00000000		
7	0.00000000		
8	0.00000000		
9	0.00000000		
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41	0.00000000		
42	0.00000000		
43	0.00000000		
44	0.00000000		
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46	0.00000000		
47	0.00000000		
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66	0.00000000		
67	0.00000000		
68	0.00000000		
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97	0.00000000		
98	0.00000000		
99	0.00000000		
100	0.00000000		

**FORTRAN FIXED 10 DIGIT DECIMAL DATA**

DECK NO. \_\_\_\_\_ PROGRAMMER \_\_\_\_\_ DATE \_\_\_\_\_ PAGE 10 of 31 JOB NO. 252-20

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	0.00000000		
2	0.00000000		
3	0.00000000		
4	0.00000000		
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13	0.00000000		
14	0.00000000		
15	0.00000000		
16	0.00000000		
17	0.00000000		
18	0.00000000		
19	0.00000000		
20	0.00000000		
21	0.00000000		
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97	0.00000000		
98	0.00000000		
99	0.00000000		
100	0.00000000		

FIGURE 22. Group B Sample Problems Input Data Code Sheets

FORTRAN FIXED 10 DIGIT DECIMAL DATA			
DECK NO.	PROGRAMMER	DATE	PAGE 11 OF 31 JOB NO. 2502-30
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
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FORTRAN FIXED 10 DIGIT DECIMAL DATA			
DECK NO.	PROGRAMMER	DATE	PAGE 12 OF 31 JOB NO. 2502-30
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
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FIGURE 22. Group B Sample Problems Input Data Code Sheets  
(continued)

NRA SPACE AND INFORMATION SYSTEMS DIVISION  
T-4 PROJECT AIRCRAFT-INTERFERENCE CONFIGURATION FACTOR PROGRAM

C O N F A C I

NRA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (8)-K<sub>4</sub>10UP511/1/63

I N P L T D A T A

```

***** DATA NAME= *PLATE * A SKEWED RECTANGULAR SURFACE
POINT X Y Z POINT X Y Z
1 0.4131776 01 0.3000000 01 0.7450139 01---(INTERNALLY GENERATED ORIENTATION VECTORS)
2 0.4131776 01 0.3000000 01 0.7450139 01 0.7450139 01 0.7450139 01 0.7450139 01
3 0.4100000 01 0.4000000 01 0.4000000 01 0.4000000 01 0.4000000 01 0.4000000 01

```

```

***** DATA NAME= *3DISK * OCTAGONAL DISK
SURFACE SPECIFICATIONS=
NO OF X-SECTIONS = 1 NO OF Z-SECTION BOUNDARY DIVISIONS = 8
LOCATION OF VERTICAL CENTRALLINE, X= 0.
Y= 0.
X-SECTION NO. Y-RADIUS Y-AXIS RADIUS ELEVATION ABOVE XY PLANE
1 0.3000000 01 0.3000000 01 0.1000000 01

```

THE FOLLOWING INTERNALLY GENERATED SURFACE DATA RESULTED FROM THE ABOVE SPECIFICATIONS--

```

POINT X Y Z POINT X Y Z
1 0.5136000 01 0. 0.2000000 01---(INTERNALLY GENERATED ORIENTATION VECTORS)
2 0.5136000 01 0. 0.2000000 01 0.2000000 01 0.2000000 01 0.2000000 01
3 0.5879331 07 0.3000000 01 0.1000000 01 4 -0.2121320 01 0.2121320 01 0.1000000 01
4 -0.2121320 01 0.1000000 01 5 -0.2121320 01 0.2121320 01 0.1000000 01
5 -0.2121320 01 0.1000000 01 6 -0.2121320 01 0.2121320 01 0.1000000 01
6 -0.2121320 01 0.1000000 01 7 0.2121320 01 0.2121320 01 0.1000000 01
7 0.2121320 01 0.1000000 01 8 0.2121320 01 0.2121320 01 0.1000000 01

```

```

***** DATA NAME= *9DISK * TRANSFORMS 3DISK TO SKEWED POSITION IN II QUADRANT
TRANSFORMATION DATA=

```

FIGURE 23. Group B Sample Problems Program Results  
(27 pages)

	X	Y	Z	POINT	X	Y	Z
1	-0.193940E 01	0.6181981E 01	0.4590725E 01	1	-0.511130E 01	0.511130E 01	0.919616E 01
7	-0.360000E 01	0.300000E 01	0.400000E 01				

FIGURE 23. Group 3 Sample Problems Program Results  
(continued)

WIAA COIFAC II REPORT SAMPLE PROBLEMS FROM FIG. (P)-K.A.YCUPS.11/1/63

[illegible]

FIGURE 23. Group B Sample Problems Program Results  
(continued)









[illegible]

FIGURE 23. Group 3 Sample Problems Program Results  
(continued)

NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (B)-K-A.TOUPO<sub>5</sub> 1.1/1/63

```

RUN NO. 2 DATA USED FOR THIS RUN= *3DISK *1PLAT1*
          *0*
          *
          *
THE FORM FACTOR FROM SURFACE *3DISK * TO SURFACE *1PLAT1 * = 0.01613
THE EXCHANGE COEFFICIENT (FAI)= 0.46198E+00 50 UNITS
THE MAPPIIC AREA = 0.2112591E 02 50 UNITS

ONLY A PART OF SURFACE *3DISK * COMPRISING AN AREA OF 0.2111364E 02 50 UNITS,
SEES SURFACE *1PLAT1 *
THE AREA OF SURFACE *3DISK * = 0.2547584E 02 50 UNITS.

ONLY A PART OF SURFACE *1PLAT1 * COMPRISING AN AREA OF 0.4146304E 02 50 UNITS,
SEES SURFACE *3DISK *
THE AREA OF SURFACE *1PLAT1 * = 0.4937355E 02 50 UNITS.

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION=

***** DATA NAME= *3DISK *
POINT O. X Y Z POINT X Y Z
1 0. 0. 0. 0.100000E 01--(INTERNALLY GENERATED ORIENTATION VECTOR)
2 0.1324901 01 0.1423588 01 0. 0.700000E 01 0.
3 0.1324901 01 0.1423588 01 0. 0.3344400E 01 0.
4 0.1324901 01 0.1423588 01 0. 0.3344400E 01 0.
5 0.1324901 01 0.1423588 01 0. 0.3344400E 01 0.
6 0.1324901 01 0.1423588 01 0. 0.3344400E 01 0.

***** DATA NAME= *1PLAT1 *
POINT X Y Z POINT X Y Z

```

FIGURE 23. Group B Sample Problems Program Results  
(continued)











NAA CONPAC II REPORT SAMPLE PROBLEMS FROM FIG. (B)-A-A, 10UP5, 11/1/63

RUN NO. 3 DATA USED FOR THIS RUN- \*IPLATL\* \*OLIK\*  
 \*O\* \* \*  
 \*O\* \*  
 \*O\* \*  
 \*O\* \*  
 \*O\* \*

THE FORM FACTOR FROM SURFACE \*IPLATL\* \* TO SURFACE \*JDISK 97DISK\* = 0.03377

THE EXCHANGE COEFFICIENT (FA) = 0.12470E 01 50 UNITS

THE MAPPING AREA = 0.3686819E 02 SQ UNITS

ONLY A PART OF SURFACE \*IPLATL\*  
 SEES SURFACE \*JDISK 97DISK\*

THE AREA OF SURFACE \*IPLATL\* \* = 0.4837355E 02 SQ UNITS.

THE AREA OF SURFACE \*JDISK 97DISK\* = 0.2545584E 02 SQ UNITS.

THE FOLLOWING ARE THE (F), (L) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

\*\*\*\* DATA NAME= \*IPLATL\* \*

POINT	X	Y	Z	POINT	X	Y	Z
1	0.	0.	0.	1	0.1000000E 01	0.	0.
2	0.6000000E 01	0.	0.	2	0.6000000E 01	0.	0.
3	0.	0.8062258E 01	0.	3	0.7340150E 00	0.8062258E 01	0.
4	0.	0.	0.	4	0.7340150E 00	0.8062258E 01	0.

\*\*\*\* DATA NAME= \*JDISK 97DISK\*

POINT	X	Y	Z	POINT	X	Y	Z
1	0.356030E 01	0.355390E 01	0.2542007E 01	1	0.356030E 01	0.355390E 01	0.2542007E 01
2	0.421322E 01	0.371475E 01	0.2825626E 01	2	0.421322E 01	0.371475E 01	0.2825626E 01
3	0.421322E 01	0.371475E 01	0.2825626E 01	3	0.421322E 01	0.371475E 01	0.2825626E 01
4	0.421322E 01	0.371475E 01	0.2825626E 01	4	0.421322E 01	0.371475E 01	0.2825626E 01
5	0.421322E 01	0.371475E 01	0.2825626E 01	5	0.421322E 01	0.371475E 01	0.2825626E 01
6	0.421322E 01	0.371475E 01	0.2825626E 01	6	0.421322E 01	0.371475E 01	0.2825626E 01
7	0.	0.	0.	7	0.	0.	0.
8	0.	0.	0.	8	0.	0.	0.

FIGURE 23. Group B Sample Problems Program Results  
 (continued)







0.201026-E-04	0.193197-E-01	0.1884237E-01	0.178643E-01	0.171147E-01	0.163712E-01
0.153576E-01	0.147119-E-01	0.148477E-01	0.130473E-01	0.122020E-01	0.113642E-01
0.457505E-02	0.431587E-02	0.475224E-02	0.485820E-02	0.497881E-02	0.509767E-02
0.457496E-02	0.431588E-02	0.475224E-02	0.485820E-02	0.497881E-02	0.509767E-02
0.111800E-01	0.107262E-01	0.140178E-01	0.134537E-01	0.128422E-01	0.122447E-01
0.111800E-01	0.107262E-01	0.140178E-01	0.134537E-01	0.128422E-01	0.122447E-01
0.735875E-02	0.710228E-02	0.150311E-02	0.140771E-02	0.132722E-02	0.124902E-02
0.735875E-02	0.710228E-02	0.150311E-02	0.140771E-02	0.132722E-02	0.124902E-02
0.393768E-02	0.377944E-02	0.2841180E-02	0.1993449E-02	0.137028E-02	0.651337E-03
0.103708E-01	0.102744E-01	0.9750507E-02	0.934320E-02	0.891454E-02	0.841080E-02
0.805458E-02	0.763305E-02	0.190495E-02	0.675301E-02	0.513844E-02	0.312102E-02
0.273519E-02	0.266644E-02	0.1825368E-02	0.130905E-02	0.818860E-03	0.339272E-03
0.443047E-02	0.414748E-02	0.580676E-02	0.542224E-02	0.522165E-02	0.511363E-02
0.443047E-02	0.414748E-02	0.580676E-02	0.542224E-02	0.522165E-02	0.511363E-02
0.346308E-02	0.250483E-02	0.272375E-02	0.145500E-02	0.118594E-02	0.103043E-02
0.164211E-02	0.130906E-02	0.1098564E-02	0.823028E-03	0.540054E-03	0.274601E-03

FIGURE 23. Group B Sample Problems Program Results  
(continued)













NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. 10) \* - A.T.O.U.P.S., 11/1/63

```

RUN NO. 5 DATA USED FOR THIS RUN= *JOISK *PLAT1*
          *OTCIS* *
          *O
THE FORM FACTOR FROM SURFACE *JOISK *OTCIS* TO SURFACE *PLAT1 * = 0.04739
THE EXCHANGE COEFFICIENT (FA) = 0.120346 O1 50 UNITS
      THE MAPPING AREA = 0.2542277E 02 50 UNITS
THE AREA OF SURFACE *JOISK *OTCIS* = 6.2545584E 02 50 UNITS.
ONLY A PART OF SURFACE *PLAT1
SEE SURFACE *JOISK *OTCIS*
      * COMPARISING AN AREA OF 0.3688701E 02 50 UNITS.
THE AREA OF SURFACE *PLAT1 * = 0.4937355E 02 50 UNITS.

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION=

***** DATA NAME= *JOISK *OTCIS*
POINT 1 0. X -0. Y -0. Z -0.100000E 01---(INTERNALLY GENERATED ORIENTATION VECTOR) Z
2 0.2549687E 01 0.4223588E 01 0.
3 0.2549687E 01 0.4223588E 01 0.
4 0.3919687E 01 0.3919687E 01 0.
5 0.3919687E 01 0.3919687E 01 0.
6 0.3919687E 01 0.3919687E 01 0.
7 -0.1623587E 01 0.1623587E 01 0.
***** DATA NAME= *PLAT1*
POINT 1 0. X -0. Y -0. Z -0.100000E 01---(INTERNALLY GENERATED ORIENTATION VECTOR) Z
2 -0.1623587E 01 -0.1623587E 01 -0.3688701E 01
3 -0.1623587E 01 -0.1623587E 01 -0.3688701E 01
4 -0.1623587E 01 -0.1623587E 01 -0.3688701E 01
5 -0.1623587E 01 -0.1623587E 01 -0.3688701E 01
6 -0.1623587E 01 -0.1623587E 01 -0.3688701E 01
7 -0.1623587E 01 -0.1623587E 01 -0.3688701E 01

```

FIGURE 13. Group B Sample Problems Program Results  
(continued)

	X-LEFT	X-RIGHT	Y	X-LEFT	X-RIGHT	Y
1	0	0	0	0	0	0
2	0	0	0	0	0	0
3	0	0	0	0	0	0
4	0	0	0	0	0	0
5	0	0	0	0	0	0
6	0	0	0	0	0	0
7	0	0	0	0	0	0
8	0	0	0	0	0	0
9	0	0	0	0	0	0
10	0	0	0	0	0	0
11	0	0	0	0	0	0
12	0	0	0	0	0	0
13	0	0	0	0	0	0
14	0	0	0	0	0	0
15	0	0	0	0	0	0
16	0	0	0	0	0	0
17	0	0	0	0	0	0
18	0	0	0	0	0	0
19	0	0	0	0	0	0
20	0	0	0	0	0	0
21	0	0	0	0	0	0
22	0	0	0	0	0	0
23	0	0	0	0	0	0
24	0	0	0	0	0	0
25	0	0	0	0	0	0
26	0	0	0	0	0	0
27	0	0	0	0	0	0
28	0	0	0	0	0	0
29	0	0	0	0	0	0
30	0	0	0	0	0	0
31	0	0	0	0	0	0
32	0	0	0	0	0	0
33	0	0	0	0	0	0
34	0	0	0	0	0	0
35	0	0	0	0	0	0
36	0	0	0	0	0	0
37	0	0	0	0	0	0
38	0	0	0	0	0	0
39	0	0	0	0	0	0
40	0	0	0	0	0	0
41	0	0	0	0	0	0
42	0	0	0	0	0	0
43	0	0	0	0	0	0
44	0	0	0	0	0	0
45	0	0	0	0	0	0
46	0	0	0	0	0	0
47	0	0	0	0	0	0
48	0	0	0	0	0	0
49	0	0	0	0	0	0
50	0	0	0	0	0	0
51	0	0	0	0	0	0
52	0	0	0	0	0	0
53	0	0	0	0	0	0
54	0	0	0	0	0	0
55	0	0	0	0	0	0
56	0	0	0	0	0	0
57	0	0	0	0	0	0
58	0	0	0	0	0	0
59	0	0	0	0	0	0
60	0	0	0	0	0	0
61	0	0	0	0	0	0
62	0	0	0	0	0	0
63	0	0	0	0	0	0
64	0	0	0	0	0	0
65	0	0	0	0	0	0
66	0	0	0	0	0	0
67	0	0	0	0	0	0
68	0	0	0	0	0	0
69	0	0	0	0	0	0
70	0	0	0	0	0	0
71	0	0	0	0	0	0
72	0	0	0	0	0	0
73	0	0	0	0	0	0
74	0	0	0	0	0	0
75	0	0	0	0	0	0
76	0	0	0	0	0	0
77	0	0	0	0	0	0
78	0	0	0	0	0	0
79	0	0	0	0	0	0
80	0	0	0	0	0	0
81	0	0	0	0	0	0
82	0	0	0	0	0	0
83	0	0	0	0	0	0
84	0	0	0	0	0	0

THE FOLLOWING ARE PLANE POINT CONFIGURATION FACTORS COMPUTED FOR THIS RUN  
LOWEST GRID LINE FIRST, FROM X-LEFT TO X-HIGH.

0.9533347E+01	0.92933347E+01	0.89923347E+01	0.87103347E+01	0.84483347E+01	0.82063347E+01
0.79743347E+01	0.77303347E+01	0.74983347E+01	0.72723347E+01	0.70623347E+01	0.68673347E+01
0.66863347E+01	0.65003347E+01	0.63223347E+01	0.61603347E+01	0.60123347E+01	0.58783347E+01
0.57563347E+01	0.56363347E+01	0.55223347E+01	0.54143347E+01	0.53123347E+01	0.52163347E+01
0.51263347E+01	0.50423347E+01	0.49643347E+01	0.48923347E+01	0.48263347E+01	0.47663347E+01
0.47123347E+01	0.46543347E+01	0.45983347E+01	0.45443347E+01	0.44923347E+01	0.44423347E+01
0.43943347E+01	0.43463347E+01	0.42983347E+01	0.42523347E+01	0.42083347E+01	0.41663347E+01
0.41263347E+01	0.40863347E+01	0.40463347E+01	0.40083347E+01	0.39723347E+01	0.39383347E+01
0.39063347E+01	0.38723347E+01	0.38383347E+01	0.38063347E+01	0.37763347E+01	0.37483347E+01
0.37223347E+01	0.36943347E+01	0.36663347E+01	0.36403347E+01	0.36163347E+01	0.35943347E+01
0.35723347E+01	0.35523347E+01	0.35323347E+01	0.35143347E+01	0.34983347E+01	0.34843347E+01
0.34723347E+01	0.34543347E+01	0.34363347E+01	0.34203347E+01	0.34063347E+01	0.33943347E+01
0.33823347E+01	0.33723347E+01	0.33623347E+01	0.33543347E+01	0.33463347E+01	0.33383347E+01
0.33323347E+01	0.33243347E+01	0.33163347E+01	0.33083347E+01	0.33023347E+01	0.32963347E+01
0.32903347E+01	0.32843347E+01	0.32783347E+01	0.32723347E+01	0.32683347E+01	0.32643347E+01
0.32603347E+01	0.32563347E+01	0.32523347E+01	0.32483347E+01	0.32443347E+01	0.32403347E+01
0.32363347E+01	0.32323347E+01	0.32283347E+01	0.32243347E+01	0.32203347E+01	0.32163347E+01
0.32123347E+01	0.32083347E+01	0.32043347E+01	0.32003347E+01	0.31963347E+01	0.31923347E+01
0.31883347E+01	0.31843347E+01	0.31803347E+01	0.31763347E+01	0.31723347E+01	0.31683347E+01
0.31643347E+01	0.31603347E+01	0.31563347E+01	0.31523347E+01	0.31483347E+01	0.31443347E+01
0.31403347E+01	0.31363347E+01	0.31323347E+01	0.31283347E+01	0.31243347E+01	0.31203347E+01
0.31163347E+01	0.31123347E+01	0.31083347E+01	0.31043347E+01	0.31003347E+01	0.30963347E+01
0.30923347E+01	0.30883347E+01	0.30843347E+01	0.30803347E+01	0.30763347E+01	0.30723347E+01
0.30683347E+01	0.30643347E+01	0.30603347E+01	0.30563347E+01	0.30523347E+01	0.30483347E+01
0.30443347E+01	0.30403347E+01	0.30363347E+01	0.30323347E+01	0.30283347E+01	0.30243347E+01
0.30203347E+01	0.30163347E+01	0.30123347E+01	0.30083347E+01	0.30043347E+01	0.30003347E+01
0.29963347E+01	0.29923347E+01	0.29883347E+01	0.29843347E+01	0.29803347E+01	0.29763347E+01
0.29723347E+01	0.29683347E+01	0.29643347E+01	0.29603347E+01	0.29563347E+01	0.29523347E+01
0.29483347E+01	0.29443347E+01	0.29403347E+01	0.29363347E+01	0.29323347E+01	0.29283347E+01
0.29243347E+01	0.29203347E+01	0.29163347E+01	0.29123347E+01	0.29083347E+01	0.29043347E+01
0.29003347E+01	0.28963347E+01	0.28923347E+01	0.28883347E+01	0.28843347E+01	0.28803347E+01
0.28763347E+01	0.28723347E+01	0.28683347E+01	0.28643347E+01	0.28603347E+01	0.28563347E+01
0.28523347E+01	0.28483347E+01	0.28443347E+01	0.28403347E+01	0.28363347E+01	0.28323347E+01
0.28283347E+01	0.28243347E+01	0.28203347E+01	0.28163347E+01	0.28123347E+01	0.28083347E+01
0.28043347E+01	0.28003347E+01				

FIGURE 23. Group 3 Sample Problems: Program Results  
(continued)

0.1514432E-01	0.5415525E-01	0.6421239E-01	0.6335611E-01	0.5114125E-01	0.4919021E-01
0.1707508E-01	0.5580456E-01	0.6525247E-01	0.6413981E-01	0.5300217E-01	0.5276222E-01
0.1635981E-01	0.1027147E-00	0.5951011E-01	0.5493180E-01	0.5002212E-01	0.4954663E-01
0.1109345E-00	0.5631880E-01	0.6457132E-01	0.5146344E-01	0.4889560E-01	0.4845623E-01
0.1732323E-01	0.5631880E-01	0.6457132E-01	0.5146344E-01	0.4889560E-01	0.4845623E-01
0.4446221E-01	0.4232695E-01	0.6109590E-01	0.3882872E-01	0.3676205E-01	0.3369004E-01
0.1136352E-01	0.1312851E-01	0.5013544E-00	0.5576503E-01	0.5048345E-01	0.4951029E-01
0.4092113E-01	0.7642877E-01	0.7241408E-01	0.6832255E-01	0.6463317E-01	0.6116047E-01
0.2782126E-01	0.5481056E-01	0.5102549E-01	0.4953931E-01	0.4653614E-01	0.4422550E-01
0.1087114E-01	0.3986834E-01	0.3309382E-01	0.3257614E-01	0.3541394E-01	0.3253960E-01
0.1155538E-01	0.1097127E-00	0.1023784E-00	0.9622743E-01	0.9054078E-01	0.8913807E-01
0.1594564E-01	0.5271757E-01	0.4978200E-01	0.4662768E-01	0.4444640E-01	0.4188374E-01
0.1818811E-01	0.3741379E-01	0.3358723E-01	0.3348752E-01	0.3444640E-01	0.3053568E-01
0.1408141E-00	0.1092107E-00	0.1014450E-00	0.9620898E-01	0.9017814E-01	0.8453306E-01
0.2491611E-01	0.7476595E-01	0.6997123E-01	0.6534816E-01	0.6130917E-01	0.5753762E-01
0.1401611E-01	0.5029702E-01	0.4765271E-01	0.4460100E-01	0.4213098E-01	0.3938936E-01
0.2687723E-01	0.3548425E-01	0.3312107E-01	0.3183101E-01	0.2946661E-01	0.2781603E-01
0.1103939E-00	0.1034603E-00	0.9734502E-01	0.9140361E-01	0.8582190E-01	0.8038166E-01
0.1256007E-01	0.4312840E-01	0.4062517E-01	0.3818114E-01	0.3578282E-01	0.3340597E-01
0.3654444E-01	0.3412405E-01	0.3218971E-01	0.3038609E-01	0.2868600E-01	0.2710663E-01
0.2320502E-01	0.9772531E-01	0.9125440E-01	0.8651623E-01	0.8159384E-01	0.7659296E-01
0.2320502E-01	0.6771631E-01	0.6375572E-01	0.5998798E-01	0.5645551E-01	0.5313376E-01
0.3308483E-01	0.2714431E-01	0.2448970E-01	0.2182558E-01	0.1942868E-01	0.1718882E-01
0.2458928E-01	0.3311721E-01	0.3127488E-01	0.2954908E-01	0.2793288E-01	0.2641834E-01
0.2744455E-01	0.9107081E-01	0.8666917E-01	0.8171508E-01	0.7703125E-01	0.7281127E-01
0.2458928E-01	0.4459543E-01	0.4079543E-01	0.3707543E-01	0.3401572E-01	0.3092262E-01
0.3308483E-01	0.2109382E-01	0.2034335E-01	0.1870102E-01	0.1716001E-01	0.1571394E-01
0.2458928E-01	0.4611007E-01	0.4311842E-01	0.3702684E-01	0.3276495E-01	0.2871031E-01
0.4458882E-01	0.6139358E-01	0.5767644E-01	0.5405041E-01	0.5160237E-01	0.4871362E-01
0.3408805E-01	0.4340056E-01	0.4100136E-01	0.3862276E-01	0.3670008E-01	0.3470294E-01
0.3310160E-01	0.3105997E-01	0.2946071E-01	0.2784109E-01	0.2637531E-01	0.2499740E-01
0.2534603E-01	0.4078159E-01	0.7652825E-01	0.7124745E-01	0.6661509E-01	0.6494454E-01

FIGURE 23. Group B Sample Problems Program Results  
(continued)



0.342553E-01	0.373614E-01	0.364815E-01	0.336076E-01	0.347138E-01	0.3388517E-01
0.330361E-01	0.322015E-01	0.333303E-01	0.305703E-01	0.297743E-01	0.2899237E-01
0.232258E-01	0.274710E-01	0.267307E-01	0.260158E-01	0.251099E-01	0.244224E-01
0.215050E-01	0.231736E-01	0.226550E-01	0.212889E-01	0.211406E-01	0.208283E-01
0.202815E-01	0.218876E-01	0.216196E-01	0.203397E-01	0.218192E-01	0.2119927E-01
0.355558E-01	0.278925E-01	0.262931E-01	0.268143E-01	0.278974E-01	0.271691E-01
0.277571E-01	0.278925E-01	0.262931E-01	0.268143E-01	0.278974E-01	0.271691E-01
0.233596E-01	0.227705E-01	0.222419E-01	0.211235E-01	0.211652E-01	0.207197E-01
0.202367E-01	0.207891E-01	0.204830E-01	0.201706E-01	0.203263E-01	0.207891E-01
0.242705E-01	0.277741E-01	0.272822E-01	0.267946E-01	0.251024E-01	0.2351237E-01
0.235398E-01	0.268915E-01	0.264594E-01	0.259730E-01	0.255275E-01	0.2507637E-01
0.201078E-01	0.177797E-01	0.178976E-01	0.173653E-01	0.169533E-01	0.1654797E-01
0.244431E-01	0.230688E-01	0.226926E-01	0.223177E-01	0.228440E-01	0.2267175E-01
0.252195E-01	0.259227E-01	0.254522E-01	0.251010E-01	0.243893E-01	0.2437845E-01
0.216339E-01	0.216339E-01	0.216339E-01	0.216339E-01	0.216339E-01	0.216339E-01
0.109986E-01					

FIGURE 23. Group B Sample Problems Program Results  
(continued)



#### SAMPLE PROBLEM GROUP C

The geometrical relationships for this sample problem are shown in Figure 24. The data sheets are presented in Figure 25 and the results are shown in Figure 26.

##### Problem 1C

In this problem, a solid surface which could not be created by the program surface generator is entered manually along with the necessary connections data. A cube with four truncated corners, named SCURF, is entered in data from a convenient location in its coordinate system, i.e., at the origin, as shown in Figure 24. Only three points were computed and entered as 9TCUBE transformation data to move the surface to the desired position shown over Surface 1, 1PLATS. The factor from 1PLATS to SCURF9TCUBE is requested as Run #1.

The silhouette generator was used to compute the silhouette from each point in 1PLATS, and because a detailed output was requested with 6 horizontal and 6 vertical divisions of 1PLATS, 49 silhouettes were computed as shown in Figure 26. The numbers following each identifying naming line and naming point number are the boundary point numbers which form the silhouette when connected together. It was not possible, since there are no crossovers in the silhouette, to run this problem in the simple mode in SILFAC at greater speed. The naming divisions were deliberately set at 6 x 6 to reduce the output, some experimentation is required to determine how many divisions are required to yield the factor to the accuracy desired.

##### Problem 2C

The silhouette generator requires that all points in Surface 2 be above the plane of Surface 1 when operating in either the simple or complex mode. A view of SCUBE in its original position from 1PLATS clearly shows part of SCUBE below the surface of 1PLATS; the run is therefore rejected with a diagnostic indicating this condition.

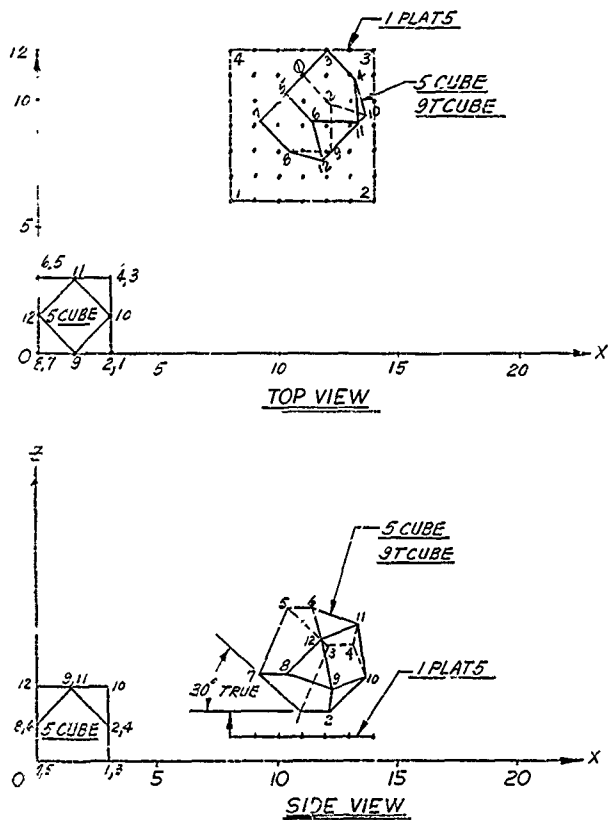


FIGURE 24. GROUP C SAMPLE PROBLEM'S GEOMETRY

FORTRAN FIXED 10 DIGIT DECIMAL DATA				
CODE NO.	PROGRAMMER	DATE	PAGE 11 of 36	JOB NO. 2470-30
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1	1.0			
2	2.0			
3	3.0			
4	4.0			
5	5.0			
6	6.0			
7	7.0			
8	8.0			
9	9.0			
10	10.0			
11	11.0			
12	12.0			
13	13.0			
14	14.0			
15	15.0			
16	16.0			
17	17.0			
18	18.0			
19	19.0			
20	20.0			
21	21.0			
22	22.0			
23	23.0			
24	24.0			
25	25.0			
26	26.0			
27	27.0			
28	28.0			
29	29.0			
30	30.0			

FORTRAN FIXED 10 DIGIT DECIMAL DATA				
CODE NO.	PROGRAMMER	DATE	PAGE 11 of 36	JOB NO. 2470-30
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1	1.0			
2	2.0			
3	3.0			
4	4.0			
5	5.0			
6	6.0			
7	7.0			
8	8.0			
9	9.0			
10	10.0			
11	11.0			
12	12.0			
13	13.0			
14	14.0			
15	15.0			
16	16.0			
17	17.0			
18	18.0			
19	19.0			
20	20.0			
21	21.0			
22	22.0			
23	23.0			
24	24.0			
25	25.0			
26	26.0			
27	27.0			
28	28.0			
29	29.0			
30	30.0			

FIGURE 25. Group C Sample Problems Input Data Code Sheets

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE 11 OF 20	JOB NO. 2025-10
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1				
2				
3				
4				
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
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97				
98				
99				
100				

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE 11 OF 20	JOB NO. 2025-10
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1				
2				
3				
4				
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
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92				
93				
94				
95				
96				
97				
98				
99				
100				

FIGURE 25. Group C Sample Problems Input Data Code Sheets  
(continued)

FORTRAN FIXED 10 DIGIT DECIMAL DATA				
DECK NO.	PROGRAMMER	DATE	PAGE 22 of 36	JOB NO. 285-10
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1	C			
2	C			
3	C			
4	C			
5	C			
6	C			
7	C			
8	C			
9	C			
10	C			
11	C			
12	C			
13	C			
14	C			
15	C			
16	C			
17	C			
18	C			
19	C			
20	C			
21	C			
22	C			
23	C			
24	C			
25	C			
26	C			
27	C			
28	C			
29	C			
30	C			
31	C			
32	C			
33	C			
34	C			
35	C			
36	C			
37	C			
38	C			
39	C			
40	C			
41	C			
42	C			
43	C			
44	C			
45	C			
46	C			
47	C			
48	C			
49	C			
50	C			
51	C			
52	C			
53	C			
54	C			
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56	C			
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64	C			
65	C			
66	C			
67	C			
68	C			
69	C			
70	C			
71	C			
72	C			
73	C			
74	C			
75	C			
76	C			
77	C			
78	C			
79	C			
80	C			
81	C			
82	C			
83	C			
84	C			
85	C			
86	C			
87	C			
88	C			
89	C			
90	C			
91	C			
92	C			
93	C			
94	C			
95	C			
96	C			
97	C			
98	C			
99	C			
100	C			

FIGURE 25. Group C Sample Problems Input Data Code Sheets  
(continued)

NAA SPACE AND INFORMATION SYSTEMS DIVISION  
 T-4 PROJECT RADIAN-INTERCHANGE CONFIGURATION FACTOR PROGRAM  
 C O N F I  
 NAA CGJFAC II REPORT SAMPLE PROBLEMS FROM FIG. (C)-K.A.T.O.U.S., 1/1/63  
 I N P U T D A T A

\*\*\*\*\* DATA NAME= \*1PLATS \* 6X6 PLATE PARALLEL TO XY PLANE, Z=1  
 POINT X Y Z POINT X Y Z  
 1 0.8000000E 01 0.4000000E 01 0.2000000E 01 1 0.1400000E 01 0.1400000E 01 0.1400000E 01  
 2 0.8000000E 01 0.4000000E 01 0.2000000E 01 2 0.1400000E 01 0.1400000E 01 0.1400000E 01  
 3 0.8000000E 01 0.4000000E 01 0.2000000E 01 3 0.1400000E 01 0.1400000E 01 0.1400000E 01

\*\*\*\*\* DATA NAME= \*SCURE \* 3 UNITS ON A SIDE, WITH FOUR ADJACENT CORNERS INDICATED  
 POINT X Y Z POINT X Y Z  
 1 0.3000000E 01 0.3000000E 01 0.3000000E 01 1 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 2 0.3000000E 01 0.3000000E 01 0.3000000E 01 2 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 3 0.3000000E 01 0.3000000E 01 0.3000000E 01 3 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 4 0.3000000E 01 0.3000000E 01 0.3000000E 01 4 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 5 0.3000000E 01 0.3000000E 01 0.3000000E 01 5 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 6 0.3000000E 01 0.3000000E 01 0.3000000E 01 6 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 7 0.3000000E 01 0.3000000E 01 0.3000000E 01 7 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 8 0.3000000E 01 0.3000000E 01 0.3000000E 01 8 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 9 0.3000000E 01 0.3000000E 01 0.3000000E 01 9 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 10 0.3000000E 01 0.3000000E 01 0.3000000E 01 10 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 11 0.3000000E 01 0.3000000E 01 0.3000000E 01 11 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 12 0.3000000E 01 0.3000000E 01 0.3000000E 01 12 0.3000000E 01 0.3000000E 01 0.3000000E 01

POINT CONNECTING POINTS POINT CONNECTING POINTS POINT CONNECTING POINTS  
 1 0.3000000E 01 0.3000000E 01 0.3000000E 01 1 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 2 0.3000000E 01 0.3000000E 01 0.3000000E 01 2 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 3 0.3000000E 01 0.3000000E 01 0.3000000E 01 3 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 4 0.3000000E 01 0.3000000E 01 0.3000000E 01 4 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 5 0.3000000E 01 0.3000000E 01 0.3000000E 01 5 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 6 0.3000000E 01 0.3000000E 01 0.3000000E 01 6 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 7 0.3000000E 01 0.3000000E 01 0.3000000E 01 7 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 8 0.3000000E 01 0.3000000E 01 0.3000000E 01 8 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 9 0.3000000E 01 0.3000000E 01 0.3000000E 01 9 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 10 0.3000000E 01 0.3000000E 01 0.3000000E 01 10 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 11 0.3000000E 01 0.3000000E 01 0.3000000E 01 11 0.3000000E 01 0.3000000E 01 0.3000000E 01  
 12 0.3000000E 01 0.3000000E 01 0.3000000E 01 12 0.3000000E 01 0.3000000E 01 0.3000000E 01

\*\*\*\*\* DATA NAME= \*SCURE \* TRANSFORMS SCURE TO SKEWED POSITION IN 15° QUAD.  
 TRANSFORMATION DATA  
 POINT X Y Z POINT X Y Z  
 1 0.1100000E 02 0.1100000E 02 0.2000000E 01 1 0.1200000E 02 0.999999E 01 0.200000E 01

FIGURE 26. Group C Sample Problems Program Results  
 (7 pages)

7 0.9162683E 01 0.9.62683E 01 0.3500000E 0.

FIGURE 26. Group C Sample Problems Program Results  
(continued)





```

1 1 9 10 1 3 1 7 0 9
2 2 9 2 1 3 1 7 0 9
3 3 9 3 1 3 1 7 0 9
4 4 9 4 1 3 1 7 0 9
5 5 9 5 1 3 1 7 0 9
6 6 9 6 1 3 1 7 0 9
7 7 9 7 1 3 1 7 0 9
8 8 9 8 1 3 1 7 0 9
9 9 9 9 1 3 1 7 0 9
10 10 9 10 1 3 1 7 0 9
11 11 9 11 1 3 1 7 0 9
12 12 9 12 1 3 1 7 0 9
13 13 9 13 1 3 1 7 0 9
14 14 9 14 1 3 1 7 0 9
15 15 9 15 1 3 1 7 0 9
16 16 9 16 1 3 1 7 0 9
17 17 9 17 1 3 1 7 0 9
18 18 9 18 1 3 1 7 0 9
19 19 9 19 1 3 1 7 0 9
20 20 9 20 1 3 1 7 0 9

```

TOTAL TIME IN SILFAC = 1.869 SECONDS.  
 THE FURN FACTOR FROM SURFACE \*PLATS \* TO SURFACE \*SCUBE 9TCUBE\* = 0.20965  
 THE EXCHANGE COEFFICIENT (EAC) = 0.75435E 01 SQ UNITS

THE MAPPING AREA = 0.3600000E 02 SQ UNITS  
 THE AREA OF SURFACE \*PLATS \* = 0.3600000E 02 SQ UNITS.  
 THE AREA OF SL NITS.

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

```

***** DATA NAME= *PLATS *
POINT 3. X Y Z POINT X Y Z
1 3. 0. 0. 0.000000E 01---(INITIALLY ORIENTED ORIENTATION VECTOR)
2 3. 0.000000E 01 0.000000E 01 0.000000E 01
3 3. 0.000000E 01 0.000000E 01 0.000000E 01
4 3. 0.000000E 01 0.000000E 01 0.000000E 01
5 3. 0.000000E 01 0.000000E 01 0.000000E 01

```

\*\*\*\*\* DATA NAME= \*SCUBE 9TCUBE\*

FIGURE 26. Group C Sample Problems Program Results  
 (continued)

POINT	X	Y	Z	POINT	X	Y	Z
1	0.3000000E-01	0.5000000E-01	1.0000000E-00	2	0.4000000E-01	0.3000000E-01	1.0000000E-00
3	0.4000000E-01	0.4000000E-01	0.3000000E-01	4	0.5000000E-01	0.2000000E-01	0.3000000E-01
5	0.5000000E-01	0.3000000E-01	0.2000000E-01	6	0.6000000E-01	0.1000000E-01	0.2000000E-01
7	0.6000000E-01	0.2000000E-01	0.1000000E-01	8	0.7000000E-01	0.1000000E-01	0.1000000E-01
9	0.7000000E-01	0.1000000E-01	0.0000000E-01	10	0.8000000E-01	0.0000000E-01	0.0000000E-01
11	0.8000000E-01	0.0000000E-01	0.0000000E-01	12	0.9000000E-01	0.0000000E-01	0.0000000E-01
13	0.9000000E-01	0.0000000E-01	0.0000000E-01	14	1.0000000E-01	0.0000000E-01	0.0000000E-01

COORDINATES OF POINTS ON BOUNDARY OF SURF \* PLATES \* FOR EACH Y INTERVAL

X-LEFT	X-RIGHT	Y	X-LEFT	X-RIGHT	Y
0.	0.4000000E-01	0.	0.	0.4000000E-01	0.
0.	0.4000000E-01	0.2000000E-01	0.	0.4000000E-01	0.2000000E-01
0.	0.4000000E-01	0.4000000E-01	0.	0.4000000E-01	0.4000000E-01
0.	0.4000000E-01	0.6000000E-01	0.	0.4000000E-01	0.6000000E-01

NO. OF HORIZONTAL INCREMENTS\* 6 NO. OF VERTICAL INCREMENTS\* 6

THE FOLLOWING ARE PLANE POINT CONFIGURATION FACTORS COMPUTED FOR THIS RUN  
 LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

0.5500000E-01	0.7770000E-01	0.8770000E-01	0.1046541E-00	0.1106608E-00	0.6935200E-01
0.7770000E-01	0.1046541E-00	0.1106608E-00	0.1793724E-00	0.1513111E-00	0.2363911E-00
0.1106608E-00	0.1793724E-00	0.1513111E-00	0.2748954E-00	0.2748954E-00	0.2721936E-00
0.2748954E-00	0.2721936E-00	0.2721936E-00	0.3933245E-00	0.3933245E-00	0.3570930E-00
0.3570930E-00	0.3570930E-00	0.3570930E-00	0.4081478E-00	0.4081478E-00	0.2582763E-00
0.4081478E-00	0.2582763E-00	0.2582763E-00	0.1717333E-00	0.1717333E-00	0.1757866E-00

FIGURE 26. Group C Sample Problems Program Results  
 (continued)

HAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (CI-K.A./JPS.11/1/63

RUN NO. 2 DATA USED FOR THIS RUN \*PLAYS+SCUBE \*  
 \*0 1\* 1\*

MAPPING SURFACE 2 SILHOUETTE COMPUTED FROM MAPPING POINT SHOWN  
 LINE PT

SURF 2 HAS A 0 OR - 2-CD340 FEL TO SURF 1-THIS RUN ABORTED.

FIGURE 26. Group C Sample Problems Program Results  
 (continued)

NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. 1C)-K.A.-TOUPS.11/1/63

RUN NO. 3 DATA USED FOR THIS RUN- \*SCUB \*PLATIS\*  
\* \* \* \* \*

A NONPLANAR SURFACE CANNOT BE USED AS SURFACE 1-THIS RUN ABORTED.

FIGURE 26. Group C Sample Problems Program Results  
(continued)

#### SAMPLE PROBLEM GROUP D

The geometrical relationship for this sample problem are presented in Figure 27. The data sheets are shown in Figure 28 and the results are presented in Figure 29.

##### Problem 1D

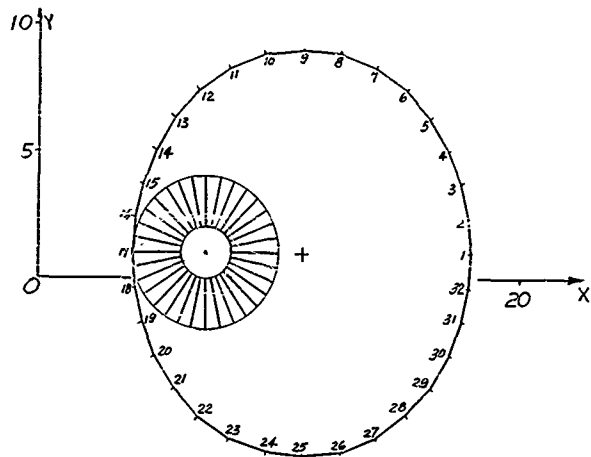
The referenced figure, Figure 27, shows a truncated-cone-on-cylinder and a disk, skewed with respect to the cylinder-cone centerline. The cylinder-cone is created by the surface generator as 6CYTR, a 32-sided solid in its final position in the unprimed coordinate system. The disk is also internally generated, but because the generator (in its present version) is limited to cross sections parallel to XY plane, the disk, 3DISK, had to be transformed to the skewed position by transformation data 9TDSKC. The results are shown in Figure 29. The simple mode was used for processing because no line segment crossovers are present, which enabled the use of transformations to construct the problem. The warning note concerning the difference between the mapping area and the actual 3DISK surface area is supplied to attract attention to possible errors in Surface 1 data entry of the choice of mapping increments. As indicated in the comments on Problem 1 of Sample Problem Group C, the coarse increment 6 x 6 was selected to reduce output. A finer increment should probably be used to insure accuracy to the third place, if such is desired. It must be emphasized that the form factor obtained in Run #1 is the factor to the solid figure, 6CYLTR, which, of course, includes the bases. Since the factor to the skin is the desired number, it is necessary to subtract the factors to the ends. The upper end is obviously not seen ( $f = 0$ ), so the factor to the base only must be obtained. The base is easily created by the surface generator (3DISKB), but it is created with the orientation vector pointing toward the +Z axis--the wrong way. It is necessary to turn it around by a primary transformation--(9TDSKN). Thus, the full capability of the primary transformation feature is utilized and exemplified, shown by Run #2. The factor to the skin of 6CYLTR is obtained by subtracting the results of Run #2 from Run #1, or

$$f_{\text{skin}} = f_{\text{total}} - f_{\text{base}}$$

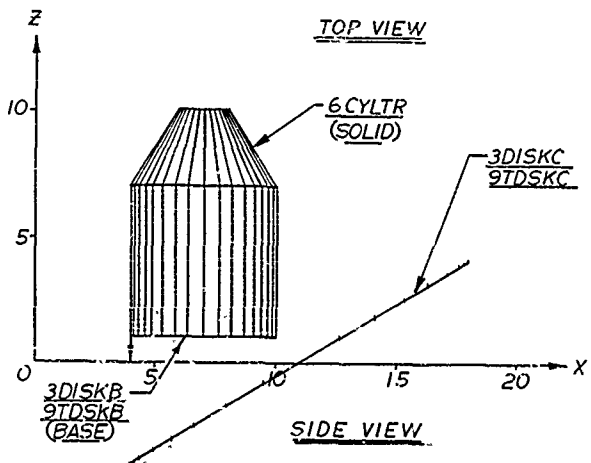
$$f = 0.18946 - 0.09955$$

$$f = .08991$$

The exchange coefficient is computed in a similar manner.



TOP VIEW



SIDE VIEW

FIGURE 27. GROUP D SAMPLE PROBLEM'S GEOMETRY

FORTRAN FIXED 10 DIGIT DECIMAL DATA			
DECK NO.	PROGRAMMER	DATE	PAGE 37 OF 38 JOB NO. 252-72
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	1	1	
2	2	2	
3	3	3	
4	4	4	
5	5	5	
6	6	6	
7	7	7	
8	8	8	
9	9	9	
10	10	10	
11	11	11	
12	12	12	
13	13	13	
14	14	14	
15	15	15	
16	16	16	
17	17	17	
18	18	18	
19	19	19	
20	20	20	
21	21	21	
22	22	22	
23	23	23	
24	24	24	
25	25	25	
26	26	26	
27	27	27	
28	28	28	
29	29	29	
30	30	30	
31	31	31	
32	32	32	
33	33	33	
34	34	34	
35	35	35	
36	36	36	
37	37	37	
38	38	38	
39	39	39	
40	40	40	
41	41	41	
42	42	42	
43	43	43	
44	44	44	
45	45	45	
46	46	46	
47	47	47	
48	48	48	
49	49	49	
50	50	50	
51	51	51	
52	52	52	
53	53	53	
54	54	54	
55	55	55	
56	56	56	
57	57	57	
58	58	58	
59	59	59	
60	60	60	
61	61	61	
62	62	62	
63	63	63	
64	64	64	
65	65	65	
66	66	66	
67	67	67	
68	68	68	
69	69	69	
70	70	70	
71	71	71	
72	72	72	
73	73	73	
74	74	74	
75	75	75	
76	76	76	
77	77	77	
78	78	78	
79	79	79	
80	80	80	
81	81	81	
82	82	82	
83	83	83	
84	84	84	
85	85	85	
86	86	86	
87	87	87	
88	88	88	
89	89	89	
90	90	90	
91	91	91	
92	92	92	
93	93	93	
94	94	94	
95	95	95	
96	96	96	
97	97	97	
98	98	98	
99	99	99	
100	100	100	

FORTRAN FIXED 10 DIGIT DECIMAL DATA			
DECK NO.	PROGRAMMER	DATE	PAGE 37 OF 38 JOB NO. 252-72
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	1	1	
2	2	2	
3	3	3	
4	4	4	
5	5	5	
6	6	6	
7	7	7	
8	8	8	
9	9	9	
10	10	10	
11	11	11	
12	12	12	
13	13	13	
14	14	14	
15	15	15	
16	16	16	
17	17	17	
18	18	18	
19	19	19	
20	20	20	
21	21	21	
22	22	22	
23	23	23	
24	24	24	
25	25	25	
26	26	26	
27	27	27	
28	28	28	
29	29	29	
30	30	30	
31	31	31	
32	32	32	
33	33	33	
34	34	34	
35	35	35	
36	36	36	
37	37	37	
38	38	38	
39	39	39	
40	40	40	
41	41	41	
42	42	42	
43	43	43	
44	44	44	
45	45	45	
46	46	46	
47	47	47	
48	48	48	
49	49	49	
50	50	50	
51	51	51	
52	52	52	
53	53	53	
54	54	54	
55	55	55	
56	56	56	
57	57	57	
58	58	58	
59	59	59	
60	60	60	
61	61	61	
62	62	62	
63	63	63	
64	64	64	
65	65	65	
66	66	66	
67	67	67	
68	68	68	
69	69	69	
70	70	70	
71	71	71	
72	72	72	
73	73	73	
74	74	74	
75	75	75	
76	76	76	
77	77	77	
78	78	78	
79	79	79	
80	80	80	
81	81	81	
82	82	82	
83	83	83	
84	84	84	
85	85	85	
86	86	86	
87	87	87	
88	88	88	
89	89	89	
90	90	90	
91	91	91	
92	92	92	
93	93	93	
94	94	94	
95	95	95	
96	96	96	
97	97	97	
98	98	98	
99	99	99	
100	100	100	

FIGURE 28. Group D Sample Problems Input Data Code Sheets

# FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE 30 of 36	JOB NO. 2422-30
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1				
2				
3				
4				
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				
17				
18				
19				
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21				
22				
23				
24				
25				
26				
27				
28				
29				
30				

# FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE 31 of 36	JOB NO. 2422-30
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1				
2				
3				
4				
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				
17				
18				
19				
20				
21				
22				
23				
24				
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28				
29				
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31				
32				
33				
34				
35				
36				
37				
38				
39				
40				

FIGURE 28. Group D Sample Problems Input Data/Code Sheets  
(continued)



NAA SPACE AND INFORMATION SYSTEMS DIVISION  
 T-4 PROJECT RADIANT-INTERCHANGE CONFIGURATION FILE PROGRAM  
 C O H F A C I I  
 NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (D)-K.A.TODPS.11/1/65

# INPUT DATA

```

***** DATA NAME= *30SKC      *      B UNIT RADIUS DISK
SURFACE SPECIFICATIONS-
NO OF X-SECTIONS = 1          NO OF X-SECTION BOUNDARY DIVISIONS = 32
LOCATION OF VERTICAL CENTERLINE, X= 0.      * Y= 0.
X-SECTION NO.      X-AXIS RADIUS      Y AXIS RADIUS      ELEVATION ABOVE XY .LANE
1      0.8000000E 01      0.8000000E 01      0.

THE FOLLOWING INTERNALLY GENERATED SURFACE DATA RESULTED FROM THE ABOVE SPECIFICATIONS-
POINT      X      Y      Z      POINT      X      Y      Z
1 0.8000000E 01 0. 0.1000000E 01----(INTERNALLY GENERATED ORIENTATION VECTOR)
2 0.7391036E 01 0.3061807E 01 0.
3 0.7391036E 01 0.7391036E 01 0.
4 0.6651758E 01 0.4484562E 01 0.
5 0.6651758E 01 0.8000000E 01 0.
6 0.4484562E 01 0.4021750E 01 0.
7 0.4021750E 01 0.7391036E 01 0.
8 0.3061807E 01 0.7391036E 01 0.
9 0.2800272E -07 0.1699999E 01 0.
10 0.1699999E 01 0.1699999E 01 0.
11 0.1699999E 01 0.7391036E 01 0.
12 0.7391036E 01 0.6021750E 01 0.
13 0.6021750E 01 0.6021750E 01 0.
14 0.6021750E 01 0.1500722E 01 0.
15 0.1500722E 01 0.7846378E 01 0.
16 0.7846378E 01 0.1500722E 01 0.
17 0.1500722E 01 0.4021750E 01 0.
18 0.4021750E 01 0.1500722E 01 0.
19 0.1500722E 01 0.7846378E 01 0.
20 0.7846378E 01 0.4021750E 01 0.
21 0.4021750E 01 0.1500722E 01 0.
22 0.1500722E 01 0.7846378E 01 0.
23 0.7846378E 01 0.4021750E 01 0.
24 0.4021750E 01 0.1500722E 01 0.
25 0.1500722E 01 0.7846378E 01 0.
26 0.7846378E 01 0.4021750E 01 0.
27 0.4021750E 01 0.1500722E 01 0.
28 0.1500722E 01 0.7846378E 01 0.
29 0.7846378E 01 0.4021750E 01 0.
30 0.4021750E 01 0.1500722E 01 0.
31 0.1500722E 01 0.7846378E 01 0.
32 0.7846378E 01 0.1500722E 01 0.
  
```

FIGURE 29. Group D Sample Problems Program Results  
 (14 pages)

```

***** DATA NAME= *GCYL*
SURFACE SPECIFICATIONS=
NO OF X-SECTIONS = 3          NO OF X-SECTION BOUNDARY DIVISIONS = 32
LOCATION OF VERTICAL CENTERLINE, X= 0.700000E 01, Y= 0.100000E 01
X-SECTION NO.      X-AXIS RADIUS      Y-AXIS RADIUS      ELEVATION ABOVE XY PLANE
1      0.400000E 01      0.300000E 01      0.100000E 01
2      0.400000E 01      0.300000E 01      0.700000E 01
3      0.100000E 01      0.100000E 01      0.100000E 02

THE FOLLOWING INTERNALLY GENERATED SURFACE DATA RESULTED FROM THE ABOVE SPECIFICATIONS-

PRINT      X      Y      Z      POINT
1 0.100000E 02 0.100000E 01 0.100000E 01 1
2 0.400000E 01 0.100000E 01 0.100000E 02 2
3 0.400000E 01 0.100000E 01 0.700000E 02 3
4 0.700000E 01 0.100000E 01 0.100000E 02 4
5 0.700000E 01 0.100000E 01 0.700000E 02 5
6 0.700000E 01 0.100000E 01 0.100000E 02 6
7 0.700000E 01 0.100000E 01 0.700000E 02 7
8 0.700000E 01 0.100000E 01 0.100000E 02 8
9 0.700000E 01 0.100000E 01 0.700000E 02 9
10 0.700000E 01 0.100000E 01 0.100000E 02 10
11 0.700000E 01 0.100000E 01 0.700000E 02 11
12 0.700000E 01 0.100000E 01 0.100000E 02 12
13 0.700000E 01 0.100000E 01 0.700000E 02 13
14 0.700000E 01 0.100000E 01 0.100000E 02 14
15 0.700000E 01 0.100000E 01 0.700000E 02 15
16 0.700000E 01 0.100000E 01 0.100000E 02 16
17 0.700000E 01 0.100000E 01 0.700000E 02 17
18 0.700000E 01 0.100000E 01 0.100000E 02 18
19 0.700000E 01 0.100000E 01 0.700000E 02 19
20 0.700000E 01 0.100000E 01 0.100000E 02 20
21 0.700000E 01 0.100000E 01 0.700000E 02 21
22 0.700000E 01 0.100000E 01 0.100000E 02 22
23 0.700000E 01 0.100000E 01 0.700000E 02 23
24 0.700000E 01 0.100000E 01 0.100000E 02 24
25 0.700000E 01 0.100000E 01 0.700000E 02 25
26 0.700000E 01 0.100000E 01 0.100000E 02 26
27 0.700000E 01 0.100000E 01 0.700000E 02 27
28 0.700000E 01 0.100000E 01 0.100000E 02 28
29 0.700000E 01 0.100000E 01 0.700000E 02 29
30 0.700000E 01 0.100000E 01 0.100000E 02 30
31 0.700000E 01 0.100000E 01 0.700000E 02 31
32 0.700000E 01 0.100000E 01 0.100000E 02 32
33 0.700000E 01 0.100000E 01 0.700000E 02 33
34 0.700000E 01 0.100000E 01 0.100000E 02 34
35 0.700000E 01 0.100000E 01 0.700000E 02 35
36 0.700000E 01 0.100000E 01 0.100000E 02 36
37 0.700000E 01 0.100000E 01 0.700000E 02 37
38 0.700000E 01 0.100000E 01 0.100000E 02 38
39 0.700000E 01 0.100000E 01 0.700000E 02 39
40 0.700000E 01 0.100000E 01 0.100000E 02 40
41 0.700000E 01 0.100000E 01 0.700000E 02 41
42 0.700000E 01 0.100000E 01 0.100000E 02 42
43 0.700000E 01 0.100000E 01 0.700000E 02 43
44 0.700000E 01 0.100000E 01 0.100000E 02 44
45 0.700000E 01 0.100000E 01 0.700000E 02 45
46 0.700000E 01 0.100000E 01 0.100000E 02 46
47 0.700000E 01 0.100000E 01 0.700000E 02 47
48 0.700000E 01 0.100000E 01 0.100000E 02 48
49 0.700000E 01 0.100000E 01 0.700000E 02 49
50 0.700000E 01 0.100000E 01 0.100000E 02 50
51 0.700000E 01 0.100000E 01 0.700000E 02 51
52 0.700000E 01 0.100000E 01 0.100000E 02 52
53 0.700000E 01 0.100000E 01 0.700000E 02 53
54 0.700000E 01 0.100000E 01 0.100000E 02 54
55 0.700000E 01 0.100000E 01 0.700000E 02 55
56 0.700000E 01 0.100000E 01 0.100000E 02 56
57 0.700000E 01 0.100000E 01 0.700000E 02 57
58 0.700000E 01 0.100000E 01 0.100000E 02 58
59 0.700000E 01 0.100000E 01 0.700000E 02 59
60 0.700000E 01 0.100000E 01 0.100000E 02 60
61 0.700000E 01 0.100000E 01 0.700000E 02 61
62 0.700000E 01 0.100000E 01 0.100000E 02 62
63 0.700000E 01 0.100000E 01 0.700000E 02 63
64 0.700000E 01 0.100000E 01 0.100000E 02 64
65 0.700000E 01 0.100000E 01 0.700000E 02 65
66 0.700000E 01 0.100000E 01 0.100000E 02 66
67 0.700000E 01 0.100000E 01 0.700000E 02 67
68 0.700000E 01 0.100000E 01 0.100000E 02 68
69 0.700000E 01 0.100000E 01 0.700000E 02 69
70 0.700000E 01 0.100000E 01 0.100000E 02 70
71 0.700000E 01 0.100000E 01 0.700000E 02 71
72 0.700000E 01 0.100000E 01 0.100000E 02 72
73 0.700000E 01 0.100000E 01 0.700000E 02 73
74 0.700000E 01 0.100000E 01 0.100000E 02 74
75 0.700000E 01 0.100000E 01 0.700000E 02 75
76 0.700000E 01 0.100000E 01 0.100000E 02 76
77 0.700000E 01 0.100000E 01 0.700000E 02 77
78 0.700000E 01 0.100000E 01 0.100000E 02 78
79 0.700000E 01 0.100000E 01 0.700000E 02 79
80 0.700000E 01 0.100000E 01 0.100000E 02 80
81 0.700000E 01 0.100000E 01 0.700000E 02 81
82 0.700000E 01 0.100000E 01 0.100000E 02 82
83 0.700000E 01 0.100000E 01 0.700000E 02 83
84 0.700000E 01 0.100000E 01 0.100000E 02 84
85 0.700000E 01 0.100000E 01 0.700000E 02 85
86 0.700000E 01 0.100000E 01 0.100000E 02 86
87 0.700000E 01 0.100000E 01 0.700000E 02 87
88 0.700000E 01 0.100000E 01 0.100000E 02 88
89 0.700000E 01 0.100000E 01 0.700000E 02 89
90 0.700000E 01 0.100000E 01 0.100000E 02 90
91 0.700000E 01 0.100000E 01 0.700000E 02 91
92 0.700000E 01 0.100000E 01 0.100000E 02 92
93 0.700000E 01 0.100000E 01 0.700000E 02 93
94 0.700000E 01 0.100000E 01 0.100000E 02 94
95 0.700000E 01 0.100000E 01 0.700000E 02 95
96 0.700000E 01 0.100000E 01 0.100000E 02 96
97 0.700000E 01 0.100000E 01 0.700000E 02 97
98 0.700000E 01 0.100000E 01 0.100000E 02 98
99 0.700000E 01 0.100000E 01 0.700000E 02 99
100 0.700000E 01 0.100000E 01 0.100000E 02 100

```

FIGURE 29. Group D Sample Problems Program Results  
(continued)

137

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61 84. 0. 78. 60 82 85. 83. 79. 0 83 86. 84. 80. 82 88 86. 0. 81. 83  
 62 88. 38. 82. 0 86 89. 81. 83. 85 87 90. 0. 84. 86 89 91. 89. 85. 90  
 63 90. 0. 90. 82 94 91. 0. 91. 89 95 92. 88. 94 96 93. 89. 91  
 95 0. 93. 95

\*\*\*\*\* DATA NAME= \*DISK \* BASE OF \*CYLINDER-CREATED WITH ACTIVE SIDE TOWARD +Z AXIS

SURFACE SPECIFICATIONS-

NO OF X-SECTIONS = 1 NO OF X-SECTION BOUNDARY DIVISIONS = 32

LOCATION OF VERTICAL CENTERLINE, X=0. \* Y=0.

X-SECTION NO. X-AXIS RADIUS X-AXIS RADIUS ELEVATION ABOVE XY PLANE  
 1 0.1000000 01 0.1000000 01 0.

THE FOLLOWING INTERNALLY GENERATED SURFACE DATA RESULTED FROM THE ABOVE SPECIFICATIONS-

POINT	X	Y	Z	POINT	X	Y	Z
1	0.100000	01	0.	33	0.10000000	01	0.
2	0.277163	01	0.	34	0.284235	01	0.
3	0.277163	01	0.118050	35	0.284235	01	0.118050
4	0.212130	01	0.212130	36	0.166671	01	0.284235
5	0.212130	01	0.	37	0.166671	01	0.284235
6	0.111757	01	0.300000	38	0.166671	01	0.284235
7	0.111757	01	0.	39	0.166671	01	0.284235
8	0.111757	01	0.	40	0.166671	01	0.284235
9	0.111757	01	0.	41	0.166671	01	0.284235
10	0.111757	01	0.	42	0.166671	01	0.284235
11	0.111757	01	0.	43	0.166671	01	0.284235
12	0.111757	01	0.	44	0.166671	01	0.284235
13	0.111757	01	0.	45	0.166671	01	0.284235
14	0.111757	01	0.	46	0.166671	01	0.284235
15	0.111757	01	0.	47	0.166671	01	0.284235
16	0.111757	01	0.	48	0.166671	01	0.284235
17	0.111757	01	0.	49	0.166671	01	0.284235
18	0.111757	01	0.	50	0.166671	01	0.284235
19	0.111757	01	0.	51	0.166671	01	0.284235
20	0.111757	01	0.	52	0.166671	01	0.284235
21	0.111757	01	0.	53	0.166671	01	0.284235
22	0.111757	01	0.	54	0.166671	01	0.284235
23	0.111757	01	0.	55	0.166671	01	0.284235
24	0.111757	01	0.	56	0.166671	01	0.284235
25	0.111757	01	0.	57	0.166671	01	0.284235
26	0.111757	01	0.	58	0.166671	01	0.284235
27	0.111757	01	0.	59	0.166671	01	0.284235
28	0.111757	01	0.	60	0.166671	01	0.284235
29	0.111757	01	0.	61	0.166671	01	0.284235
30	0.111757	01	0.	62	0.166671	01	0.284235
31	0.277163	01	0.118050	63	0.284235	01	0.
32	0.277163	01	0.	64	0.284235	01	0.

\*\*\*\*\* DATA NAME= \*DISK \* MOVES DISK TO SKINNED POSITION ON X-AXIS  
 TRANSFORMATION DATA-

FIGURE 29. Group D Sample Problems Program Results  
 (continued)

```

POINT  X      Y      Z      POINT  X      Y      Z
1  0.172800E 02  0.100000E 01  0.400000E 01  0.
25  0.100000E 02 -0.700000E 01  0.

```

\*\*\*\*\* DATA NAME= \*OTDSK0 \* FLIPS 3CISK0 AROUND SO THAT ACTIVE SIDE SEES 3DINCEOTDSK0

TRANSFORMATION DATA-

```

POINT  X      Y      Z      POINT  X      Y      Z
1  0.400000E 01  0.100000E 01  0.100000E 01
25  0.700000E 01 -0.200000E 01  0.100000E 01

```

FIGURE 29. Group D Sample Problems Program Results  
(continued)

NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (DI)→A.TOURS.11/1/63

RUN NO.	I	DATA USED FOR THIS RUN		SURFACE 2 SILHOUETTE COMPUTED FROM MAPPING POINT SHOWN	
		ABSCISSA CYCLING → 01000000	→ 1°	→ 1°	→ 1°
MAPPING LINE PT					
1 1	1	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 76 77			
1 2	2	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
1 3	3	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
1 4	4	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
1 5	5	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
1 6	6	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
1 7	7	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
2 1	1	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
2 2	2	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
2 3	3	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
2 4	4	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
2 5	5	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
2 6	6	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
2 7	7	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
3 1	1	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
3 2	2	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			
3 3	3	0 12 15 18 21 20 32 22 19 16 13 10 7 4 1 94 91 88 85 82 79 80 83			

FIGURE 29. Group D Sample Problems Program Results  
(continued)



6	1	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70
7	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
8	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
9	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
10	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
11	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
12	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
13	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
14	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
15	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
16	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
17	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
18	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
19	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
20	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
21	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
22	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
23	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
24	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
25	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
26	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
27	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
28	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
29	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
30	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
31	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
32	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
33	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
34	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
35	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
36	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
37	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
38	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
39	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
40	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
41	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
42	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
43	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
44	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
45	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
46	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
47	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
48	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
49	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	
50	1	7	10	13	16	19	22	25	28	31	34	37	40	43	46	49	52	55	58	61	64	67	70	

TOTAL TIME IN SLFAC = 9.837 SECONDS.

THE FORM FACTOR FROM SURFACE \*DISKCOFOS\* = TO SURFACE \*COYL\* \* = 0.18946

THE EXCHANGE COEFFICIENT TEA\* = 0.378491 02 SU UNITS

THE MAPPING AREA = 0.18940444 03 SU UNITS

THE AREA OF SURFACE \*DISKCOFOS\* = 0.18977256 03 SU UNITS.

THE AREA OF SURFACE \*COYL\* \* = 0.18927026 03 SU UNITS.

WARNING-BARREL IS MORE THAN 1 PERCENT DIFFERENCE FROM THE AREA IN SURFACE \*DISKCOFOS\* SEEN BY SURFACE \*COYL\* \*\* THIS MAY BE CAUSED BY WRONG SURFACE DATA IN THE SURFACE \*DISKCOFOS\* OR BY CRISSES A MAPPING LINE IN MORE THAN TWO PLACES, OR TOO COARSE INCREMENTS. THE FACTOR MAY BE INCORRECT.

THE FOLLOWING ARE THE (FIAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

\*\*\*\*\* DATA NAME= \*DISKCOFOS\*

FIGURE 29. Group D Sample Problems Program Results  
(continued)







LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

0.705322E-01	0.712180E-01	0.715384E-01	0.716875E-01	0.716778E-01	0.715095E-01
0.715078E-01	0.958000E-01	0.110071E-00	0.128763E-00	0.117009E-00	0.971605E-01
0.782575E-01	0.121181E-00	0.181047E-00	0.217763E-00	0.184452E-00	0.122625E-00
0.796008E-01	0.143289E-00	0.261013E-00	0.363596E-00	0.276150E-00	0.152891E-00
0.779010E-01	0.155632E-00	0.305749E-00	0.552303E-00	0.369274E-00	0.167908E-00
0.815718E-01	0.430074E-00	0.237469E-00	0.319074E-00	0.210681E-00	0.155458E-00
0.965181E-01	0.116069E-00	0.115531E-00	0.116652E-00	0.117180E-00	0.116966E-00
0.112201E-00					
0.116100E-00					

FIGURE 29. Group D Sample Problems Program Results  
(continued)

# NMA CONTACT II REPORT SAMPLE PROBLEMS FROM FIG. 101-A.A.TROUPS.11/1/63

RUN NO. 2 DATA USED FOR THIS RUN- \*DISKSCOTDSKC\*  
 \*DISKSCOTDSKC\*  
 \*DISKSCOTDSKC\*  
 \*DISKSCOTDSKC\*

THE FORM FACTOR FROM SURFACE \*DISKSCOTDSKC\* TO SURFACE \*DISKSCOTDSKC\* = 0.00955

THE EXCHANGE COEFFICIENT (FA) = 0.19888E 02 SQ UNITS

THE MAPPING AREA = 0.123045HE 03 SQ UNITS

ONLY A PART OF SURFACE \*DISKSCOTDSKC\*, COMPRISING AN AREA OF 0.13145HE 03 SQ UNITS,  
 SEES SURFACE \*DISKSCOTDSKC\*

THE AREA OF SURFACE \*DISKSCOTDSKC\* = 0.1907725E 03 SQ UNITS.

THE AREA OF SURFACE \*DISKSCOTDSKC\* = 0.2809501E 02 SQ UNITS.

WARNING-  
 THE MAPPING AREA IS MORE THAN 1 PERCENT DIFFERENT FROM THE AREA IN SURFACE \*DISKSCOTDSKC\* SEEN BY  
 THE SURFACE \*DISKSCOTDSKC\* ITSELF. THIS IS DUE TO THE SURFACE \*DISKSCOTDSKC\* BEING  
 CROSSED A MAPPING LINE IN MORE THAN TWO PLACES. OR TOO COARSE INCREMENTS. THE FACTOR MAY BE INCORRECT.

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

\*\*\*\*\* DATA NAME- \*DISKSCOTDSKC\*

POINT	X	Y	Z	POINT	X	Y	Z
1	0.	0.	0.	2	0.1000000E 01	0.0000000E 00	0.
2	0.0000000E 00	0.0000000E 00	0.	3	0.0000000E 00	0.0000000E 00	0.
3	0.0000000E 00	0.0000000E 00	0.	4	0.0000000E 00	0.0000000E 00	0.
4	0.0000000E 00	0.0000000E 00	0.	5	0.0000000E 00	0.0000000E 00	0.
5	0.0000000E 00	0.0000000E 00	0.	6	0.0000000E 00	0.0000000E 00	0.
6	0.0000000E 00	0.0000000E 00	0.	7	0.0000000E 00	0.0000000E 00	0.
7	0.0000000E 00	0.0000000E 00	0.	8	0.0000000E 00	0.0000000E 00	0.
8	0.0000000E 00	0.0000000E 00	0.	9	0.0000000E 00	0.0000000E 00	0.
9	0.0000000E 00	0.0000000E 00	0.	10	0.0000000E 00	0.0000000E 00	0.
10	0.0000000E 00	0.0000000E 00	0.	11	0.0000000E 00	0.0000000E 00	0.
11	0.0000000E 00	0.0000000E 00	0.	12	0.0000000E 00	0.0000000E 00	0.
12	0.0000000E 00	0.0000000E 00	0.	13	0.0000000E 00	0.0000000E 00	0.
13	0.0000000E 00	0.0000000E 00	0.	14	0.0000000E 00	0.0000000E 00	0.
14	0.0000000E 00	0.0000000E 00	0.	15	0.0000000E 00	0.0000000E 00	0.
15	0.0000000E 00	0.0000000E 00	0.	16	0.0000000E 00	0.0000000E 00	0.
16	0.0000000E 00	0.0000000E 00	0.	17	0.0000000E 00	0.0000000E 00	0.
17	0.0000000E 00	0.0000000E 00	0.	18	0.0000000E 00	0.0000000E 00	0.

FIGURE 29. Group D Sample Problems Program Results  
 (continued)

10 -0.246270E 01 0.151400E 02 0.  
21 -0.467722E 01 0.116031E 02 0.  
20 -0.409612E 01 0.150168E 02 0.

\*\*\*\*\* DATA NAME= \*SDISK97CISK\*

```

PRINT X Y Z
1 0.447597E 01 0.072117E 01 0.150000E 02
2 0.400740E 01 0.050025E 01 0.436010E 01
3 0.447597E 01 0.072117E 01 0.150000E 02
4 0.400740E 01 0.050025E 01 0.436010E 01
5 0.447597E 01 0.072117E 01 0.150000E 02
6 0.400740E 01 0.050025E 01 0.436010E 01
7 0.428229E 01 0.458167E 01 0.346010E 01
8 0.380063E 01 0.151322E 01 0.151322E 01
9 0.380063E 01 0.151322E 01 0.151322E 01
10 0.280401E 01 0.585027E 01 0.257345E 01
11 0.317455E 01 0.351028E 01 0.257345E 01
12 0.317455E 01 0.351028E 01 0.257345E 01
13 0.150000E 01 0.255580E 01 0.160310E 01
14 0.150000E 01 0.255580E 01 0.160310E 01
15 0.150000E 01 0.255580E 01 0.160310E 01
16 0.282722E 00 0.752207E 01 0.138485E 01
17 0.282722E 00 0.752207E 01 0.138485E 01
18 0.282722E 00 0.752207E 01 0.138485E 01
19 0.118855E 00 0.221048E 01 0.188217E 01
20 0.118855E 00 0.221048E 01 0.188217E 01
21 0.118855E 00 0.221048E 01 0.188217E 01
22 0.400740E 01 0.050025E 01 0.436010E 01
23 0.400740E 01 0.050025E 01 0.436010E 01
24 0.400740E 01 0.050025E 01 0.436010E 01
25 0.160657E 01 0.116031E 02 0.544310E 01
26 0.160657E 01 0.116031E 02 0.544310E 01
27 0.160657E 01 0.116031E 02 0.544310E 01
28 0.160657E 01 0.116031E 02 0.544310E 01
29 0.400740E 01 0.050025E 01 0.436010E 01
30 0.400740E 01 0.050025E 01 0.436010E 01
31 0.400740E 01 0.050025E 01 0.436010E 01
32 0.400740E 01 0.050025E 01 0.436010E 01
33 0.400740E 01 0.050025E 01 0.436010E 01
34 0.400740E 01 0.050025E 01 0.436010E 01
35 0.400740E 01 0.050025E 01 0.436010E 01
36 0.400740E 01 0.050025E 01 0.436010E 01
37 0.400740E 01 0.050025E 01 0.436010E 01
38 0.400740E 01 0.050025E 01 0.436010E 01
39 0.400740E 01 0.050025E 01 0.436010E 01
40 0.400740E 01 0.050025E 01 0.436010E 01
41 0.400740E 01 0.050025E 01 0.436010E 01
42 0.400740E 01 0.050025E 01 0.436010E 01
43 0.400740E 01 0.050025E 01 0.436010E 01
44 0.400740E 01 0.050025E 01 0.436010E 01
45 0.400740E 01 0.050025E 01 0.436010E 01
46 0.400740E 01 0.050025E 01 0.436010E 01
47 0.400740E 01 0.050025E 01 0.436010E 01
48 0.400740E 01 0.050025E 01 0.436010E 01
49 0.400740E 01 0.050025E 01 0.436010E 01
50 0.400740E 01 0.050025E 01 0.436010E 01
51 0.400740E 01 0.050025E 01 0.436010E 01
52 0.400740E 01 0.050025E 01 0.436010E 01
53 0.400740E 01 0.050025E 01 0.436010E 01
54 0.400740E 01 0.050025E 01 0.436010E 01
55 0.400740E 01 0.050025E 01 0.436010E 01
56 0.400740E 01 0.050025E 01 0.436010E 01
57 0.400740E 01 0.050025E 01 0.436010E 01
58 0.400740E 01 0.050025E 01 0.436010E 01
59 0.400740E 01 0.050025E 01 0.436010E 01
60 0.400740E 01 0.050025E 01 0.436010E 01
61 0.400740E 01 0.050025E 01 0.436010E 01
62 0.400740E 01 0.050025E 01 0.436010E 01
63 0.400740E 01 0.050025E 01 0.436010E 01
64 0.400740E 01 0.050025E 01 0.436010E 01
65 0.400740E 01 0.050025E 01 0.436010E 01
66 0.400740E 01 0.050025E 01 0.436010E 01
67 0.400740E 01 0.050025E 01 0.436010E 01
68 0.400740E 01 0.050025E 01 0.436010E 01
69 0.400740E 01 0.050025E 01 0.436010E 01
70 0.400740E 01 0.050025E 01 0.436010E 01
71 0.400740E 01 0.050025E 01 0.436010E 01
72 0.400740E 01 0.050025E 01 0.436010E 01
73 0.400740E 01 0.050025E 01 0.436010E 01
74 0.400740E 01 0.050025E 01 0.436010E 01
75 0.400740E 01 0.050025E 01 0.436010E 01
76 0.400740E 01 0.050025E 01 0.436010E 01
77 0.400740E 01 0.050025E 01 0.436010E 01
78 0.400740E 01 0.050025E 01 0.436010E 01
79 0.400740E 01 0.050025E 01 0.436010E 01
80 0.400740E 01 0.050025E 01 0.436010E 01
81 0.400740E 01 0.050025E 01 0.436010E 01
82 0.400740E 01 0.050025E 01 0.436010E 01
83 0.400740E 01 0.050025E 01 0.436010E 01
84 0.400740E 01 0.050025E 01 0.436010E 01
85 0.400740E 01 0.050025E 01 0.436010E 01
86 0.400740E 01 0.050025E 01 0.436010E 01
87 0.400740E 01 0.050025E 01 0.436010E 01
88 0.400740E 01 0.050025E 01 0.436010E 01
89 0.400740E 01 0.050025E 01 0.436010E 01
90 0.400740E 01 0.050025E 01 0.436010E 01
91 0.400740E 01 0.050025E 01 0.436010E 01
92 0.400740E 01 0.050025E 01 0.436010E 01
93 0.400740E 01 0.050025E 01 0.436010E 01
94 0.400740E 01 0.050025E 01 0.436010E 01
95 0.400740E 01 0.050025E 01 0.436010E 01
96 0.400740E 01 0.050025E 01 0.436010E 01
97 0.400740E 01 0.050025E 01 0.436010E 01
98 0.400740E 01 0.050025E 01 0.436010E 01
99 0.400740E 01 0.050025E 01 0.436010E 01
100 0.400740E 01 0.050025E 01 0.436010E 01

```

COORDINATES OF POINTS ON BOUNDARY OF SURF \*SDISK97CISK\* FOR EACH Y INTERVAL

```

X-LEFT X-RIGHT Y X-LEFT X-RIGHT Y
-0. 0.447597E 01 0.072117E 01 0.150000E 02 0.447597E 01 0.072117E 01 0.150000E 02
-0.161003E 01 0.710321E 01 0.530762E 01 -0.161003E 01 0.710321E 01 0.530762E 01
-0.172017E 01 0.710321E 01 0.530762E 01 -0.172017E 01 0.710321E 01 0.530762E 01
-0.176008E 01 0.459187E 00 0.150220E 02 -0.176008E 01 0.459187E 00 0.150220E 02

```

NO. OF HORIZONTAL INCREMENTS= 6 NO. OF VERTICAL INCREMENTS= 6

THE FOLLOWING ARE PLATE POINT CONFIGURATION FACIAMS COMPUTED FOR THIS RUN  
LAST TWO LINE FIRST FROM X-LEFT TO X-RIGHT.

0.437204E-08 0.145160E-03 0.246096E-05 0.370251E-35 0.500246E-02 0.610883E-03

FIGURE 29. Group B Sample Problems Program Results  
(continued)

C-7228304E-03	0.6225217E-02	0.1501604E-01	0.2430070E-01	0.3101249E-01	0.3531677E-01
C-7228304E-03	0.3716789E-01	0.1256211E-00	0.1871291E-00	0.1659108E-00	0.1140264E-00
C-7228304E-03	0.1054518E-00	0.4651275E-00	0.5049026E-00	0.3690750E-00	0.2116433E-00
C-7228304E-03	0.4496273E-01	0.2592187E-00	0.4122213E-00	0.3477228E-00	0.2200286E-00
C-7228304E-03	0.9057742E-02	0.5687003E-01	0.8732407E-01	0.1281245E-00	0.13242457E-00
C-7228304E-03	0.1210962E-01	0.1161268E-01	0.1573643E-01	0.1600811E-01	0.1863135E-01

FIGURE 29. Group D Sample Problems Program Results  
(continued)

#### SAMPLE PROBLEM GROUP E

The capability of obtaining form factors to spheres in any position relative to Surface 1 is demonstrated, Figure 30. Closed form configuration factor solutions are utilized, enabling very rapid computations. The data sheets are presented in Figure 31 and the results in Figure 32.

##### Problem 1E

The factor from a rectangle, 1PLAT8, to a sphere, 7SPH1, fully above the plane of 1PLAT8 (Case I) is requested as Run #1. The configuration factor solution in this case is extremely simple (see Appendix E), which, in addition to the coarse mapping of 1PLAT8, accounts for the short computational time.

##### Problem 2E

The factor from 1PLAT8 to 7SPH2 is requested. The sphere is the same size as 7SPH1, except part or the lower half of the sphere is below, and outside of, the surface of 1PLAT8 (Case II). The results are shown as Run #2.

##### Problem 3E

A larger sphere, 7SPH3, is located with part of the upper half of the sphere below the surface of 1PLAT8 (Case III). The results are shown as Run #3.

##### Problem 4E

The program will also compute the factor to a sphere which is embedded in Surface 1, illustrated by 7SPH2 and 1PLAT7. However, no attempt is made to determine what part of 1PLAT7 sees the sphere; when a mapping point on Surface 1 appears inside the sphere, a configuration factor of zero is returned and integrated along with the other computed factors. Therefore, in Run #4 we see no indication that 1PLAT7 is bisected by 7SPH2, although in reality it is. The problem is handled in this way because of the extreme complexity of the general determination of that part of Surface 1 not seen by the sphere.

##### Problem 5E

The trivial case of the sphere completely below Surface 1 is illustrated by Run #5.

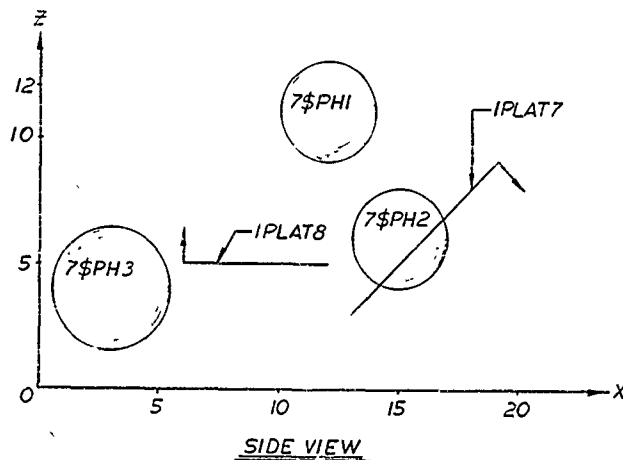
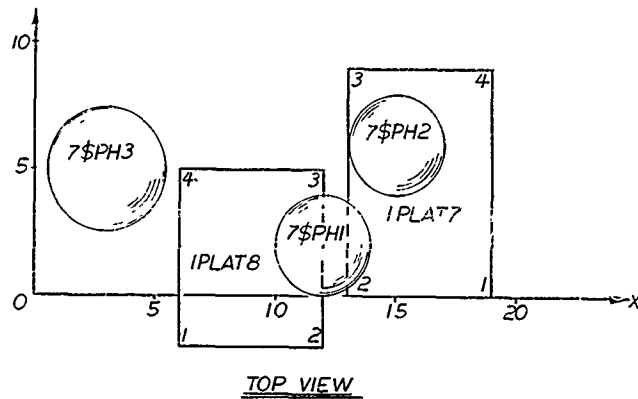


FIGURE 30. Group E Sample Problems Geometry



FORTRAN FIXED 10 DIGIT DECIMAL DATA			
DECK NO.	PROGRAMMER	DATE	PAGE 33 of 34 JOB NO. 2222-30
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
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100			

FORTRAN FIXED 10 DIGIT DECIMAL DATA			
DECK NO.	PROGRAMMER	DATE	PAGE 33 of 34 JOB NO. 2222-30
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1			
2			
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FIGURE 31. Group E Sample Problems Input Data Code Sheets

# FORTPAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE 21 of 36	JOB NO. 2023 30
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1.0				
2.0				
3.0				
4.0				
5.0				
6.0				
7.0				
8.0				
9.0				
10.0				
11.0				
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21.0				
22.0				
23.0				
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27.0				
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29.0				
30.0				

# FORTTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE 21 of 36	JOB NO. 2023 30
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1.0				
2.0				
3.0				
4.0				
5.0				
6.0				
7.0				
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30.0				

FIGURE 31. Group E Sample Problems Input Data Codo Sheets  
(continued)

**FORTTRAN FIXED 10 DIGIT DECIMAL DATA**

DECK NO. \_\_\_\_\_ PROGRAMMER \_\_\_\_\_ DATE \_\_\_\_\_ PAGE 35 of 38 JOB NO. 2222-M

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
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FIGURE 31. Group E Sample Problems Input Data Code Sheets  
(continued)

NAA SPACE AND INFORMATION SYSTEMS DIVISION  
T-4 PROJECT RADIANT-INTERCHANGE CONFIGURATION FACTOR PROGRAM  
CONFAC II

NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (E)-K-A-T-O-U-P-S, 11/11/63

INPUT DATA

```

***** DATA NAME= *IPLAT7 * SKETCHED RECTANGULAR PLATE IN 1ST QUADRANT.
POINT X Y Z POINT X Y Z
1 0.1970711E 02 0. 0.822491E 01-----INTERVALLY GENERATED ORIENTATION VECTOR) 2
2 0.1900000E 02 0. 0.903000E 01 0.190000E 02 0.190000E 01 0.400000E 01
3 0.1100000E 02 0.900000E 01 0.300000E 01 0.190000E 02 0.900000E 01 0.900000E 01

***** DATA NAME= *IPLAT8 * RECT PLATE PARALLEL TO XY PLANE, 1ST AND 4TH QUADRANTS.
POINT X Y Z POINT X Y Z
1 0.60000E 01 -0.20000E 01 0.60000E 01-----INTERVALLY GENERATED ORIENTATION VECTOR) 2
2 0.60000E 01 0.20000E 01 0.60000E 01 0.60000E 02 0.20000E 01 0.40000E 01
3 0.12000E 02 0.20000E 01 0.20000E 01 0.60000E 01 0.60000E 01 0.90000E 01

***** DATA NAME= *TSPH1
SPHERE SPECIFICATIONS-
RADIUS = 0.200000E 01
COORDINATES OF CENTER----- X = 0.100000E 02 Y = 0.200000E 01 Z = 0.110000E 02

***** DATA NAME= *TSPH2
SPHERE SPECIFICATIONS-
RADIUS = 0.200000E 01
COORDINATES OF CENTER----- X = 0.150000E 02 Y = 0.600000E 01 Z = 0.600000E 01

```

FIGURE 32. Group E Sample Problems Program Results  
(13 pages)

```

***** DATA NAME= *TSPH3
SPHERE SPECIFICATIONS=
RADIUS = 0.250000E 01
CONSTANTS OF CENTER= X = 0.300000E 01 Y = 0.500000E 01 Z = 0.400000E 01

```

FIGURE 32. Group 2 Sample Problems Program Results  
(continued)

# NIA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (E)-C.A.TROUPS.11/1/63

RUN NO. 1 DATA USED FOR THIS RUN: \*PLATB\*7SPH1 \*  
 \*D 1\* 1\*

TOTAL TIME IS 15.64C = 0.021 SECONDS.  
 THE FORM FACTOR FROM SURFACE \*PLATB \* TO SURFACE \*7SPH1 \* = 0.06310  
 THE EXCHANGE COEFFICIENT (FA) = 0.28807E 01 SQ UNITS

THE MAPPING AREA = 0.4250000E 02 SQ UNITS

THE AREA OF SURFACE \*PLATB \* = 0.4200000E 02 SQ UNITS.

THE AREA OF SURFACE \*7SPH1 \* = 0.5026548E 02 SQ UNITS.

THE FOLLOWING ARE THE (FICIAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION:

```

***** DATA NAME= *PLATB1 *
POINT 0. X Y Z POINT X Y Z
1 0. 0. 0. 0.1000000E 01 --- (INTERNALLY GENERATED ORIENTATION VECTOR)
2 0.4000000E 01 0.7000000E 01 0.
3 0.6000000E 01 0.7000000E 01 0.

```

```

***** DATA NAME= *7SPH1 *
POINT 0. X Y Z POINT X Y Z
1 0.6000000E 01 0.4000000E 01 0.4000000E 01
2 0.6000000E 01 0.4000000E 01 0.4000000E 01
3 0.6000000E 01 0.4000000E 01 0.4000000E 01
4 0.6000000E 01 0.4000000E 01 0.4000000E 01
5 0.6000000E 01 0.4000000E 01 0.4000000E 01
6 0.6000000E 01 0.4000000E 01 0.4000000E 01
7 0.6000000E 01 0.4000000E 01 0.4000000E 01
8 0.6000000E 01 0.4000000E 01 0.4000000E 01
9 0.6000000E 01 0.4000000E 01 0.4000000E 01
10 0.6000000E 01 0.4000000E 01 0.4000000E 01
11 0.6000000E 01 0.4000000E 01 0.4000000E 01
12 0.6000000E 01 0.4000000E 01 0.4000000E 01
13 0.6000000E 01 0.4000000E 01 0.4000000E 01
14 0.6000000E 01 0.4000000E 01 0.4000000E 01
15 0.6000000E 01 0.4000000E 01 0.4000000E 01
16 0.6000000E 01 0.4000000E 01 0.4000000E 01
17 0.6000000E 01 0.4000000E 01 0.4000000E 01
18 0.6000000E 01 0.4000000E 01 0.4000000E 01
19 0.6000000E 01 0.4000000E 01 0.4000000E 01
20 0.6000000E 01 0.4000000E 01 0.4000000E 01
21 0.6000000E 01 0.4000000E 01 0.4000000E 01
22 0.6000000E 01 0.4000000E 01 0.4000000E 01
23 0.6000000E 01 0.4000000E 01 0.4000000E 01
24 0.6000000E 01 0.4000000E 01 0.4000000E 01
25 0.6000000E 01 0.4000000E 01 0.4000000E 01
26 0.6000000E 01 0.4000000E 01 0.4000000E 01
27 0.6000000E 01 0.4000000E 01 0.4000000E 01
28 0.6000000E 01 0.4000000E 01 0.4000000E 01
29 0.6000000E 01 0.4000000E 01 0.4000000E 01
30 0.6000000E 01 0.4000000E 01 0.4000000E 01
31 0.6000000E 01 0.4000000E 01 0.4000000E 01
32 0.6000000E 01 0.4000000E 01 0.4000000E 01
33 0.6000000E 01 0.4000000E 01 0.4000000E 01
34 0.6000000E 01 0.4000000E 01 0.4000000E 01
35 0.6000000E 01 0.4000000E 01 0.4000000E 01
36 0.6000000E 01 0.4000000E 01 0.4000000E 01
37 0.6000000E 01 0.4000000E 01 0.4000000E 01
38 0.6000000E 01 0.4000000E 01 0.4000000E 01
39 0.6000000E 01 0.4000000E 01 0.4000000E 01
40 0.6000000E 01 0.4000000E 01 0.4000000E 01
41 0.6000000E 01 0.4000000E 01 0.4000000E 01
42 0.6000000E 01 0.4000000E 01 0.4000000E 01
43 0.6000000E 01 0.4000000E 01 0.4000000E 01
44 0.6000000E 01 0.4000000E 01 0.4000000E 01
45 0.6000000E 01 0.4000000E 01 0.4000000E 01
46 0.6000000E 01 0.4000000E 01 0.4000000E 01
47 0.6000000E 01 0.4000000E 01 0.4000000E 01
48 0.6000000E 01 0.4000000E 01 0.4000000E 01
49 0.6000000E 01 0.4000000E 01 0.4000000E 01
50 0.6000000E 01 0.4000000E 01 0.4000000E 01
51 0.6000000E 01 0.4000000E 01 0.4000000E 01
52 0.6000000E 01 0.4000000E 01 0.4000000E 01
53 0.6000000E 01 0.4000000E 01 0.4000000E 01
54 0.6000000E 01 0.4000000E 01 0.4000000E 01
55 0.6000000E 01 0.4000000E 01 0.4000000E 01
56 0.6000000E 01 0.4000000E 01 0.4000000E 01
57 0.6000000E 01 0.4000000E 01 0.4000000E 01
58 0.6000000E 01 0.4000000E 01 0.4000000E 01
59 0.6000000E 01 0.4000000E 01 0.4000000E 01
60 0.6000000E 01 0.4000000E 01 0.4000000E 01
61 0.6000000E 01 0.4000000E 01 0.4000000E 01
62 0.6000000E 01 0.4000000E 01 0.4000000E 01
63 0.6000000E 01 0.4000000E 01 0.4000000E 01
64 0.6000000E 01 0.4000000E 01 0.4000000E 01
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66 0.6000000E 01 0.4000000E 01 0.4000000E 01
67 0.6000000E 01 0.4000000E 01 0.4000000E 01
68 0.6000000E 01 0.4000000E 01 0.4000000E 01
69 0.6000000E 01 0.4000000E 01 0.4000000E 01
70 0.6000000E 01 0.4000000E 01 0.4000000E 01
71 0.6000000E 01 0.4000000E 01 0.4000000E 01
72 0.6000000E 01 0.4000000E 01 0.4000000E 01
73 0.6000000E 01 0.4000000E 01 0.4000000E 01
74 0.6000000E 01 0.4000000E 01 0.4000000E 01
75 0.6000000E 01 0.4000000E 01 0.4000000E 01
76 0.6000000E 01 0.4000000E 01 0.4000000E 01
77 0.6000000E 01 0.4000000E 01 0.4000000E 01
78 0.6000000E 01 0.4000000E 01 0.4000000E 01
79 0.6000000E 01 0.4000000E 01 0.4000000E 01
80 0.6000000E 01 0.4000000E 01 0.4000000E 01
81 0.6000000E 01 0.4000000E 01 0.4000000E 01
82 0.6000000E 01 0.4000000E 01 0.4000000E 01
83 0.6000000E 01 0.4000000E 01 0.4000000E 01
84 0.6000000E 01 0.4000000E 01 0.4000000E 01
85 0.6000000E 01 0.4000000E 01 0.4000000E 01
86 0.6000000E 01 0.4000000E 01 0.4000000E 01
87 0.6000000E 01 0.4000000E 01 0.4000000E 01
88 0.6000000E 01 0.4000000E 01 0.4000000E 01
89 0.6000000E 01 0.4000000E 01 0.4000000E 01
90 0.6000000E 01 0.4000000E 01 0.4000000E 01
91 0.6000000E 01 0.4000000E 01 0.4000000E 01
92 0.6000000E 01 0.4000000E 01 0.4000000E 01
93 0.6000000E 01 0.4000000E 01 0.4000000E 01
94 0.6000000E 01 0.4000000E 01 0.4000000E 01
95 0.6000000E 01 0.4000000E 01 0.4000000E 01
96 0.6000000E 01 0.4000000E 01 0.4000000E 01
97 0.6000000E 01 0.4000000E 01 0.4000000E 01
98 0.6000000E 01 0.4000000E 01 0.4000000E 01
99 0.6000000E 01 0.4000000E 01 0.4000000E 01
100 0.6000000E 01 0.4000000E 01 0.4000000E 01

```

FIGURE 32. Group E Sample Problems Program Results (continued)

0. 0.6000000E 0. 0.2333333E 01 0. 0.6000000E 01 0.5000000E 01  
 0. 0.6000000E 01 0.4666667E 01 0. 0.6000000E 01 0.3933333E 01  
 0. 0.6000000E 01 0.7000000E 01

NO. OF HORIZONTAL INCREMENTS= 6 NO. OF VERTICAL INCREMENTS= 6

THE FOLLOWING ARE PLANE PRINT CONFIGURATION FACTORS COMPUTED FOR THIS RUN  
 LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

0.3007282E-01 0.35510.8E-01 0.4280040E-01 0.5037517E-01 0.5727202E-01 0.6220101E-01  
 0.4400387E-01 0.4184837E-01 0.5160394E-01 0.5215214E-01 0.7210618E-01 0.7943108E-01  
 0.3223364E-01 0.4712000E-01 0.5919787E-01 0.7267287E-01 0.8577959E-01 0.9566443E-01  
 0.9938667E-01 0.500606E-01 0.6354500E-01 0.7884667E-01 0.9398584E-01 1.0556551E-01  
 0.1099637E-01 0.4982959E-01 0.6319190E-01 0.7834117E-01 0.9330887E-01 1.0474442E-01  
 0.392274E-01 0.4448105E-01 0.5826450E-01 0.7136197E-01 0.8405444E-01 0.9359800E-01  
 0.364851E-01 0.4097927E-01 0.5037517E-01 0.6048123E-01 0.6977084E-01 0.7692624E-01  
 0.372184E-01 0.4097927E-01 0.5037517E-01 0.6048123E-01 0.6977084E-01 0.7692624E-01

FIGURE 32. Group 3 Sample Problems Program Results  
 (continued)

# NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (E)-K-A-TOUP'S,11/1/63

RUN NO. 2 DATA USED FOR THIS RUN- \*IPLAT8 \*TSPH2 \*  
 \*D 1\* 1\*

TOTAL TIME IN SILFAC = 0.058 SECONDS.

THE FORM FACTOR FROM SURFACE \*IPLAT8 \* TO SURFACE \*TSPH2 \* = 0.31426

THE EXCHANGE COEFFICIENT (FA) = 0.59895E 00 SQ UNITS

THE MAPPING AREA = 0.420000E 02 SQ UNITS

THE AREA OF SURFACE \*IPLAT8 \* = 0.420000E 02 SQ UNITS.

ONLY A PART OF SURFACE \*TSPH2 \* COMPRISING AN AREA OF 0.376931E 02 SQ UNITS.  
 SEES SURFACE \*IPLAT8 \*

THE AREA OF SURFACE \*TSPH2 \* = 0.5026548E 02 SQ UNITS.

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

\*\*\*\*\* DATA NAME- \*IPLAT8 \*

POINT	X	Y	Z	POINT	X	Y	Z
1	0.	-0.	0.	1	0.100000E 01	0.	0.
2	0.600000E 01	0.700000E 01	0.	2	0.600000E 01	-0.	0.
3	0.600000E 01	0.700000E 01	0.	3	0.600000E 01	0.100000E 01	0.

\*\*\*\*\* DATA NAME- \*TSPH2 \*

POINT	X	Y	Z	POINT	X	Y	Z
1	0.900000E 01	0.800000E 01	0.100000E 01	1	0.	0.	0.

COORDINATES OF POINTS ON BOUNDARY OF SURF \*IPLAT8 \* FOR EACH Y INTERVAL

FIGURE 32. Group 3 Sample Problems Program Results  
 (continued)



	X-LEFT	X-RIGHT	Y	X-LEFT	X-RIGHT	Y
0.	0.600000E-01	0.600000E-01	0.233333E-01	0.	0.600000E-01	0.116666E-01
0.	0.600000E-01	0.600000E-01	0.466666E-01	0.	0.600000E-01	0.350000E-01
0.	0.600000E-01	0.600000E-01	0.700000E-01	0.	0.600000E-01	0.533333E-01

NO. OF HORIZONTAL INCREMENTS= 6 NO. OF VERTICAL INCREMENTS= 6

THE FOLLOWING ARE PLANE POINT CONFIGURATION FACTORS COMPUTED FOR THIS RUN  
LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

0.265334E-02	0.427480E-02	0.359177E-02	0.427204E-02	0.508021E-02	0.592181E-02
0.261723E-02	0.357257E-02	0.456101E-02	0.566616E-02	0.700287E-02	0.854221E-02
0.290842E-02	0.453304E-02	0.583173E-02	0.755584E-02	0.980659E-02	0.126333E-01
0.101774E-01	0.551498E-02	0.737242E-02	0.100292E-01	0.138269E-01	0.191558E-01
0.159234E-01	0.652568E-02	0.909130E-02	0.110394E-01	0.192640E-01	0.292897E-01
0.419331E-01	0.746092E-02	0.107423E-01	0.161638E-01	0.236495E-01	0.433551E-01
0.582823E-01	0.802771E-02	0.193474E-01	0.185889E-01	0.311208E-01	0.575082E-01
0.783234E-01					
0.973354E-01					
0.121932E-01					

FIGURE 32. Group 2 Sample Problems Program Results  
(continued)

ALA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (E)-K.A.-LIPS,11/1/63

```

RUN NO. 3 DATA USED FOR THIS RUN- *PLATB *TSPH3 *
      *O 1* 1*

TOTAL TIME IN SELFAC = 0.058 SECONDS.
THE FIRM FACTOR FROM SURFACE *PLATB * TO SURFACE *TSPH3 * = 0.00502
THE EXCHANGE COEFFICIENT (FA) = 0.21089E-00 50 UNITS
      THE MAPPING AREA = 0.4200000E 02 50 UNITS
THE AREA OF SURFACE *PLATB * = 0.4200000E 02 50 UNITS.

ONLY A PART OF SURFACE *TSPH3 *
SEES SURFACE *PLATB *
      *% COMPRISING AN AREA OF 0.2356194E 02 50 UNITS.
THE AREA OF SURFACE *TSPH3 * = 0.1653982E 02 50 UNITS.

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

***** DATA NAME- *PLATB *
POINT 0. X -0. Y 0. Z 0. POINT X Y Z
      1 0. 0. 0. 0.1000000E 01---(INTERNALLY GENERATED ORIENTATION VECTOR)
      2 0. 0. 0. 0.6000000E 01 0. 0.
      3 0. 0. 0. 0.7000000E 02 0. 0.

***** DATA NAME- *TSPH3 *
POINT 0. X Y Z
      1 -0.3000000E 01 0.7000000E 01 -0.1000000E 01 POINT X Y Z
COORDINATES OF POINTS ON BOUNDARY OF SURF *PLATB * FOR EACH Y INTERVAL

```

FIGURE 32. Group E Sample Problems Program Results  
(continued)

	X-LEFT	X-RIGHT	Y	X-LEFT	X-RIGHT	Y
0*	0.6000000E 01	0*	0*	0.6000000E 01	0.1166667E 01	
0*	0.6000000E 01	0*	0.2333333E 01	0.6000000E 01	0.1166667E 01	
0*	0.6000000E 01	0.4444444E 01	0*	0.6000000E 01	0.5000000E 01	
0*	0.6000000E 01	0.4444444E 01	0*	0.6000000E 01	0.5000000E 01	
0*	0.6000000E 01	0.7000000E 01	0*	0.6000000E 01	0.5833333E 01	

NO. OF HORIZONTAL INCREMENTS= 6 NO. OF VERTICAL INCREMENTS= 4

THE FOLLOWING ARE PLANE POINT CONFIGURATION FACTORS COMPUTED FOR THIS RUN  
LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

0.2134555E-02	0.1946E-02	0.1589449E-02	0.1325320E-02	0.8516631E-03
0.6218785E-03	0.1797E-02	0.2252464E-02	0.1332033E-02	0.1033080E-02
0.1474436E-02	0.4520665E-02	0.3233146E-02	0.2329393E-02	0.1267144E-02
0.6810705E-03	0.7178651E-02	0.4662313E-02	0.3080575E-02	0.1517988E-02
0.1115075E-02	0.1133943E-01	0.6367547E-02	0.3901600E-02	0.1752771E-02
0.1474436E-02	0.1599822E-02	0.8051566E-02	0.2553004E-02	0.1929431E-02
0.1345755E-02	0.1836423E-01	0.8945356E-02	0.4060947E-02	0.1938781E-02
0.1335305E-02		0.4679231E-02		

NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (E)-X.A.TOU<11/1/63

RUN NO. 4 DATA USED FOR THIS RUN- \*IPLAT7\*7SPH2 \*  
\*0 3 3\*

TOTAL TIME IN SILENCE = 0.393 SECONDS.

THE FORN FACTOR FROM SURFACE \*IPLAT7 \* TO SURFACE \*7SPH2 \* = 0.02446

THE EXCHANGE COEFFICIENT (FA) = 0.186832 01 SQ UNITS

THE MAPPING AREA = 0.7636752E 02 SQ UNITS

THE AREA OF SL-FAVE \*IPLAT7 \* = 0.7636752E 02 SQ UNITS.

ONLY A PART OF SURFACE \*7SPH2 \* COMPRISING AN AREA OF 0.1624699E 02 SQ UNITS.

SEES SURFACE \*IPLAT7 \*

THE AREA OF SURFACE \*7SPH2 \* = 0.5026548E 02 SQ UNITS.

THE FOLLOWING ARE THE (FIAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

```

***** DATA NAME= *IPLAT7 *
POINT 0. X -0. Y 0.9999999E 00---(INTERNALLY GENERATED ORIENTATION VECTOR) Z
1 -0. 0. 0. 2 0.8485281E 01 -0. 0.
3 0.8485281E 01 0.8999999E 01 0. 4 -0. 0.3999999E 01 0.

***** DATA NAME= *7SPH2 *
POINT 0. X 0. Y 0.5999999E 01 -0.7071059E 00 POINT A Y Z
1 0.4949747E 01 0.5999999E 01 0.5999999E 01 0.5999999E 01 0.5999999E 01 0.5999999E 01 0.
COORDINATES OF POINTS ON BOUNDARY OF SURF *IPLAT7 * FOR EACH Y INTERVAL

```

FIGURE 32. Group 3 Sample Problems Program Results  
(continued)





0.1116397E-C0	0.7366526E-01	0.4717632E-01	0.3059036E-01	0.2040013E-01	0.1-04648E-01
0.3772698E-C2	0.4744630E-02	0.6155096E-02	0.4118316E-02	0.148811E-01	0.140248E-01
0.4031024E-C1	0.277861E-01	0.3712035E-01	0.4480520E-01	0.358155E-01	0.140248E-01
0.468510E-01	0.3712032E-01	0.277861E-01	0.2031023E-01	0.148811E-01	0.1088435E-01
0.322088E-C2	0.466008E-02	0.5123229E-02	0.4525123E-02	0.6375638E-02	0.1078056E-01
0.138556E-C1	0.175374E-01	0.2153340E-01	0.2513747E-01	0.2734619E-01	0.2734619E-01
0.652512E-C2	0.2153340E-01	0.175374E-01	0.1385566E-04	0.1078056E-01	0.8375805E-02

Figure 32. Group E Sample Problems Program Results  
(continued)

NONE OF SURFACE •PLAT7 • IS SEEN BY SURFACE •TSPH1 •

IF THE ABOVE RESULT IS UNEXPECTED, DO NOT BECOME LARNED- IT HAPPENS TO THE BEST OF US. JUST CHECK YOUR DATA-SPECIFICALLY BE SURE THAT YOU ENTERED ALL POINTS IN COUNTERCLOCKWISE ORDER, AS THEY APPEAR WHEN FACING THE ACTIVE-SIDE OF THE SURFACE, AND DERIVED FROM A RIGHT-HANDED COORDINATE SYSTEM.

Figure 32. Group E Sample Problems Program Results  
(continued)



#### SAMPLE PROBLEM GROUP F

The capability of computing factors to surfaces which are occluded by intervening surfaces is demonstrated as shown in Figure 33. The data sheets are presented in Figure 34 and the results in Figure 35.

##### Problem 1F

The factor from IPLA10 to IPLA9 is desired with surface IPLA11 intervening. The surface SCOPLA, representing the boundary points of IPLA9 including connections, and the boundary points of IPLA11 including connections is entered in data. Because the silhouette is complex, the surface SCOPLA must be reentered as SCOPLA to enable the silhouette generator to operate in the complex mode. The factor to SCOPLA from IPLA10 is requested as Run #1. Then, the factor from IPLA10 to IPLA11 is requested as Run #2. The factor from IPLA10 to IPLA9 is merely the difference between the two,

$$f = 0.26787 - 0.20146$$

$$f = 0.06641$$

##### Problem 2F

This problem also illustrates the capability of determining factors to occluded surfaces, but data is entered and handled in a different manner. The factor from IPLA10 to 6PIPE2 is desired, taking into account the flux interceded by SPIPE1.

The coordinates defining 6PIPE2 are internally generated. SPIPE1 is entered manually, and the two surfaces are combined for complex processing as 820FEN.

Notice that SPIPE1 includes a line segment--a "bridge" line--connecting point 7 in SPIPE1 to 6PIPE2. If this line or any other suitably oriented line serving the purpose were not present, then the silhouette generator would not include 6PIPE2 in any of the silhouettes computed from points on mapping lines 6 and 7 on IPLA10. The line does not have to actually be in any surface--it need only appear to intersect both surfaces in the silhouette.

The form factor to 820FEN is 0.28139 (Run #3); to SPIPE1 alone is 0.21556 (Run #4); therefore, the form factor to 6PIPE2 is the difference or 0.06583.

##### Problem 3F

This problem illustrates improper use of the program, and in particular, the silhouette generator. The factor from IPLA12 to SCOPLA is requested as Run #5. Note that the data SCOPLA is in reality two surfaces. These surfaces when viewed from IPLA10 or IPLA12 present a complex silhouette, and therefore, must be processed in the complex mode. However, when a class 4, 5 or 6 surface is specified as Surface 2, the simple mode is always used. The

silhouette generator consequently saw only IPLA11 sometimes and only IPLA9 sometimes; this condition would not be relieved by use of a bridge line, because the total silhouette is complex, and must be processed as complex.

#### Problem 4F

When a class 8 surface is used as Surface 2, Surface 1 must be in the XY plane of the Surface 2 coordinate system, with its orientation vector pointing toward the +Z axis. The results of Run #6 show the diagnostic resulting from a request for the factor from IPLA12 to SCOPLA.

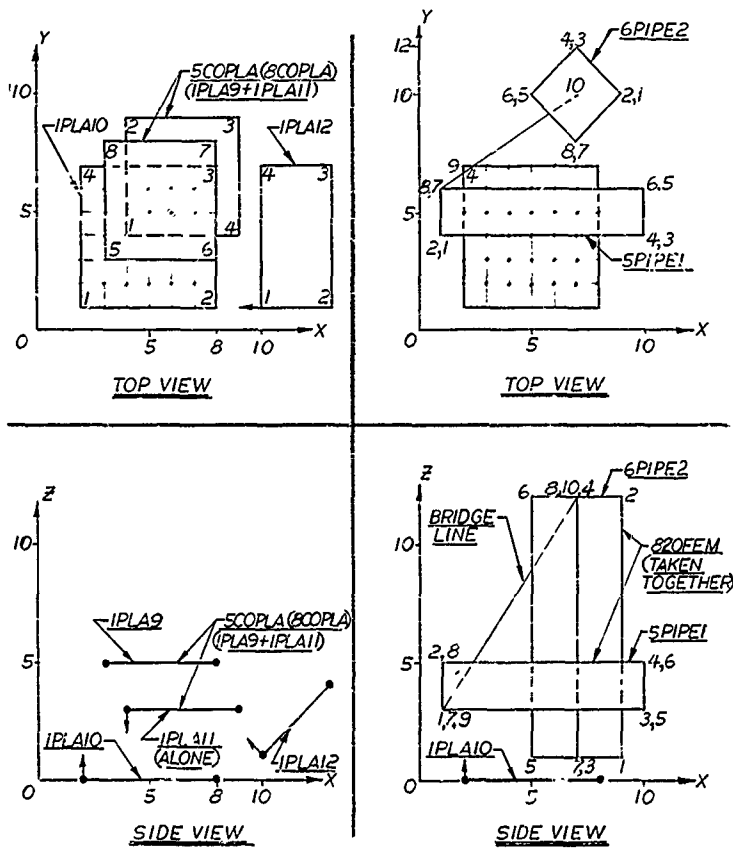


FIGURE 33. Group F Sample Problems Geometry

**FORTPAN FIXED 10 DIGIT DECIMAL DATA**

CODE NO. \_\_\_\_\_ PROGRAMMER \_\_\_\_\_ DATE \_\_\_\_\_ PAGE 27 of 36 JOB NO. 2029 30

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**FORTPAN FIXED 10 DIGIT DECIMAL DATA**

CODE NO. \_\_\_\_\_ PROGRAMMER \_\_\_\_\_ DATE \_\_\_\_\_ PAGE 28 of 36 JOB NO. 2029 30

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Figure 34. Group F Sample Problems Input Data Codo Sheets

FORTRAN FIXED 10 DIGIT DECIMAL DATA

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FORTRAN FIXED 10 DIGIT DECIMAL DATA

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Figure 34. Group F Sample Problems Input Data Code Sheets  
(continued)

**FORTRAN FIXED 10 DIGIT DECIMAL DATA**

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**FORTRAN FIXED 10 DIGIT DECIMAL DATA**

DECK NO.	PROGRAM NAME	DATE	PAGE 32 OF 36	JOB NO. 2252-36
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
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Figure 34. Group F Sample Problems Input Data Code Sheets  
(continued)

**FORTRAN: FIXED 10 DIGIT DECIMAL DATA**

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**FORTRAN: FIXED 10 DIGIT DECIMAL DATA**

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Figure 34. Group F Sample Problems Input Data Code Sheets  
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Figure 34. Group F Sample Problems Input Data Code Sheets  
(continued)



NAA SPACE AND INFORMATION SYSTEMS DIVISION  
NAA PROJECT RADIANT-INTERFERENCE CONFIGURATION FACTOR PROGRAM

C O N F A C I I

NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (F)-K.A.T.O.U.P.S., 11/1/63

I N P U T D A T A

\*\*\*\*\* DATA NAME= \*IPLA10 \* 6X6 PLATE IN XY PLANE

POINT	X	Y	Z	INTERVALLY GENERATED ORIENTATION VECTOR	Z
1	0.3000000E 01	0.1000000E 01	0.1000000E 01	0.1000000E 01	0.
2	0.2000000E 01	0.1000000E 01	0.1000000E 01	0.1000000E 01	0.
3	0.4000000E 01	0.7000000E 01	0.	0.2000000E 01	0.3000000E 01

\*\*\*\*\* DATA NAME= \*IPLA11 \* 5X5 SQUARE, Z=3, LOOKING AT IPLA10

POINT	X	Y	Z	INTERVALLY GENERATED ORIENTATION VECTOR	Z
1	0.4000000E 01	0.4000000E 01	0.2000000E 01	0.4000000E 01	0.
2	0.4000000E 01	0.4000000E 01	0.2000000E 01	0.4000000E 01	0.
3	0.2000000E 01	0.4000000E 01	0.3000000E 01	0.4000000E 01	0.3000000E 01

\*\*\*\*\* DATA NAME= \*SCOPLA \* IPLA11 COMBINED WITH IPLA0

POINT	X	Y	Z	INTERVALLY GENERATED ORIENTATION VECTOR	Z
1	0.4000000E 01	0.4000000E 01	0.3000000E 01	0.4000000E 01	0.3000000E 01
2	0.2000000E 01	0.4000000E 01	0.4000000E 01	0.4000000E 01	0.4000000E 01
3	0.2000000E 01	0.4000000E 01	0.4000000E 01	0.4000000E 01	0.4000000E 01
4	0.4000000E 01	0.4000000E 01	0.4000000E 01	0.4000000E 01	0.4000000E 01
5	0.4000000E 01	0.4000000E 01	0.3000000E 01	0.4000000E 01	0.3000000E 01
6	0.4000000E 01	0.4000000E 01	0.3000000E 01	0.4000000E 01	0.3000000E 01

POINT	CONNECTING POINTS	POINT	CONNECTING POINTS	POINT	CONNECTING POINTS
1	2, 4, 6, 0	2	1, 3, 5, 0	3	1, 2, 4, 0
4	1, 3, 5, 0	5	2, 4, 6, 0	6	1, 2, 4, 0

\*\*\*\*\* DATA NAME= \*IPLA12 \*

Figure 35. Group F Sample Problems Program Results  
(18 pages)

# SHEARED RECTANGLE LOOKING AT SCOPLA

```

POINT X Y Z POINT X Y Z
1 0.9208931 01 0.1000000 01 0.1700075 01 0.1000000 01 0.1000000 01 0.1000000 01
2 0.1000000 02 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01
3 0.1300000 02 0.7500000 01 0.4000000 01 0.1000000 02 0.7000000 01 0.1000000 01

```

\*\*\*\*\* DATA NAME= \*SPEP1 \* HORIZONTAL PARALLELEPIPED WITH LINE P-100E TO SPIPEZ

```

POINT X Y Z POINT X Y Z
1 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01
2 0.1000000 02 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01
3 0.1000000 02 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01
4 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01
5 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01
6 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01
7 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01
8 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01
9 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01
10 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01 0.1000000 01

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```

POINT CONNECTING POINTS POINT CONNECTING POINTS POINT CONNECTING POINTS
1 3, 4, 7, -0 2 4, 5, 8, -0 3 4, 5, 8, -0
4 5, 8, -0 5 9, -0, -0, -0 6 9, -0, -0, -0
7 10, -0, -0, -0

```

\*\*\*\*\* DATA NAME= \*SPIPE2 \* VERTICAL PARALLELEPIPED

SURFACE SPECIFICATIONS=

10 OF X-SECTIONS = 2

NO OF X-SECTION BOUNDARY DIVISIONS = 4

LOCATION OF VERTICAL CENTERLINE, X= 0.7000000 01, Y= 0.1000000 02

X-SECTION #0. X-AXIS RADIUS Y-AXIS RADIUS ELEVATION ABOVE XY PLANE

0.2000000 01 0.2000000 01 0.1000000 01

0.1000000 01 0.2000000 01 0.1000000 02

Y= FOLLOWING INTERNALLY GENERATED SURFACE DATA RESULTED FROM THE ABOVE SPECIFICATIONS=

```

POINT X Y Z POINT X Y Z
1 0.9208931 01 0.1000000 02 0.1000000 01 0.1000000 02 0.1000000 02
2 0.1000000 01 0.1000000 02 0.1000000 01 0.1000000 02 0.1000000 02
3 0.1000000 01 0.1000000 02 0.1000000 01 0.1000000 02 0.1000000 02
4 0.1000000 01 0.1000000 02 0.1000000 01 0.1000000 02 0.1000000 02
5 0.1000000 01 0.1000000 02 0.1000000 01 0.1000000 02 0.1000000 02
6 0.1000000 01 0.1000000 02 0.1000000 01 0.1000000 02 0.1000000 02
7 0.1000000 01 0.1000000 02 0.1000000 01 0.1000000 02 0.1000000 02

```

Figure 35. Group F Sample Problems Program Results  
(continued)

```

POINT CONNECTING POINTS  POINT CONNECTING POINTS  POINT CONNECTING POINTS  POINT
1 3, 2, 1, 0 2 4, 0, 8, 1 3 1, 8, 5, 0 8
5 7, 6, 5, 0 6 8, 0, 6, 5 7 1, 8, 5, 0 8
CONNECTIONS POINTS
***** DATA NAME= *SCOPLA * TO RUN SCOPLA IN COMPLEX MODE IN SILFAC
MULTISURFACE DATA=
SCOPLA, * * * * *
***** DATA NAME= *SOFEM * SPIPEL COMBINED WITH SPIPE2
MULTISURFACE DATA=
SPIPEL, SPIPE2, * * * * *

```

Figure 35. Group F Sample Problems Program Results  
(continued)

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NAA CONFAC II REPORT SAMPLE PROFILES FROM FIG. (F)-X-A-10UPS,11/ /63

RUN NO. 3 DATA USED FOR THIS RUN- \*IPLAIO=IPLAII\*  
 \*  
 \*D 1\*  
 \* 1\*

TR- FORM FACTOR FROM SURFACE \*IPLAIC \* TO SURFACE \*IPLAII \* = 0.21136

THE EXCHANGE COEFFICIENT (FA) = 0.76688E 01 SQ UNITS

THE MAPPING AREA = 0.3600000E 02 SQ UNITS

THE AREA OF SURFACE \*IPLAIO \* = 0.3603000E 02 SQ UNITS.

THE AREA OF SURFACE \*IPLAII \* = 0.2500000E 02 SQ UNITS.

THE FOLLOWING ARE THE FINAL SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

\*\*\*\*\* DATA NAME= \*IPLAIO \*  
 POINT X Y Z  
 1 0.2000000E 01 0.1000000E 01 0.1000000E 01  
 2 0.8000000E 01 0.1000000E 01 0.  
 3 0.8000000E 01 0.7000000E 01 0.  
 POINT X Y Z  
 1 0.2000000E 01 0.1000000E 01 0.1000000E 01  
 2 0.8000000E 01 0.1000000E 01 0.  
 3 0.8000000E 01 0.7000000E 01 0.

\*\*\*\*\* DATA NAME= \*IPLAII \*  
 POINT X Y Z  
 1 0.2000000E 01 0.1000000E 01 0.1000000E 01  
 2 0.8000000E 01 0.1000000E 01 0.1000000E 01  
 3 0.8000000E 01 0.7000000E 01 0.1000000E 01  
 COORDINATES OF POINTS ON BOUNDARY OF SURF \*IPLAIO \* FOR EACH Y INTERVAL  
 X-LEFT X-RIGHT X-LEFT X-RIGHT  
 1 0.2000000E 01 0.8000000E 01 0.1000000E 01 0.2000000E 01  
 2 0.2000000E 01 0.8000000E 01 0.1000000E 01 0.2000000E 01  
 3 0.2000000E 01 0.8000000E 01 0.1000000E 01 0.2000000E 01

Figure 35. Group F Sample Problems Program Results  
 (continued)

[illegible]



[illegible]

Figure 35. Group F Sample Problems Program Results  
(continued)

```

5 7 1 3 5 10 12 11 13 15 20 9 1 15 16 22 9 1
6 1 1 3 5 10 20 7 21 14 17 11 13 15 16 22 9 1
6 3 1 3 5 10 20 7 21 14 17 11 13 15 16 22 9 1
6 4 1 3 5 10 20 7 21 14 17 11 13 15 16 22 9 1
6 6 1 3 5 10 20 7 21 14 17 11 13 15 16 22 9 1
6 7 1 3 5 10 20 7 21 14 17 11 13 15 16 22 9 1
7 2 1 3 5 10 20 18 17 11 13 21 14 16 22 43 8 7 1
7 3 1 3 5 6 8 7 19 18 17 11 13 15 16 20 9 1
7 4 1 3 5 6 8 7 19 18 17 11 13 15 16 20 9 1
7 6 1 3 5 6 8 7 19 18 17 11 13 15 16 20 9 1
7 7 1 3 5 6 8 7 19 18 17 11 13 15 16 20 9 1

```

```

TOTAL TIME IN SILFAL = 15.570 SECONDS.
THE FORM FACTOR FROM SURFACE *IPLAIG * TO SURFACE *020FEW * = C.282/50
THE EXCHANGE COEFFICIENT (EFA3) = 0.10171E 02 50 UNITS
THE MAPPING AREA = C.9400002L 02 50 UNITS
THE AREA OF SURFACE *IPLAID * = C.3600000E 02 50 UNITS.

```

THE FOLLOWING ARE THE IFINAL SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION-

```

***** DATA NAME= *IPLAID *
POINT X Y Z POINT X Y Z
1 0.200000E 01 0.100000E 01 0.100000E 01-- (INTERMEDIATE ORIENTATION VECTOR)
2 0.200000E 01 0.100000E 01 0.100000E 01
3 0.200000E 01 0.100000E 01 0.100000E 01
COORDINATES OF POINTS ON BOUNDARY OF SURF *IPLAID * F3P EACH Y INTERVAL
X-LEFT X-RIGHT Y X-LEFT X-RIGHT Y
2.200000E 01 0.800000E 01 0.100000E 01 0.200000E 01 0.200000E 01

```

Figure 35. Group F Sample Problems Program Results  
(continued)

0.200000E 01 0.800000E 01 0.300000E 01 0.800000E 01 0.800000E 01  
 0.200000E 01 0.800000E 01 0.300000E 01 0.800000E 01 0.800000E 01  
 0.200000E 01 0.800000E 01 0.300000E 01 0.800000E 01 0.800000E 01

NO. OF HORIZONTAL INCREMENTS= 6 NO. OF VERTICAL INCREMENTS= 6

THE FOLLOWING ARE PLANE POINT CONFIGURATION FACTORS COMPUTED FOR THIS RUN  
 LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

C.114500E-00	0.132940E-00	0.185780E-00	0.152594E-00	0.153566E-00	0.188571E-00
C.117206E-00	0.175869E-00	0.193505E-00	0.202820E-00	0.264506E-00	0.198287E-00
C.189841E-00	0.227935E-00	0.280959E-00	0.231754E-00	0.204209E-00	0.257809E-00
C.190098E-00	0.267809E-00	0.295793E-00	0.311554E-00	0.317054E-00	0.311072E-00
C.268113E-00	0.536139E-00	0.587205E-00	0.380329E-00	0.394524E-00	0.594036E-00
C.282804E-00	0.318606E-00	0.389265E-00	0.365615E-00	0.380977E-00	0.378775E-00
C.368885E-00	0.301833E-00	0.350173E-00	0.584522E-00	0.340277E-00	0.386827E-00
C.353877E-00					
C.280051E-00					
C.362801E-00					

Figure 35. Group F Sample Problems Program Results  
 (continued)



```

5 7 1 3 7 1 1
6 2 1 3 3 0 8 7 1
0 7 1 3 3 0 8 7 1
0 7 1 3 3 0 8 7 1
0 6 1 3 3 0 8 7 1
7 1 1 3 3 0 8 7 1
7 2 1 3 3 0 8 7 1
7 3 1 3 3 0 8 7 1
7 4 1 3 3 0 8 7 1
7 5 1 3 3 0 8 7 1
7 6 1 3 3 0 8 7 1
7 7 1 3 3 0 8 7 1

```

TOTAL TIME IN SILENCE = 1.464 SECONDS.

THE FORM FACTOR FROM SURFACE \*IPLAID \* TO SURFACE \*SPIPEL \* = 0.42472

L/N EXCHANGE COEFFICIENT (FA) = 0.77299E 01 SC UNITS

THE MAPPING AREA = 0.3650000E 02 SQ UNITS

THE AREA OF SURFACE \*IPLAID \* = 0.3650000E 02 SQ UNITS.

THE FOLLOWING ARE THE (FINAL) SURFACE COORDINATES USED FOR THE FACTOR COMPUTATION

```

***** DATA NAME= *IPLAID *
POINT X Y Z POINT X Y Z
1 0.20000E 01 0.10000E 01 0.10000E 01 --- (INTERNALLY GENERATED ORIENTATION VECTORS)
2 0.20000E 01 0.10000E 01 0.10000E 01
3 0.2000000E 01 0.2000000E 01 0.
***** DATA NAME= *SPIPEL *

```

Figure 35. Group F Sample Problems Program Results  
(continued)

POINT	X	Y	POINT	X	Y	Z
1	0.100000E 01	0.400000E 01	1	0.100000E 01	0.400000E 01	0.500000E 01
2	0.200000E 01	0.300000E 01	2	0.200000E 01	0.300000E 01	0.400000E 01
3	0.100000E 01	0.200000E 01	3	0.100000E 01	0.200000E 01	0.300000E 01
4	0.200000E 01	0.100000E 01	4	0.200000E 01	0.100000E 01	0.200000E 01
5	0.100000E 01	0.100000E 01	5	0.100000E 01	0.100000E 01	0.100000E 01
6	0.200000E 01	0.200000E 01	6	0.200000E 01	0.200000E 01	0.200000E 01
7	0.300000E 01	0.300000E 01	7	0.300000E 01	0.300000E 01	0.300000E 01
8	0.400000E 01	0.400000E 01	8	0.400000E 01	0.400000E 01	0.400000E 01
9	0.500000E 01	0.500000E 01	9	0.500000E 01	0.500000E 01	0.500000E 01
10	0.600000E 01	0.600000E 01	10	0.600000E 01	0.600000E 01	0.600000E 01

# COORDINATES OF JOINTS ON BOUNDARY OF SURF

X=LEFT	X=RIGHT	Y
--------	---------	---

[illegible]

NO. OF HORIZONTAL INCREMENTS = 6 NO. OF VERTICAL INCREMENTS = 6

THE FOLLOWING ARE PLANE POINT CONFIGURATION FACTORS COMPUTED FOR THIS RUN  
LOWEST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

THE FOLLOWING ARE THE  
FIRST GRID LINE FIRST, FROM X-LEFT TO X-RIGHT.

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NAA CONVAC II REPORT SAMPLE PROBLEMS FROM FIG. 43-A...TODS.11/1/63

RUN NO. 5 DATA USED FOR THIS RUN= \*PLA12+SCOLA\*  
+0 1+ 1+

SURFACE 2 SILHOUETTE COMPUTED FROM MAPPING POINT SHOW

MAPPING	5	0	7	0	5
LINE	5	0	7	0	5
PT	5	0	7	0	5
1	5	0	7	0	5
2	5	0	7	0	5
3	5	0	7	0	5
4	5	0	7	0	5
5	5	0	7	0	5
6	5	0	7	0	5
7	5	0	7	0	5
8	5	0	7	0	5
9	5	0	7	0	5
10	5	0	7	0	5
11	5	0	7	0	5
12	5	0	7	0	5
13	5	0	7	0	5
14	5	0	7	0	5
15	5	0	7	0	5
16	5	0	7	0	5
17	5	0	7	0	5
18	5	0	7	0	5
19	5	0	7	0	5
20	5	0	7	0	5
21	5	0	7	0	5
22	5	0	7	0	5
23	5	0	7	0	5
24	5	0	7	0	5
25	5	0	7	0	5
26	5	0	7	0	5
27	5	0	7	0	5
28	5	0	7	0	5
29	5	0	7	0	5
30	5	0	7	0	5
31	5	0	7	0	5
32	5	0	7	0	5
33	5	0	7	0	5
34	5	0	7	0	5
35	5	0	7	0	5
36	5	0	7	0	5
37	5	0	7	0	5
38	5	0	7	0	5
39	5	0	7	0	5
40	5	0	7	0	5
41	5	0	7	0	5
42	5	0	7	0	5
43	5	0	7	0	5
44	5	0	7	0	5
45	5	0	7	0	5
46	5	0	7	0	5
47	5	0	7	0	5
48	5	0	7	0	5
49	5	0	7	0	5
50	5	0	7	0	5
51	5	0	7	0	5
52	5	0	7	0	5
53	5	0	7	0	5
54	5	0	7	0	5
55	5	0	7	0	5
56	5	0	7	0	5
57	5	0	7	0	5
58	5	0	7	0	5
59	5	0	7	0	5
60	5	0	7	0	5
61	5	0	7	0	5
62	5	0	7	0	5
63	5	0	7	0	5
64	5	0	7	0	5
65	5	0	7	0	5
66	5	0	7	0	5
67	5	0	7	0	5
68	5	0	7	0	5
69	5	0	7	0	5
70	5	0	7	0	5
71	5	0	7	0	5
72	5	0	7	0	5
73	5	0	7	0	5
74	5	0	7	0	5
75	5	0	7	0	5
76	5	0	7	0	5
77	5	0	7	0	5
78	5	0	7	0	5
79	5	0	7	0	5
80	5	0	7	0	5
81	5	0	7	0	5
82	5	0	7	0	5
83	5	0	7	0	5
84	5	0	7	0	5
85	5	0	7	0	5
86	5	0	7	0	5
87	5	0	7	0	5
88	5	0	7	0	5
89	5	0	7	0	5
90	5	0	7	0	5
91	5	0	7	0	5
92	5	0	7	0	5
93	5	0	7	0	5
94	5	0	7	0	5
95	5	0	7	0	5
96	5	0	7	0	5
97	5	0	7	0	5
98	5	0	7	0	5
99	5	0	7	0	5
100	5	0	7	0	5

Figure 35. Group F Sample Problems Program Results  
(continued)

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NAA CONFAC II REPORT SAMPLE PROBLEMS FROM FIG. (F)-K.A.TOU'S 11/1/68

PUN NO. 6 DATA USED FOR THIS RUN- \*IPLA12\*SCPLA\*  
 \*  
 \*D 1\*  
 \* 1\*

SURFACE 1 MUST BE IN THE XY PLANE OF ITS CS WHEN SURFACE 2 IS CLASS B-THIS PUN ABORTED.

Figure 35. Group F Sample Problems Program Results  
 (continued)

## APPENDIX B

### PROGRAM DECK SETUP, LISTINGS, AND MAPS

The program deck arrangement shown in Figure 36 contains a main program and six subprograms which are listed in this appendix. A listing of the main program, 7J360, is shown in Figure 37 followed by a map of the core storage locations in Figure 38.

The first subprogram in the deck setup is subroutine UNIVFC which is shown in Figure 39 and the map of core storage in Figure 40. The transformation subroutine, TAPRI, is presented in Figure 41 and the map of core storage in Figure 42. The listing and map of subroutine DOICU is presented in Figures 43 and 44. The listing and map of subroutine MAP, is presented in Figure 45 and 46. The listing of the subroutine FACTOR is presented in Figure 47 and the map of core storage in Figure 48. Subroutine SILFAC listing and core storage is presented in Figure 49. Figure 51 shows the variable formats used by this program.

This IBM FORTRAN II program uses two input-output statements which must be modified for computing systems other than the NAA Monitor, FIB III, system. These are

```
READ N, List
```

```
PRINT N, List
```

A convenient FAP assembled program is included which will convert the READ-PRINT statement to,

```
READ INPUT TAPE 5, N, List
```

```
WRITE OUTPUT TAPE 6, N, List
```

This assembly is listed in Figure 52. The convert to any other computing system using peripheral equipment and not using the same tape designations, the last three EOU cards are simply changed to read

```
MIN EOU A (Input statement tape number)
```

```
MAX EOU B (Output statement tape number)
```

```
MPUNCH EOU C (Punch statement tape number)
```

For computing centers using attached printing equipment, the FAP assembly can be removed and the program will execute in that system.

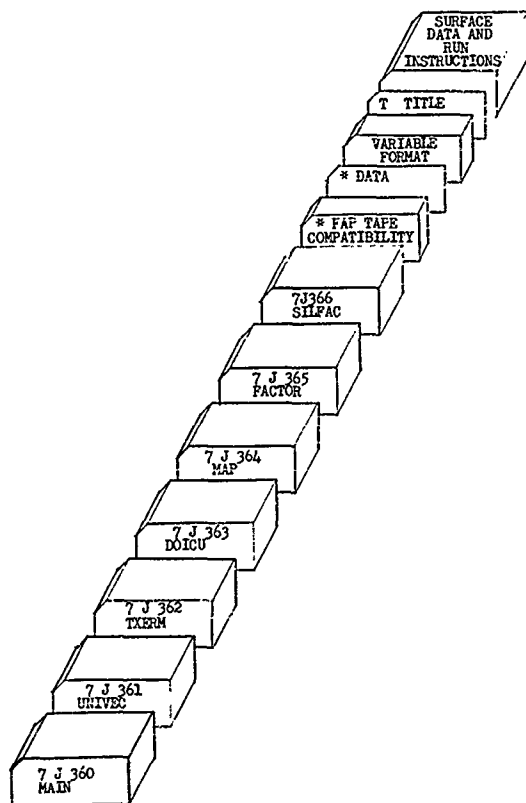


FIGURE 36. PROGRAM DECK SETUP

73360 CONFAC II-MAIN PROG-ANALYSIS AND PROG BY K.A.TOUPE,NIA SID. 11/1/63 02/06/64 PAGE 1

C CONFAC II-MAIN PROG-ANALYSIS AND PROG BY K.A.TOUPE,NIA SID. 11/1/63 36000100  
 C FACTORS BETWEEN SURFACES. THE COMPUTATION OF CONFIGURATION AND TORQ 36000200  
 C FORTRAN SUBROUTINES USED ARE UNIVG,FAIRNO,DISCUM,FACTOR, AND SILFAC 36000300  
 C ALL READ FUNCTIONS USED ARE SINCOS AND SORT 36000400  
 C ARE CONVERTED TO TAPE READ AND WRITE BY A.F.P. COMPUTING PATENTERS 36000500  
 C C TITING FAP SUBROUTINES COUNIV AND TITVARE USED IN SILFAC. 36000600  
 C OF PARACAM STRUCTURE AND USE OF SYSTEMS REPORT S.V. 63-1387 FOR DETAILS 36000700  
 C DIMENSION F1(12),F1(30),F2(12),F2(12),F3(12),F4(12),F5(12),F6(12) 36000800  
 C F1(12),F2(12),F3(12),F4(12),F5(12),F6(12),F7(12),F8(12),F9(12),F10(12) 36000900  
 C F11(12),F12(12),F13(12),F14(12),F15(12),F16(12),F17(12),F18(12),F19(12),F20(12) 36001000  
 C F21(12),F22(12),F23(12),F24(12),F25(12),F26(12),F27(12),F28(12),F29(12),F30(12) 36001100  
 C F31(12),F32(12),F33(12),F34(12),F35(12),F36(12),F37(12),F38(12),F39(12),F40(12) 36001200  
 C F41(12),F42(12),F43(12),F44(12),F45(12),F46(12),F47(12),F48(12),F49(12),F50(12) 36001300  
 C F51(12),F52(12),F53(12),F54(12),F55(12),F56(12),F57(12),F58(12),F59(12),F60(12) 36001400  
 C F61(12),F62(12),F63(12),F64(12),F65(12),F66(12),F67(12),F68(12),F69(12),F70(12) 36001500  
 C F71(12),F72(12),F73(12),F74(12),F75(12),F76(12),F77(12),F78(12),F79(12),F80(12) 36001600  
 C F81(12),F82(12),F83(12),F84(12),F85(12),F86(12),F87(12),F88(12),F89(12),F90(12) 36001700  
 C F91(12),F92(12),F93(12),F94(12),F95(12),F96(12),F97(12),F98(12),F99(12),F100(12) 36001800  
 C F101(12),F102(12),F103(12),F104(12),F105(12),F106(12),F107(12),F108(12),F109(12),F110(12) 36001900  
 C F111(12),F112(12),F113(12),F114(12),F115(12),F116(12),F117(12),F118(12),F119(12),F120(12) 36002000  
 C F121(12),F122(12),F123(12),F124(12),F125(12),F126(12),F127(12),F128(12),F129(12),F130(12) 36002100  
 C F131(12),F132(12),F133(12),F134(12),F135(12),F136(12),F137(12),F138(12),F139(12),F140(12) 36002200  
 C F141(12),F142(12),F143(12),F144(12),F145(12),F146(12),F147(12),F148(12),F149(12),F150(12) 36002300  
 C F151(12),F152(12),F153(12),F154(12),F155(12),F156(12),F157(12),F158(12),F159(12),F160(12) 36002400  
 C F161(12),F162(12),F163(12),F164(12),F165(12),F166(12),F167(12),F168(12),F169(12),F170(12) 36002500  
 C F171(12),F172(12),F173(12),F174(12),F175(12),F176(12),F177(12),F178(12),F179(12),F180(12) 36002600  
 C F181(12),F182(12),F183(12),F184(12),F185(12),F186(12),F187(12),F188(12),F189(12),F190(12) 36002700  
 C F191(12),F192(12),F193(12),F194(12),F195(12),F196(12),F197(12),F198(12),F199(12),F200(12) 36002800  
 C F201(12),F202(12),F203(12),F204(12),F205(12),F206(12),F207(12),F208(12),F209(12),F210(12) 36002900  
 C F211(12),F212(12),F213(12),F214(12),F215(12),F216(12),F217(12),F218(12),F219(12),F220(12) 36003000  
 C F221(12),F222(12),F223(12),F224(12),F225(12),F226(12),F227(12),F228(12),F229(12),F230(12) 36003100  
 C F231(12),F232(12),F233(12),F234(12),F235(12),F236(12),F237(12),F238(12),F239(12),F240(12) 36003200  
 C F241(12),F242(12),F243(12),F244(12),F245(12),F246(12),F247(12),F248(12),F249(12),F250(12) 36003300  
 C F251(12),F252(12),F253(12),F254(12),F255(12),F256(12),F257(12),F258(12),F259(12),F260(12) 36003400  
 C F261(12),F262(12),F263(12),F264(12),F265(12),F266(12),F267(12),F268(12),F269(12),F270(12) 36003500  
 C F271(12),F272(12),F273(12),F274(12),F275(12),F276(12),F277(12),F278(12),F279(12),F280(12) 36003600  
 C F281(12),F282(12),F283(12),F284(12),F285(12),F286(12),F287(12),F288(12),F289(12),F290(12) 36003700  
 C F291(12),F292(12),F293(12),F294(12),F295(12),F296(12),F297(12),F298(12),F299(12),F300(12) 36003800  
 C F301(12),F302(12),F303(12),F304(12),F305(12),F306(12),F307(12),F308(12),F309(12),F310(12) 36003900  
 C F311(12),F312(12),F313(12),F314(12),F315(12),F316(12),F317(12),F318(12),F319(12),F320(12) 36004000  
 C F321(12),F322(12),F323(12),F324(12),F325(12),F326(12),F327(12),F328(12),F329(12),F330(12) 36004100  
 C F331(12),F332(12),F333(12),F334(12),F335(12),F336(12),F337(12),F338(12),F339(12),F340(12) 36004200  
 C F341(12),F342(12),F343(12),F344(12),F345(12),F346(12),F347(12),F348(12),F349(12),F350(12) 36004300  
 C F351(12),F352(12),F353(12),F354(12),F355(12),F356(12),F357(12),F358(12),F359(12),F360(12) 36004400  
 C F361(12),F362(12),F363(12),F364(12),F365(12),F366(12),F367(12),F368(12),F369(12),F370(12) 36004500  
 C F371(12),F372(12),F373(12),F374(12),F375(12),F376(12),F377(12),F378(12),F379(12),F380(12) 36004600  
 C F381(12),F382(12),F383(12),F384(12),F385(12),F386(12),F387(12),F388(12),F389(12),F390(12) 36004700  
 C F391(12),F392(12),F393(12),F394(12),F395(12),F396(12),F397(12),F398(12),F399(12),F400(12) 36004800  
 C F401(12),F402(12),F403(12),F404(12),F405(12),F406(12),F407(12),F408(12),F409(12),F410(12) 36004900  
 C F411(12),F412(12),F413(12),F414(12),F415(12),F416(12),F417(12),F418(12),F419(12),F420(12) 36005000  
 C F421(12),F422(12),F423(12),F424(12),F425(12),F426(12),F427(12),F428(12),F429(12),F430(12) 36005100  
 C F431(12),F432(12),F433(12),F434(12),F435(12),F436(12),F437(12),F438(12),F439(12),F440(12) 36005200  
 C F441(12),F442(12),F443(12),F444(12),F445(12),F446(12),F447(12),F448(12),F449(12),F450(12) 36005300  
 C F451(12),F452(12),F453(12),F454(12),F455(12),F456(12),F457(12),F458(12),F459(12),F460(12) 36005400  
 C F461(12),F462(12),F463(12),F464(12),F465(12),F466(12),F467(12),F468(12),F469(12),F470(12) 36005500  
 C F471(12),F472(12),F473(12),F474(12),F475(12),F476(12),F477(12),F478(12),F479(12),F480(12) 36005600  
 C F481(12),F482(12),F483(12),F484(12),F485(12),F486(12),F487(12),F488(12),F489(12),F490(12) 36005700  
 C F491(12),F492(12),F493(12),F494(12),F495(12),F496(12),F497(12),F498(12),F499(12),F500(12) 36005800  
 C F501(12),F502(12),F503(12),F504(12),F505(12),F506(12),F507(12),F508(12),F509(12),F510(12) 36005900  
 C F511(12),F512(12),F513(12),F514(12),F515(12),F516(12),F517(12),F518(12),F519(12),F520(12) 36006000  
 C F521(12),F522(12),F523(12),F524(12),F525(12),F526(12),F527(12),F528(12),F529(12),F530(12) 36006100  
 C F531(12),F532(12),F533(12),F534(12),F535(12),F536(12),F537(12),F538(12),F539(12),F540(12) 36006200  
 C F541(12),F542(12),F543(12),F544(12),F545(12),F546(12),F547(12),F548(12),F549(12),F550(12) 36006300  
 C F551(12),F552(12),F553(12),F554(12),F555(12),F556(12),F557(12),F558(12),F559(12),F560(12) 36006400  
 C F561(12),F562(12),F563(12),F564(12),F565(12),F566(12),F567(12),F568(12),F569(12),F570(12) 36006500  
 C F571(12),F572(12),F573(12),F574(12),F575(12),F576(12),F577(12),F578(12),F579(12),F580(12) 36006600  
 C F581(12),F582(12),F583(12),F584(12),F585(12),F586(12),F587(12),F588(12),F589(12),F590(12) 36006700  
 C F591(12),F592(12),F593(12),F594(12),F595(12),F596(12),F597(12),F598(12),F599(12),F600(12) 36006800  
 C F601(12),F602(12),F603(12),F604(12),F605(12),F606(12),F607(12),F608(12),F609(12),F610(12) 36006900  
 C F611(12),F612(12),F613(12),F614(12),F615(12),F616(12),F617(12),F618(12),F619(12),F620(12) 36007000  
 C F621(12),F622(12),F623(12),F624(12),F625(12),F626(12),F627(12),F628(12),F629(12),F630(12) 36007100  
 C F631(12),F632(12),F633(12),F634(12),F635(12),F636(12),F637(12),F638(12),F639(12),F640(12) 36007200  
 C F641(12),F642(12),F643(12),F644(12),F645(12),F646(12),F647(12),F648(12),F649(12),F650(12) 36007300  
 C F651(12),F652(12),F653(12),F654(12),F655(12),F656(12),F657(12),F658(12),F659(12),F660(12) 36007400  
 C F661(12),F662(12),F663(12),F664(12),F665(12),F666(12),F667(12),F668(12),F669(12),F670(12) 36007500  
 C F671(12),F672(12),F673(12),F674(12),F675(12),F676(12),F677(12),F678(12),F679(12),F680(12) 36007600  
 C F681(12),F682(12),F683(12),F684(12),F685(12),F686(12),F687(12),F688(12),F689(12),F690(12) 36007700  
 C F691(12),F692(12),F693(12),F694(12),F695(12),F696(12),F697(12),F698(12),F699(12),F700(12) 36007800  
 C F701(12),F702(12),F703(12),F704(12),F705(12),F706(12),F707(12),F708(12),F709(12),F710(12) 36007900  
 C F711(12),F712(12),F713(12),F714(12),F715(12),F716(12),F717(12),F718(12),F719(12),F720(12) 36008000  
 C F721(12),F722(12),F723(12),F724(12),F725(12),F726(12),F727(12),F728(12),F729(12),F730(12) 36008100  
 C F731(12),F732(12),F733(12),F734(12),F735(12),F736(12),F737(12),F738(12),F739(12),F740(12) 36008200  
 C F741(12),F742(12),F743(12),F744(12),F745(12),F746(12),F747(12),F748(12),F749(12),F750(12) 36008300  
 C F751(12),F752(12),F753(12),F754(12),F755(12),F756(12),F757(12),F758(12),F759(12),F760(12) 36008400  
 C F761(12),F762(12),F763(12),F764(12),F765(12),F766(12),F767(12),F768(12),F769(12),F770(12) 36008500  
 C F771(12),F772(12),F773(12),F774(12),F775(12),F776(12),F777(12),F778(12),F779(12),F780(12) 36008600  
 C F781(12),F782(12),F783(12),F784(12),F785(12),F786(12),F787(12),F788(12),F789(12),F790(12) 36008700  
 C F791(12),F792(12),F793(12),F794(12),F795(12),F796(12),F797(12),F798(12),F799(12),F800(12) 36008800  
 C F801(12),F802(12),F803(12),F804(12),F805(12),F806(12),F807(12),F808(12),F809(12),F810(12) 36008900  
 C F811(12),F812(12),F813(12),F814(12),F815(12),F816(12),F817(12),F818(12),F819(12),F820(12) 36009000  
 C F821(12),F822(12),F823(12),F824(12),F825(12),F826(12),F827(12),F828(12),F829(12),F830(12) 36009100  
 C F831(12),F832(12),F833(12),F834(12),F835(12),F836(12),F837(12),F838(12),F839(12),F840(12) 36009200  
 C F841(12),F842(12),F843(12),F844(12),F845(12),F846(12),F847(12),F848(12),F849(12),F850(12) 36009300  
 C F851(12),F852(12),F853(12),F854(12),F855(12),F856(12),F857(12),F858(12),F859(12),F860(12) 36009400  
 C F861(12),F862(12),F863(12),F864(12),F865(12),F866(12),F867(12),F868(12),F869(12),F870(12) 36009500  
 C F871(12),F872(12),F873(12),F874(12),F875(12),F876(12),F877(12),F878(12),F879(12),F880(12) 36009600  
 C F881(12),F882(12),F883(12),F884(12),F885(12),F886(12),F887(12),F888(12),F889(12),F890(12) 36009700  
 C F891(12),F892(12),F893(12),F894(12),F895(12),F896(12),F897(12),F898(12),F899(12),F900(12) 36009800  
 C F901(12),F902(12),F903(12),F904(12),F905(12),F906(12),F907(12),F908(12),F909(12),F910(12) 36009900  
 C F911(12),F912(12),F913(12),F914(12),F915(12),F916(12),F917(12),F918(12),F919(12),F920(12) 36010000  
 C F921(12),F922(12),F923(12),F924(12),F925(12),F926(12),F927(12),F928(12),F929(12),F930(12) 36010100  
 C F931(12),F932(12),F933(12),F934(12),F935(12),F936(12),F937(12),F938(12),F939(12),F940(12) 36010200  
 C F941(12),F942(12),F943(12),F944(12),F945(12),F946(12),F947(12),F948(12),F949(12),F950(12) 36010300  
 C F951(12),F952(12),F953(12),F954(12),F955(12),F956(12),F957(12),F958(12),F959(12),F960(12) 36010400  
 C F961(12),F962(12),F963(12),F964(12),F965(12),F966(12),F967(12),F968(12),F969(12),F970(12) 36010500  
 C F971(12),F972(12),F973(12),F974(12),F975(12),F976(12),F977(12),F978(12),F979(12),F980(12) 36010600  
 C F981(12),F982(12),F983(12),F984(12),F985(12),F986(12),F987(12),F988(12),F989(12),F990(12) 36010700  
 C F991(12),F992(12),F993(12),F994(12),F995(12),F996(12),F997(12),F998(12),F999(12),F1000(12) 36010800  
 C F1001(12),F1002(12),F1003(12),F1004(12),F1005(12),F1006(12),F1007(12),F1008(12),F1009(12),F1010(12) 36010900  
 C F1011(12),F1012(12),F1013(12),F1014(12),F1015(12),F1016(12),F1017(12),F1018(12),F1019(12),F1020(12) 36011000  
 C F1021(12),F1022(12),F1023(12),F1024(12),F1025(12),F1026(12),F1027(12),F1028(12),F1029(12),F1030(12) 36011100  
 C F1031(12),F1032(12),F1033(12),F1034(12),F1035(12),F1036(12),F1037(12),F1038(12),F1039(12),F1040(12) 36011200  
 C F1041(12),F1042(12),F1043(12),F1044(12),F1045(12),F1046(12),F1047(12),F1048(12),F1049(12),F1050(12) 36011300  
 C F1051(12),F1052(12),F1053(12),F1054(12),F1055(12),F1056(12),F1057(12),F1058(12),F1059(12),F1060(12) 36011400  
 C F1061(12),F1062(12),F1063(12),F1064(12),F1065(12),F1066(12),F1067(12),F1068(12),F1069(12),F1070(12) 36011500  
 C F1071(12),F1072(12),F1073(12),F1074(12),F1075(12),F1076(12),F1077(12),F1078(12),F1079(12),F1080(12) 36011600  
 C F1081(12),F1082(12),F1083(12),F1084(12),F1085(12),F1086(12),F1087(12),F1088(12),F1089(12),F1090(12) 36011700  
 C F1091(12),F1092(12),F1093(12),F1094(12),F1095(12),F1096(12),F1097(12),F1098(12),F1099(12),F1100(12) 36011800  
 C F1101(12),F1102(12),F1103(12),F1104(12),F1105(12),F1106(12),F1107(12),F1108(12),F1109(12),F1110(12) 36011900  
 C F1111(12),F1112(12),F1113(12),F1114(12),F1115(12),F1116(12),F1117(12),F1118(12),F1119(12),F1120(12) 36012000  
 C F1121(12),F1122(12),F1123(12),F1124(12),F1125(12),F1126(12),F1127(12),F1128(12),F1129(12),F1130(12) 36012100  
 C F1131(12),F1132(12),F1133(12),F1134(12),F1135(12),F1136(12),F1137(12),F1138(12),F1139(12),F1140(12) 36012200  
 C F1141(12),F1142(12),F1143(12),F1144(12),F1145(12),F1146(12),F1147(12),F1148(12),F1149(12),F1150(12) 36012300  
 C F1151(12),F1152(12),F1153(12),F1154(12),F1155(12),F1156(12),F1157(12),F1158(12),F1159(12),F1160(12) 36012400  
 C F1161(12),F1162(12),F1163(12),F1164(12),F1165(12),F1166(12),F1167(12),F1168(12),F1169(12),F1170(12) 36012500  
 C F1171(12),F1172(12),F1173(12),F1174(12),F1175(12),F1176(12),F1177(12),F1178(12),F1179(12),F1180(12) 36012600  
 C F1181(12),F1182(12),F1183(12),F1184(12),F1185(12),F1186(12),F1187(12),F1188(12),F1189(12),F1190(12) 36012700  
 C F1191(12),F1192(12),F1193(12),F1194(12),F1195(12),F1196(12),F1197(12),F1198(12),F1199(12),F1200(12) 36012800  
 C F1201(12),F1202(12),F1203(12),F1204(12),F1205(12),F1206(12),F1207(12),F1208(12),F1209(12),F1210(12) 36012900  
 C F1211(12),F1212(12),F1213(12),F1214(12),F1215(12),F1216(12),F1217(12),F1218(12),F1219(12),F1220(12) 36013000  
 C F1221(12),F1222(12),F1223(12),F1224(12),F1225(12),F1226(12),F1227(12),F1228(12),F1229(12),F1230(12) 36013100  
 C F1231(12),F1232(12),F1233(12),F1234(12),F1235(12),F1236(12),F1237(12),F1238(12),F1239(12),F1240(12) 36013200  
 C F1241(12),F1242(12),F1243(12),F1244(12),F1245(12),F1246(12),F1247(12),F1248(12),F1249(12),F1250(12) 36013300  
 C F1251(12),F1252(12),F1253(12),F1254(12),F1255(12),F1256(12),F1257(12),F1258(12),F1259(12),F1260(12) 3601340

36004030



[illegible]



73300 COMPAC II-MAIN PROG-ANALYSIS AND PROG BY K.A.TOURP, NAA SIO, 11/1/63 11/08/63 PAGE 5

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12200 F1(101-FILLID)
C SELECT REMAINDER FOR ERROR PRINTOUT AND TERMINATE JOB
C READ REMAINDER OF THIS SURFACE DATA
12400 W/CONNECTION DATA
      F5,P1(3),2(1),((P(K,M),1,3,M-3,NP)
      GO TO 22200
C READ CLASS 5 DATA-INTERNAL PLANE POLYGON-CONSTANT SILUET BOUNDARY PTS.
13000 W/CONNECTION DATA
      F5, SILUET,10(1,1),10(1,1),10(1,1)
C PRINT SPECIFICATIONS
      H5ID=SID
      GO TO 10500
C READ DATA FOR A PLANE SURFACE W/CONNECTION DATA-CLASS 4
14000 W/CONNECTION DATA
C READ DATA FOR A NO-PLANAR SURFACE W/CONNECTION DATA-CLASS 5
C ADVANCE COUNTER LOCATING CONNECTIONS DATA
15000 IF(41C-1)13114500,14600,14500
      14500 PRINT
      14600 W/CONNECTION DATA
      GO TO 13400
C READ SURFACE DATA LOCATION TO CONNECTIONS
C READ SENSE LIGHT 1
14600 AC1(1)-1C
C READ SENSE LIGHT 2
14600 AC2(1)-1C
C BOUNDARY LINE Q
      READ
      F0,P0,((P(1,1),M+1,3),((P(M,1),1C),M+1,4),P1)
      131411)
C TEST AGAINST MAX ALLOWABLE
C READ F5(50P11-100)115200,15200,112200
C READ REMAINDER OF DATA IF MAX NO. OF POINTS IS NOT EXCEEDED
15200 W/CONNECTION DATA
      READ
      F7,P1(2,2),1(1),P1(3,2),1(1),((P(M,1),2,1C),M+1,4),
      GO TO 142000
C READ CLASS 6 DATA TO GENERATE A PLANE POLYGON OR MULTIFACETED SURFACE
W/CONNECTION DATA
16000 SENSE LIGHT 1

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Figure 37. Main Program Listing  
(continued)





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73300  COMPAC II-MAIN PROG-ANALYSIS AND PROG BY K.A-TOUPS,MAA SID, 11/71/63
41800  P11:1:1=P11:1:1
P12:1:1=P12:1:1
P13:1:1=P13:1:1
C TRAN:2:2 TO GENERATE CONNECTIONS DATA
C CLAS:3:3 TO SURFACE TO FACILITATE AREA AND FACTOR COMPUTATION--CLASS 1:2
22000  K=1
P11:1:1=P11:1:1
P12:1:1=P12:1:1
P13:1:1=P13:1:1
P14:1:1=P14:1:1
P15:1:1=P15:1:1
P16:1:1=P16:1:1
P17:1:1=P17:1:1
P18:1:1=P18:1:1
P19:1:1=P19:1:1
P20:1:1=P20:1:1
P21:1:1=P21:1:1
P22:1:1=P22:1:1
P23:1:1=P23:1:1
P24:1:1=P24:1:1
P25:1:1=P25:1:1
P26:1:1=P26:1:1
P27:1:1=P27:1:1
P28:1:1=P28:1:1
P29:1:1=P29:1:1
P30:1:1=P30:1:1
P31:1:1=P31:1:1
P32:1:1=P32:1:1
P33:1:1=P33:1:1
P34:1:1=P34:1:1
P35:1:1=P35:1:1
P36:1:1=P36:1:1
P37:1:1=P37:1:1
P38:1:1=P38:1:1
P39:1:1=P39:1:1
P40:1:1=P40:1:1
P41:1:1=P41:1:1
P42:1:1=P42:1:1
P43:1:1=P43:1:1
P44:1:1=P44:1:1
P45:1:1=P45:1:1
P46:1:1=P46:1:1
P47:1:1=P47:1:1
P48:1:1=P48:1:1
P49:1:1=P49:1:1
P50:1:1=P50:1:1
P51:1:1=P51:1:1
P52:1:1=P52:1:1
P53:1:1=P53:1:1
P54:1:1=P54:1:1
P55:1:1=P55:1:1
P56:1:1=P56:1:1
P57:1:1=P57:1:1
P58:1:1=P58:1:1
P59:1:1=P59:1:1
P60:1:1=P60:1:1
P61:1:1=P61:1:1
P62:1:1=P62:1:1
P63:1:1=P63:1:1
P64:1:1=P64:1:1
P65:1:1=P65:1:1
P66:1:1=P66:1:1
P67:1:1=P67:1:1
P68:1:1=P68:1:1
P69:1:1=P69:1:1
P70:1:1=P70:1:1
P71:1:1=P71:1:1
P72:1:1=P72:1:1
P73:1:1=P73:1:1
P74:1:1=P74:1:1
P75:1:1=P75:1:1
P76:1:1=P76:1:1
P77:1:1=P77:1:1
P78:1:1=P78:1:1
P79:1:1=P79:1:1
P80:1:1=P80:1:1
P81:1:1=P81:1:1
P82:1:1=P82:1:1
P83:1:1=P83:1:1
P84:1:1=P84:1:1
P85:1:1=P85:1:1
P86:1:1=P86:1:1
P87:1:1=P87:1:1
P88:1:1=P88:1:1
P89:1:1=P89:1:1
P90:1:1=P90:1:1
P91:1:1=P91:1:1
P92:1:1=P92:1:1
P93:1:1=P93:1:1
P94:1:1=P94:1:1
P95:1:1=P95:1:1
P96:1:1=P96:1:1
P97:1:1=P97:1:1
P98:1:1=P98:1:1
P99:1:1=P99:1:1
P100:1:1=P100:1:1

```

Figure 37. Main Program Listing  
(continued)

```

DO 26500 M=1,N
26500 AREA11=AREA11-OPFIN2,M,1,1-OPFIN1,M,1,1)
36031300
36031400
36031500
36031600
36031700
36031800
36031900
36032000
36032100
36032200
36032300
36032400
36032500
36032600
36032700
36032800
36032900
36033000
36033100
36033200
36033300
36033400
36033500
36033600
36033700
36033800
36033900
36034000
36034100
36034200
36034300
36034400
36034500
36034600
36034700
36034800
36034900
36035000
36035100

```

CONFAC 11, MAIN PROG-ANALYSIS AND PHOD BY K.A.T.O.U.P.S.+N.A. SIO, 11/1/63

DO 26500 M=1,N  
26500 AREA11=AREA11-OPFIN2,M,1,1-OPFIN1,M,1,1)  
36031300  
36031400  
36031500  
36031600  
36031700  
36031800  
36031900  
36032000  
36032100  
36032200  
36032300  
36032400  
36032500  
36032600  
36032700  
36032800  
36032900  
36033000  
36033100  
36033200  
36033300  
36033400  
36033500  
36033600  
36033700  
36033800  
36033900  
36034000  
36034100  
36034200  
36034300  
36034400  
36034500  
36034600  
36034700  
36034800  
36034900  
36035000  
36035100

CONFAC 11, MAIN PROG-ANALYSIS AND PHOD BY K.A.T.O.U.P.S.+N.A. SIO, 11/1/63

DO 26500 M=1,N  
26500 AREA11=AREA11-OPFIN2,M,1,1-OPFIN1,M,1,1)  
36031300  
36031400  
36031500  
36031600  
36031700  
36031800  
36031900  
36032000  
36032100  
36032200  
36032300  
36032400  
36032500  
36032600  
36032700  
36032800  
36032900  
36033000  
36033100  
36033200  
36033300  
36033400  
36033500  
36033600  
36033700  
36033800  
36033900  
36034000  
36034100  
36034200  
36034300  
36034400  
36034500  
36034600  
36034700  
36034800  
36034900  
36035000  
36035100

Figure 37. Main Program Listing (continued)

[illegible]

[illegible]









00895091

Figure 37. Main Program Listing  
(continued)





STORAGE NOT USED BY PROGRAM

DEC	DEC	DEC	DEC
4006 07646	14613 34425		

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

DEC	DEC	DEC	DEC	DEC	DEC
AMAP 13169 35501	AREA 21067 31113	AREAX 21011 31023	CL 22094 31116		
C2 21945 32671	C3 21795 32443	CL 16140 37414	OK 22154 32112		
FO 15746 35216	FO 15746 35216	OP 15179 35317	PL 15077 14995		
F 15160 35514	FV 14950 35146	INC 14449 14471	RC 20976 07650		
AD 22154 33212	KP 15492 36204	KX 15492 36205	LD 16125 32401		
MSV65 15023 35257	CL 15152 35116	NOA 22100 33124	MOD 22112 53140		
NOL 21157 31245	NON 22114 53142	ND3 15168 35503	ND 23493 18206		
NOM 21002 32176	NYP 21014 31750	NB 15493 35203	NIC 31111 50191		
MS10 22101 51125	MSL 23217 61201	ASN 21269 14455	NITLE 21293 51455		
NV 15182 35516	NVL 15191 35215	PAF 16151 37427	PP 32761 27461		
AV 20968 51006	SL 21693 52275	SP 16445 40075	TDA 22100 53124		
TON 22114 53142	TNSD 22101 53125	VA 22094 53116	Y 16154 37432		
TS 20987 50273	Y 14889 50051	Y1 15368 36010			

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC	DEC	DEC	DEC	DEC	DEC
F0 3993 07631	F10 3777 07701	F11 3753 07251	F12 3741 07235		
F17 3659 07125	F18 3657 07111	F19 3633 07081	F6 3681 07615		
F20 3621 07045	F21 3597 07015	F22 3565 07001	F23 3573 08765		
F24 3547 06931	F25 3409 06641	F26 3474 06561	F27 3455 06551		
F30 3345 06421	F31 3321 06371	F32 3285 06325	F33 3271 06311		
F34 3249 06261	F35 3237 06245	F36 3214 06210	F37 3202 06202		
F42 4006 07845	F43 3185 06181	F5 3685 07455	F6 1873 07441		

Figure 58. Main Program Core Storage Map



C11GH	3085 06015	C11G1	3086 06016	C1201	3097 06017	C1209	3088 06020
C120P	3089 06021	C126G	3090 06022	C1201	3091 06023	C120J	3092 06024
C1112	3111 06077	C1118	3095 01123	C1118	3095 01123	C1118	3095 01123
C1112F	357 01675	C112U	1183 02237	C1131	1201 02363	C113V	1515 01753
C1115G	2009 03213	C114U	1095 02602	C114U	1095 02602	C114U	1095 02602
C1213F	1472 02700	C123U	1478 02706	C124F	1724 03274	C1251	1974 03666
C123M	1988 03704	C1264	2112 04100	C1269	2135 04127	C126A	2150 04162
C1265	2293 04365	C1270	2560 05000	C1278	2588 05034	C1282	2638 05116
C1281	2821 05405	C1312	510 00776	C1318	594 01132	C1320	745 01681
C1313	2008 05730	C136F	2216 04250	C138C	2320 05406	C1407	705 00312
C1404	221 00335	C142L	1077 02065	C143F	1376 02549	C1440	1539 03003
C1422	1867 05113	C1453	2012 03250	C1454	245 01670	C1470	2311 04412
C1473	2491 04673	C1479	2563 05003	C147R	2586 05032	C1503	201 00311
C1512	508 00774	C152F	1956 01674	C1540	1538 03002	C1547	1577 03051
C152L	1976 01670	C1555	2030 03767	C1603	198 00306	C1604	220 00334
C162L	1076 02064	C164F	1723 03273	C1659	2013 03735	C1665	2292 04364
C170F	1732 03273	C170U	1400 03445	C1750	2007 03727	C1767	2215 02747
E10	576 00602	E134	1277 02375	E135	1281 02401	E137	1298 02422
E136	1313 02441	E13F	1409 02601	E13M	1418 02612	E150	1537 03001
E13E	1927 03697	E161	2246 04306	E177	2412 04554	E17M	2222 04732
E170	2562 05012	E17P	2567 05007	E17Q	2513 05015	E17R	2590 05036

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	061	DEC	062	DEC	063	DEC	064
COS	14 00012	ORICU	15 00017	EXIT	7 00007	FACT04	14 00070
HAP	14 00016	SILFAC	15 00017	SIN	9 00011	SORT	11 00013
PERM	12 00014	UNIVEC	8 00010	ICSWH	1 00001	151CT	5 00005
LS-PM	4 00004	IRMI	3 00003	3L11	2 00002	1310;	6 00006

Figure 36. Main Program Core Storage Map  
(continued)



COS FORM (SPH)	DSICH UNITEC	ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY				SRT (SLP)
		EXIT (CMP)	FACTOR (FEL)	MAP (MPT)	SELEC (SEK)	
EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND ACTUAL LOCATIONS						
EFN	IFN	LDC	IFN	LDC	IFN	LDC
100	9	00340	2500	19	00342	1000
200	18	00340	2500	19	00342	1000
300	34	00456	4000	36	00463	4100
400	34	00456	4000	36	00463	4100
500	34	00456	4000	36	00463	4100
600	34	00456	4000	36	00463	4100
700	79	00731	11000	80	00732	12000
800	67	01003	13000	68	01004	14000
900	106	01174	17000	107	01175	18000
1000	176	01510	19000	177	01511	20000
1100	185	01510	19000	186	01511	20000
1200	176	01510	19000	177	01511	20000
1300	185	01510	19000	186	01511	20000
1400	193	01676	19800	193	01677	20500
1500	246	02240	22400	246	02241	23000
1600	246	02240	22400	246	02241	23000
1700	246	02240	22400	246	02241	23000
1800	258	02373	23800	259	02377	24500
1900	258	02373	23800	259	02377	24500
2000	274	02530	27000	274	02531	27500
2100	274	02530	27000	274	02531	27500
2200	274	02530	27000	274	02531	27500
2300	305	02644	31000	307	02646	31500
2400	502	02616	1732	506	02633	1832
2500	502	02616	1732	506	02633	1832
2600	502	02616	1732	506	02633	1832
2700	502	02616	1732	506	02633	1832
2800	502	02616	1732	506	02633	1832
2900	502	02616	1732	506	02633	1832
3000	502	02616	1732	506	02633	1832
3100	502	02616	1732	506	02633	1832
3200	502	02616	1732	506	02633	1832
3300	502	02616	1732	506	02633	1832
3400	502	02616	1732	506	02633	1832
3500	502	02616	1732	506	02633	1832
3600	502	02616	1732	506	02633	1832
3700	502	02616	1732	506	02633	1832
3800	502	02616	1732	506	02633	1832
3900	502	02616	1732	506	02633	1832
4000	502	02616	1732	506	02633	1832
4100	502	02616	1732	506	02633	1832
4200	502	02616	1732	506	02633	1832
4300	502	02616	1732	506	02633	1832
4400	502	02616	1732	506	02633	1832
4500	502	02616	1732	506	02633	1832
4600	502	02616	1732	506	02633	1832
4700	502	02616	1732	506	02633	1832
4800	502	02616	1732	506	02633	1832
4900	502	02616	1732	506	02633	1832
5000	502	02616	1732	506	02633	1832
5100	502	02616	1732	506	02633	1832
5200	502	02616	1732	506	02633	1832
5300	502	02616	1732	506	02633	1832
5400	502	02616	1732	506	02633	1832
5500	502	02616	1732	506	02633	1832
5600	502	02616	1732	506	02633	1832
5700	502	02616	1732	506	02633	1832
5800	502	02616	1732	506	02633	1832
5900	502	02616	1732	506	02633	1832
6000	502	02616	1732	506	02633	1832
6100	502	02616	1732	506	02633	1832
6200	502	02616	1732	506	02633	1832
6300	502	02616	1732	506	02633	1832
6400	502	02616	1732	506	02633	1832
6500	502	02616	1732	506	02633	1832
6600	502	02616	1732	506	02633	1832
6700	502	02616	1732	506	02633	1832
6800	502	02616	1732	506	02633	1832
6900	502	02616	1732	506	02633	1832
7000	502	02616	1732	506	02633	1832
7100	502	02616	1732	506	02633	1832
7200	502	02616	1732	506	02633	1832
7300	502	02616	1732	506	02633	1832
7400	502	02616	1732	506	02633	1832
7500	502	02616	1732	506	02633	1832
7600	502	02616	1732	506	02633	1832
7700	502	02616	1732	506	02633	1832
7800	502	02616	1732	506	02633	1832
7900	502	02616	1732	506	02633	1832
8000	502	02616	1732	506	02633	1832
8100	502	02616	1732	506	02633	1832
8200	502	02616	1732	506	02633	1832
8300	502	02616	1732	506	02633	1832
8400	502	02616	1732	506	02633	1832
8500	502	02616	1732	506	02633	1832
8600	502	02616	1732	506	02633	1832
8700	502	02616	1732	506	02633	1832
8800	502	02616	1732	506	02633	1832
8900	502	02616	1732	506	02633	1832
9000	502	02616	1732	506	02633	1832
9100	502	02616	1732	506	02633	1832
9200	502	02616	1732	506	02633	1832
9300	502	02616	1732	506	02633	1832
9400	502	02616	1732	506	02633	1832
9500	502	02616	1732	506	02633	1832
9600	502	02616	1732	506	02633	1832
9700	502	02616	1732	506	02633	1832
9800	502	02616	1732	506	02633	1832
9900	502	02616	1732	506	02633	1832
10000	502	02616	1732	506	02633	1832

Figure 38. Main Program Core Storage Map  
(continued)

JF360	CONVEX II MAIN PROG-ANALYSIS AND PROG BY K.A.TOUPS-NAA STD. 11/1/63										02/06/64		PAGE 22	
	266232	420 04101	264932	421 04107	265332	423 04115	267232	426 04124	267232	426 04124	267232	426 04124		
	267232	431 04130	267432	439 04145	267432	440 04145	267432	440 04145	267432	440 04145	267432	440 04145		
	267432	441 04145	267432	441 04145	267432	441 04145	267432	441 04145	267432	441 04145	267432	441 04145		
	267732	442 04145	267732	449 04150	267732	450 04150	268032	451 04153	268032	451 04153	268032	451 04153		
	268032	443 04150	268232	449 04150	268232	450 04150	268232	451 04153	268232	451 04153	268232	451 04153		
	268232	444 04153	268232	450 04153	268232	450 04153	268232	451 04153	268232	451 04153	268232	451 04153		
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	268232	447 04153	268232	450 04153	268232	450 04153	268232	451 04153	268232	451 04153	268232	451 04153		
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	268232	463 04153	268232	450 04153	268232	450 04153	268232	451 04153	268232	451 04153	268232	451 04153		
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	268232	466 04153	268232	450 04153	268232	450 04153	268232	451 04153	268232	451 04153	268232	451 04153		
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	268232	480 04153	268232	450 04153	268232	450 04153	268232	451 04153	268232	451 04153	268232	451 04153		
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	268232	512 04153	268232	450 04153	268232	450 04153	268232	451 04153	268232	451 04153	268232	451 04153		
	268232													

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UNITECUNFAC EIGENANALYSIS AND PROGRAMMING BY K.A.TOUPEY,MINASIO,21/1/69
SUBROUTINE UNITECUNFAC (N,NP,NM,NM2,NM3,NM4,NM5,NM6,NM7,NM8,NM9,NM10,NM11,NM12,NM13,NM14,NM15,NM16,NM17,NM18,NM19,NM20,NM21,NM22,NM23,NM24,NM25,NM26,NM27,NM28,NM29,NM30,NM31,NM32,NM33,NM34,NM35,NM36,NM37,NM38,NM39,NM40,NM41,NM42,NM43,NM44,NM45,NM46,NM47,NM48,NM49,NM50,NM51,NM52,NM53,NM54,NM55,NM56,NM57,NM58,NM59,NM60,NM61,NM62,NM63,NM64,NM65,NM66,NM67,NM68,NM69,NM70,NM71,NM72,NM73,NM74,NM75,NM76,NM77,NM78,NM79,NM80,NM81,NM82,NM83,NM84,NM85,NM86,NM87,NM88,NM89,NM90,NM91,NM92,NM93,NM94,NM95,NM96,NM97,NM98,NM99,NM100,NM101,NM102,NM103,NM104,NM105,NM106,NM107,NM108,NM109,NM110,NM111,NM112,NM113,NM114,NM115,NM116,NM117,NM118,NM119,NM120,NM121,NM122,NM123,NM124,NM125,NM126,NM127,NM128,NM129,NM130,NM131,NM132,NM133,NM134,NM135,NM136,NM137,NM138,NM139,NM140,NM141,NM142,NM143,NM144,NM145,NM146,NM147,NM148,NM149,NM150,NM151,NM152,NM153,NM154,NM155,NM156,NM157,NM158,NM159,NM160,NM161,NM162,NM163,NM164,NM165,NM166,NM167,NM168,NM169,NM170,NM171,NM172,NM173,NM174,NM175,NM176,NM177,NM178,NM179,NM180,NM181,NM182,NM183,NM184,NM185,NM186,NM187,NM188,NM189,NM190,NM191,NM192,NM193,NM194,NM195,NM196,NM197,NM198,NM199,NM200,NM201,NM202,NM203,NM204,NM205,NM206,NM207,NM208,NM209,NM210,NM211,NM212,NM213,NM214,NM215,NM216,NM217,NM218,NM219,NM220,NM221,NM222,NM223,NM224,NM225,NM226,NM227,NM228,NM229,NM230,NM231,NM232,NM233,NM234,NM235,NM236,NM237,NM238,NM239,NM240,NM241,NM242,NM243,NM244,NM245,NM246,NM247,NM248,NM249,NM250,NM251,NM252,NM253,NM254,NM255,NM256,NM257,NM258,NM259,NM260,NM261,NM262,NM263,NM264,NM265,NM266,NM267,NM268,NM269,NM270,NM271,NM272,NM273,NM274,NM275,NM276,NM277,NM278,NM279,NM280,NM281,NM282,NM283,NM284,NM285,NM286,NM287,NM288,NM289,NM290,NM291,NM292,NM293,NM294,NM295,NM296,NM297,NM298,NM299,NM300,NM301,NM302,NM303,NM304,NM305,NM306,NM307,NM308,NM309,NM310,NM311,NM312,NM313,NM314,NM315,NM316,NM317,NM318,NM319,NM320,NM321,NM322,NM323,NM324,NM325,NM326,NM327,NM328,NM329,NM330,NM331,NM332,NM333,NM334,NM335,NM336,NM337,NM338,NM339,NM340,NM341,NM342,NM343,NM344,NM345,NM346,NM347,NM348,NM349,NM350,NM351,NM352,NM353,NM354,NM355,NM356,NM357,NM358,NM359,NM360,NM361,NM362,NM363,NM364,NM365,NM366,NM367,NM368,NM369,NM370,NM371,NM372,NM373,NM374,NM375,NM376,NM377,NM378,NM379,NM380,NM381,NM382,NM383,NM384,NM385,NM386,NM387,NM388,NM389,NM390,NM391,NM392,NM393,NM394,NM395,NM396,NM397,NM398,NM399,NM400,NM401,NM402,NM403,NM404,NM405,NM406,NM407,NM408,NM409,NM410,NM411,NM412,NM413,NM414,NM415,NM416,NM417,NM418,NM419,NM420,NM421,NM422,NM423,NM424,NM425,NM426,NM427,NM428,NM429,NM430,NM431,NM432,NM433,NM434,NM435,NM436,NM437,NM438,NM439,NM440,NM441,NM442,NM443,NM444,NM445,NM446,NM447,NM448,NM449,NM450,NM451,NM452,NM453,NM454,NM455,NM456,NM457,NM458,NM459,NM460,NM461,NM462,NM463,NM464,NM465,NM466,NM467,NM468,NM469,NM470,NM471,NM472,NM473,NM474,NM475,NM476,NM477,NM478,NM479,NM480,NM481,NM482,NM483,NM484,NM485,NM486,NM487,NM488,NM489,NM490,NM491,NM492,NM493,NM494,NM495,NM496,NM497,NM498,NM499,NM500,NM501,NM502,NM503,NM504,NM505,NM506,NM507,NM508,NM509,NM510,NM511,NM512,NM513,NM514,NM515,NM516,NM517,NM518,NM519,NM520,NM521,NM522,NM523,NM524,NM525,NM526,NM527,NM528,NM529,NM530,NM531,NM532,NM533,NM534,NM535,NM536,NM537,NM538,NM539,NM540,NM541,NM542,NM543,NM544,NM545,NM546,NM547,NM548,NM549,NM550,NM551,NM552,NM553,NM554,NM555,NM556,NM557,NM558,NM559,NM560,NM561,NM562,NM563,NM564,NM565,NM566,NM567,NM568,NM569,NM570,NM571,NM572,NM573,NM574,NM575,NM576,NM577,NM578,NM579,NM580,NM581,NM582,NM583,NM584,NM585,NM586,NM587,NM588,NM589,NM590,NM591,NM592,NM593,NM594,NM595,NM596,NM597,NM598,NM599,NM600,NM601,NM602,NM603,NM604,NM605,NM606,NM607,NM608,NM609,NM610,NM611,NM612,NM613,NM614,NM615,NM616,NM617,NM618,NM619,NM620,NM621,NM622,NM623,NM624,NM625,NM626,NM627,NM628,NM629,NM630,NM631,NM632,NM633,NM634,NM635,NM636,NM637,NM638,NM639,NM640,NM641,NM642,NM643,NM644,NM645,NM646,NM647,NM648,NM649,NM650,NM651,NM652,NM653,NM654,NM655,NM656,NM657,NM658,NM659,NM660,NM661,NM662,NM663,NM664,NM665,NM666,NM667,NM668,NM669,NM670,NM671,NM672,NM673,NM674,NM675,NM676,NM677,NM678,NM679,NM680,NM681,NM682,NM683,NM684,NM685,NM686,NM687,NM688,NM689,NM690,NM691,NM692,NM693,NM694,NM695,NM696,NM697,NM698,NM699,NM700,NM701,NM702,NM703,NM704,NM705,NM706,NM707,NM708,NM709,NM710,NM711,NM712,NM713,NM714,NM715,NM716,NM717,NM718,NM719,NM720,NM721,NM722,NM723,NM724,NM725,NM726,NM727,NM728,NM729,NM730,NM731,NM732,NM733,NM734,NM735,NM736,NM737,NM738,NM739,NM740,NM741,NM742,NM743,NM744,NM745,NM746,NM747,NM748,NM749,NM750,NM751,NM752,NM753,NM754,NM755,NM756,NM757,NM758,NM759,NM760,NM761,NM762,NM763,NM764,NM765,NM766,NM767,NM768,NM769,NM770,NM771,NM772,NM773,NM774,NM775,NM776,NM777,NM778,NM779,NM780,NM781,NM782,NM783,NM784,NM785,NM786,NM787,NM788,NM789,NM790,NM791,NM792,NM793,NM794,NM795,NM796,NM797,NM798,NM799,NM800,NM801,NM802,NM803,NM804,NM805,NM806,NM807,NM808,NM809,NM810,NM811,NM812,NM813,NM814,NM815,NM816,NM817,NM818,NM819,NM820,NM821,NM822,NM823,NM824,NM825,NM826,NM827,NM828,NM829,NM830,NM83
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### Figure 39. Subroutine UNIVTEC Listing

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73361 UNIVETCSNFC ISANALYSIS AND PROGRAMMING BY K.A.TROUPS,MAISTO,11/1/63 11/07/73 PAGE 3

DEC	QCT	DEC	QCT	DEC	QCT	DEC	QCT
13	189 00275	21	178 00262	61	183 00257	C11C0	193 00301
C11C0	193 00301	C11C0	193 00301	C11C0	193 00301	C11C0	193 00301
D1103	193 00301	D1103	193 00301	D1103	193 00301	D1103	193 00301
C1703	193 00301	E11	30 00036	E12	17 00045	D11C0	193 00301

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	QCT	DEC	QCT	DEC	QCT
3007	0 00000				

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

SGRT

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LCC	EFN	IFN	LCC	EFN	IFN	LCC
10	8 00032	20	10 00046	25	11 00111	30	13 00123	
35	14 00102	40	15 00174					

Figure 40. Subroutine UNIVET Core Storage Map  
(continued)

[illegible]

Figure 41. Subroutine TXFRM Listing

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C AND P ARE STAGGERED 1 POINT 3 COORDINATES THROUGH EQUIVALENCE.
C THIS POINT IS THE NEW ORIGIN.
C COMPUTE DIRECTION COSINES OF NEW Y-AXIS RELATIVE TO OLD X-Y-Z
C USE VECTOR CROSS OF OTHER COMPONENTS.
COS(A12,1)=COS(A13,2)*COS(A11,3)-COS(A11,2)*COS(A13,3)
COS(A12,2)=COS(A13,1)*COS(A11,3)+COS(A11,2)*COS(A13,3)
COS(A12,3)=COS(A13,1)*COS(A11,2)-COS(A11,3)*COS(A13,2)
C COMPUTE TRANSLATION COMPONENTS H*XL MOVING OLD ORIGIN TO NEW ORIGIN
C AT P05 K*1.
15 T(A1)=P11,2,1,NO)+COS(A1K,1)*P12,1,1,NO)+COS(A1K,2)*P13,1,1,NO)+COS(A1K,3)
GO TO 310
C START OF PRIMARY TRANSFORMATION SECTION
C SELECT TRANSFORMATION DATA NAME
C NAME=CONV
C PICKUP TFRM DATA FROM NOL
C NAME=NOL
C SELECT TRANSFORMATION DATA FOR MULTIPLE USE LATER.
C NAME=NOL
C COMPUTE A FOURTH POINT FROM THE THREE COORDINATES IN SURFACE DATA.
C NECESSARILY NOT IN THE PLANE OF THE OTHER THREE. THIS POINT CORRESPONDS TO THE POINT GIVEN IN THE SURFACE DATA. USING THE
C THREE POINTS GIVEN IN TRANSFORMATION DATA(SEE MAIN PROGRAM)
CALL UNIVECTOR(NOL,KO12,NC1,NP,NO(4),NC1)
R11=NP(1),NP,NO(4),NC1
R12=NP(2),NP,NO(4),NC1
R13=NP(3),NP,NO(4),NC1
C THE FOLLOWING FUNDAMENTAL EQUATION IS SOLVED FOR THE NEW CS AXES
C DIRECTION COSINES RELATIVE TO OLD, ALONG WITH THE TRANSLATION COMP
C X,Y,Z=PP+COS(A1,81,1)*PP+COS(A2,82,2)*PP+COS(A3,83,3)*PP+K*1
C THIS EQUATION IS WRITTEN FOUR TIMES, FORMING A 4X4 DETERMINANT, AND
C SOLVED FOR COS(A2,82,1,2) AND COS(A3,83,3) BY CRAMER'S RULE. COS(A1,81,3)
C IS THEN DERIVED BY THE X-PRODUCT OF THE Y-Z UNIT VECTORS COS(SINES)
C COS(A1,81,3)=COS(A2,82,1,2)*COS(A3,83,3)
C COMPUTE DIRECTION COSINES OF NEW AXES BY MEANS OF A 4X4 DETERMINANT
C WITH 4TH COLUMN 1'S(COEFFICIENT OF TRANSLATION COMPONENT).
36204000
36204100
36204200
36204300
36204400
36204500
36204600
36204700
36204800
36204900
36205000
36205100
36205200
36205300
36205400
36205500
36205600
36205700
36205800
36205900
36206000
36206100
36206200
36206300
36206400
36206500
36206600
36206700
36206800
36206900
36207000
36207100
36207200
36207300
36207400
36207500
36207600
36207700
36207800
36207900

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Figure 41. Subroutine TFRM Listing (continued)





2099-000





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C DTICUICNFAC III ANALYSIS AND PROGRAMMING BY K.A.TOUPS,HAASID,11/1/63 36300100
C THIS SUBROUTINE DETERMINES WHETHER THE SURFACES SEE EACH OTHER IN 36300200
C WHOLE OR IN PART, AND IF A PART, COMPUTES THE COORDINATE AND AREA OF 36300300
C THE PART OF SURFACE WHICH IS IN THE OTHER'S FOV. 36300400
C DIMENSION NITE,SURFAC,NITEIN,NITEOUT,NITEIN2,NITEOUT2,NITEIN3,NITEOUT3, 36300500
1AREAL569,NOL569,NOLP34,NP3,LOS,21,25,11,11,RY(11),AC(34),NISC(569), 36300600
2P4,102,11,MA(9),543,91,NM511,21,10K(10),OIN(10),OIP(13),LOI,36300700
34REXAL7,NINC(11),FAP(25),25,11,61,21,V(10),21,02(10),M5CL(12,12), 36300800
34S5N51121,FH(10),1,FV(10),N5CL(12,25),21,1201,V(120),M5CL(10), 36300900
520UTVALERGE IP,P4(11),MO(10),1,100,NOM1,101,NOM2,17M5ID,M5ID0,10M5 36301000
1,0,0,1,N5CL,3,P4(12),5,1,100,NOM3,NOMC(11),1,VA(11),C(11),1,23,36301100
100,NITEIN,NITEOUT,NITEIN2,NITEOUT2,NITEIN3,NITEOUT3,NITEIN4,NITEOUT4, 36301200
COPON,NITEIN,NITEOUT,NITEIN2,NITEOUT2,NITEIN3,NITEOUT3,NITEIN4,NITEOUT4, 36301300
164,3P,NM5,MOP,P4,V,P4F,CL,NOM2,POT,LO,LP,LI,FHP,NOM,KK,AP,NP,AL,YL, 36301400
30R,FAP,WH,NINC,NITEIN,NITEOUT,NITEIN2,NITEOUT2,NITEIN3,NITEOUT3,NITEIN4, 36301500
NITEOUT4,NITEIN5,NITEOUT5,NITEIN6,NITEOUT6,NITEIN7,NITEOUT7,NITEIN8, 36301600
IFSENSE LIGHT 41600,450 36301700
400 KL=30 34000 36301800
450 KL=2 36301900
C DB 10000 KP=1,2 36302000
C INITIALIZE SURFACES 36302100
C IF SURFACE KP IS NONPLANAR, DO NOT CHECK BISECTION OF SURFACE KL 36302200
C INITIALIZE SURFACES 36302300
C SELECT POSITION OF SURFACE KP IN ARRAY P 36302400
C DO J=1,NITEIN FOR SURFACE KL 36302500
J=LP,KL3 36302600
C VP= NO. OF POINTS DEFINING SURFACE JL 36302700
C COMPUTE COMPONENTS OF UNIT VECTOR IN SURFACE KP 36302800
OXP=PP(1,1-JP)-PP(1,2-JP) 36302900
OYP=PP(2,1-JP)-PP(2,2-JP) 36303000
OZP=PP(3,1-JP)-PP(3,2-JP) 36303100
36303200
36303300
36303400
36303500
36303600
36303700
36303800
36303900
36304000

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Figure 43. Subroutine DTICU Listing

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Figure 43. Subroutine DOICU Listing  
(continued)



72363 D01CUCONFAC I1) ANALYSIS AND PROGRAMMING BY K.A.TOUPS;NA:ID:1.1/163 11/09/75 PAGE 4

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C PROCEED TO RESPECT SURFACE KL IF REQUIRED
15700 IF(L1,M1)116000,7000,34000
C PICKUP SUBSCRIPTS OF SURFACES IN ARRAY P
16000 IS=1;M1=1;N=1;N1=1
C TEST Z-COORDINATES OF SURFACE KL. COMPUTE X,Y AT TRANSITION AND RETURN--36312200
C 8th POINTS ABOVE HORIZON.
SENSE LIGHT 0
DO 22000 N=1,NP
C IF 1ST POINT IS HORIZON, USE THE POINT. TURN ON SLL IF ZERO.
IF(L1,M1,J1)17000,18000,19000
C IF NEXT POINT IS - OR 0 CONTINUE. IF +, GO TO COMPUTE X,Y AT HORIZON.
IF(L1,M1,J1)20000,22000,23000
C ADVANCE TO THE NEXT SUBSCRIPT TO NEW POSITION IN KP OF ARRAY P.
19000 P1=M1;M1=PI1,M1,J1
PI1,M1=PI1,M1,J1
PI1,M1=PI1,M1,J1
C TEST IF NEXT POINT IS HORIZON. IF YES, GO TO PICKUP ON NEXT GO ROUND.
IF(L1,M1,J1)20000,22000,23000
C IF 1ST POINT IS HORIZON, THE VALUE OF X,Y AT THE HORIZON MUST
C BE COMPUTED.
20000 IF(SENSE LIGHT 1)22000,21000
C COMPUTE X,Y AT HORIZON(=0) FROM TRACE OF LINE SEGMENT M=M+1 ON XZ AND
C YZ PLANES.
ZG=PI1,M1,J1/PI1,M1,J1=PI1,M1,J1
21500 PI1,M1=PI1,M1,J1=-C*PI1,M1,J1=PI1,M1,J1
22000 PI1,M1=PI1,M1,J1=0.
C ADVANCE TO NEXT POINT.
22000 L1=M1;M1=PI1,M1,J1
N1=PI1,M1,J1
C COMPUTE X,Y AT HORIZON(=0) FROM ELU COORDINATES.
C USE THE HORIZON(=0) VECTORS IN ARRAY M AND P.
C ADVANCE TO NEXT POINT. IF NEXT POINT IS HORIZON, GO TO PICKUP ON NEXT GO ROUND.
C USE IF(SENSE LIGHT 1) EQUAL TO POINT 1 FOR USE LATER.
36311700
36311800
36311900
36312000
36312100
36312200
36312300
36312400
36312500
36312600
36312700
36312800
36312900
36313000
36313100
36313200
36313300
36313400
36313500
36313600
36313700
36313800
36313900
36314000
36314100
36314200
36314300
36314400
36314500
36314600
36314700
36314800
36314900
36315000
36315100
36315200
36315300
36315400
36315500

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Figure 4.3. Subroutine MOICU Listing  
(continued)

$\chi = \chi_0$ 

Figure 43. Subroutine DOICU Listing  
(continued)



## STORAGE NOT USED BY PROGRAM

DEC OCT  
831 01477 14237 34451

## STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

DEC OCT	DEC OCT	DEC OCT	DEC OCT	DEC OCT
ANAP 21045 32571	ARCA 21093 5443	AREX 21140 37413	CL 21154 33112	CT
C2 21045 32571	C3 21093 5443	CL 21140 37414	C4 21154 33112	
DT 22102 33126	DX 13446 35616	UY 13179 35513	FA 13185 35511	
EM 14449 34477	EM 14449 34477	NO 21154 33112	GA 13485 35511	
EX 12493 34205	LO 16129 37401	LI 18121 37371	KD 15492 36206	
MP 22042 32076	MOL 13172 35179	45LL 18121 37371	LP 16123 37373	
NO 15168 35500	ND 15494 34206	NUT 22102 33116	NLM 22116 33116	
NH 12183 35217	NMS 16418 40042	NO 21093 35215	NM 15184 35440	
NS 12183 35217	NT 16418 40042	NO 21093 35215	NM 15184 35440	
PAF 16151 37427	PP 22061 37461	NO 21093 35215	NM 15184 35440	
SP 14446 34477	RA 14446 34477	NO 21093 35215	NM 15184 35440	
VA 21094 33116	TDA 22000 33124	NO 21093 35215	NM 15184 35440	
YI 13368 36015	Y 14769 34661	NO 21093 35215	NM 15184 35440	

## STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENTS

DEC OCT	DEC OCT	L'C	DEC OCT
C5 830 01476	DC 829 01475	DXL 842 01474	DGP 827 01473
DYL 826 01472	DYP 825 01471	OZL 824 01470	DIP 823 01467
J 817 01466	K 816 01465	L 815 01464	JM 814 01463
JP 814 01456	N 813 01455	K 810 01460	M 815 01457
	N2 813 01455	P1 812 01454	ZC 811 01453

## LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

Figure 44. Subroutine DOICU Core Storage Map

OEC	JCT
774	01436
706	01302
764	01420
788	01424
792	01430
796	01434
800	01440
804	01444
808	01450
230	00346
638	01177
638	01176
439	00667
174	00256
543	01037
176	00260
542	00230
152	01036
404	00624

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	OCT
TAL LOCATIONS	
IFN	LOC
26	00201
3	00263
42	00347
48	00406
53	00422

Figure 44. Subroutine DOICU Core Storage Map  
(continued)

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15300	34 00427	15400	56 00440	15500	59 00461	15600	90 00483
15400	51 00471	15500	58 00451	15600	60 00462	15700	61 00463
15500	62 00472	15600	71 00474	15700	72 00475	15800	73 00476
15600	82 00470	15700	84 00472	15800	85 00473	15900	86 00474
15700	97 01041	15800	98 01042	15900	99 01043	16000	100 01044
15800	104 01045	15900	105 01046	16000	106 01047	16100	107 01048
15900	108 01049	16000	109 01050	16100	110 01051	16200	111 01052
16000	112 01053	16100	113 01054	16200	114 01055	16300	115 01056
16100	116 01057	16200	117 01058	16300	118 01059	16400	119 01060
16200	120 01061	16300	121 01062	16400	122 01063	16500	123 01064
16300	124 01065	16400	125 01066	16500	126 01067	16600	127 01068
16400	128 01069	16500	129 01070	16600	130 01071	16700	131 01072
16500	132 01073	16600	133 01074	16700	134 01075	16800	135 01076
16600	136 01077	16700	137 01078	16800	138 01079	16900	139 01080
16700	140 01081	16800	141 01082	16900	142 01083	17000	143 01084
16800	144 01085	16900	145 01086	17000	146 01087	17100	147 01088
16900	148 01089	17000	149 01090	17100	150 01091	17200	151 01092
17000	152 01093	17100	153 01094	17200	154 01095	17300	155 01096
17100	156 01097	17200	157 01098	17300	158 01099	17400	159 01100
17200	160 01101	17300	161 01102	17400	162 01103	17500	163 01104
17300	164 01105	17400	165 01106	17500	166 01107	17600	167 01108
17400	168 01109	17500	169 01110	17600	170 01111	17700	171 01112
17500	172 01113	17600	173 01114	17700	174 01115	17800	175 01116
17600	176 01117	17700	177 01118	17800	178 01119	17900	179 01120
17700	180 01121	17800	181 01122	17900	182 01123	18000	183 01124
17800	184 01125	17900	185 01126	18000	186 01127	18100	187 01128
17900	188 01129	18000	189 01130	18100	190 01131	18200	191 01132
18000	192 01133	18100	193 01134	18200	194 01135	18300	195 01136
18100	196 01137	18200	197 01138	18300	198 01139	18400	199 01140
18200	200 01141	18300	201 01142	18400	202 01143	18500	203 01144
18300	204 01145	18400	205 01146	18500	206 01147	18600	207 01148
18400	208 01149	18500	209 01150	18600	210 01151	18700	211 01152
18500	212 01153	18600	213 01154	18700	214 01155	18800	215 01156
18600	216 01157	18700	217 01158	18800	218 01159	18900	219 01160
18700	220 01161	18800	221 01162	18900	222 01163	19000	223 01164
18800	224 01165	18900	225 01166	19000	226 01167	19100	227 01168
18900	228 01169	19000	229 01170	19100	230 01171	19200	231 01172
19000	232 01173	19100	233 01174	19200	234 01175	19300	235 01176
19100	236 01177	19200	237 01178	19300	238 01179	19400	239 01180
19200	240 01181	19300	241 01182	19400	242 01183	19500	243 01184
19300	244 01185	19400	245 01186	19500	246 01187	19600	247 01188
19400	248 01189	19500	249 01190	19600	250 01191	19700	251 01192
19500	252 01193	19600	253 01194	19700	254 01195	19800	255 01196
19600	256 01197	19700	257 01198	19800	258 01199	19900	259 01200
19700	260 01201	19800	261 01202	19900	262 01203	20000	263 01204
19800	264 01205	19900	265 01206	20000	266 01207	20100	267 01208
19900	268 01209	20000	269 01210	20100	270 01211	20200	271 01212
20000	272 01213	20100	273 01214	20200	274 01215	20300	275 01216
20100	276 01217	20200	277 01218	20300	278 01219	20400	279 01220
20200	280 01221	20300	281 01222	20400	282 01223	20500	283 01224
20300	284 01225	20400	285 01226	20500	286 01227	20600	287 01228
20400	288 01229	20500	289 01230	20600	290 01231	20700	291 01232
20500	292 01233	20600	293 01234	20700	294 01235	20800	295 01236
20600	296 01237	20700	297 01238	20800	298 01239	20900	299 01240
20700	300 01241	20800	301 01242	20900	302 01243	21000	303 01244
20800	304 01245	20900	305 01246	21000	306 01247	21100	307 01248
20900	308 01249	21000	309 01250	21100	310 01251	21200	311 01252
21000	312 01253	21100	313 01254	21200	314 01255	21300	315 01256
21100	316 01257	21200	317 01258	21300	318 01259	21400	319 01260
21200	320 01261	21300	321 01262	21400	322 01263	21500	323 01264
21300	324 01265	21400	325 01266	21500	326 01267	21600	327 01268
21400	328 01269	21500	329 01270	21600	330 01271	21700	331 01272
21500	332 01273	21600	333 01274	21700	334 01275	21800	335 01276
21600	336 01277	21700	337 01278	21800	338 01279	21900	339 01280
21700	340 01281	21800	341 01282	21900	342 01283	22000	343 01284
21800	344 01285	21900	345 01286	22000	346 01287	22100	347 01288
21900	348 01289	22000	349 01290	22100	350 01291	22200	351 01292
22000	352 01293	22100	353 01294	22200	354 01295	22300	355 01296
22100	356 01297	22200	357 01298	22300	358 01299	22400	359 01300
22200	360 01301	22300	361 01302	22400	362 01303	22500	363 01304
22300	364 01305	22400	365 01306	22500	366 01307	22600	367 01308
22400	368 01309	22500	369 01310	22600	370 01311	22700	371 01312
22500	372 01313	22600	373 01314	22700	374 01315	22800	375 01316
22600	376 01317	22700	377 01318	22800	378 01319	22900	379 01320
22700	380 01321	22800	381 01322	22900	382 01323	23000	383 01324
22800	384 01325	22900	385 01326	23000	386 01327	23100	387 01328
22900	388 01329	23000	389 01330	23100	390 01331	23200	391 01332
23000	392 01333	23100	393 01334	23200	394 01335	23300	395 01336
23100	396 01337	23200	397 01338	23300	398 01339	23400	399 01340
23200	400 01341	23300	401 01342	23400	402 01343	23500	403 01344
23300	404 01345	23400	405 01346	23500	406 01347	23600	407 01348
23400	408 01349	23500	409 01350	23600	410 01351	23700	411 01352
23500	412 01353	23600	413 01354	23700	414 01355	23800	415 01356
23600	416 01357	23700	417 01358	23800	418 01359	23900	419 01360
23700	420 01361	23800	421 01362	23900	422 01363	24000	423 01364
23800	424 01365	23900	425 01366	24000	426 01367	24100	427 01368
23900	428 01369	24000	429 01370	24100	430 01371	24200	431 01372
24000	432 01373	24100	433 01374	24200	434 01375	24300	435 01376
24100	436 01377	24200	437 01378	24300	438 01379	24400	439 01380
24200	440 01381	24300	441 01382	24400	442 01383	24500	443 01384
24300	444 01385	24400	445 01386	24500	446 01387	24600	447 01388
24400	448 01389	24500	449 01390	24600	450 01391	24700	451 01392
24500	452 01393	24600	453 01394	24700	454 01395	24800	455 01396
24600	456 01397	24700	457 01398	24800	458 01399	24900	459 01400
24700	460 01401	24800	461 01402	24900	462 01403	25000	463 01404
24800	464 01405	24900	465 01406	25000	466 01407	25100	467 01408
24900	468 01409	25000	469 01410	25100	470 01411	25200	471 01412
25000	472 01413	25100	473 01414	25200	474 01415	25300	475 01416
25100	476 01417	25200	477 01418	25300	478 01419	25400	479 01420
25200	480 01421	25300	481 01422	25400	482 01423	25500	483 01424
25300	484 01425	25400	485 01426	25500	486 01427	25600	487 01428
25400	488 01429	25500	489 01430	25600	490 01431	25700	491 01432
25500	492 01433	25600	493 01434	25700	494 01435	25800	495 01436
25600	496 01437	25700	497 01438	25800	498 01439	25900	499 01440
25700	500 01441	25800	501 01442	25900	502 01443	26000	503 01444
25800	504 01445	25900	505 01446	26000	506 01447	26100	507 01448
25900	508 01449	26000	509 01450	26100	510 01451	26200	511 01452
26000	512 01453	26100	513 01454	26200	514 01455	26300	515 01456
26100	516 01457	26200	517 01458	26300	518 01459	26400	519 01460
26200	520 01461	26300	521 01462	26400	522 01463	26500	523 01464
26300	524 01465	26400	525 01466	26500	526 01467	26600	527 01468</

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C MAP (SUBROUTINE III) ANALYSIS AND PROGRAMMING BY K.A.TROUPS,NASASID,11/1/63
C MAP SUBROUTINE MAP
C GIVEN THE COORDINATES OF THE SURFACE FROM WHICH THE FACTOR IS DESIRED,
C THE COORDINATES OF THE SURFACE TO WHICH THE FACTOR IS TO BE COMPUTED,
C C PLANE POINT FACTOR TO THE RECEIVING SURFACE WILL BE COMPUTED.
C DIMENSION NITILE(24),NMS(5),TONI(5),NONTI(5),NCELS(5),IASC(5),
C JASC(5),CO
C JASC(5)=NOL(5),NMS(5)=1,5,10,15,20,25,30,35,40,45,50,55,60,65,70,75,80,85,90,95,100,105,110,115,120,125,130,135,140,145,150,155,160,165,170,175,180,185,190,195,200,205,210,215,220,225,230,235,240,245,250,255,260,265,270,275,280,285,290,295,300,305,310,315,320,325,330,335,340,345,350,355,360,365,370,375,380,385,390,395,400,405,410,415,420,425,430,435,440,445,450,455,460,465,470,475,480,485,490,495,500,505,510,515,520,525,530,535,540,545,550,555,560,565,570,575,580,585,590,595,600,605,610,615,620,625,630,635,640,645,650,655,660,665,670,675,680,685,690,695,700,705,710,715,720,725,730,735,740,745,750,755,760,765,770,775,780,785,790,795,800,805,810,815,820,825,830,835,840,845,850,855,860,865,870,875,880,885,890,895,900,905,910,915,920,925,930,935,940,945,950,955,960,965,970,975,980,985,990,995,1000,1005,1010,1015,1020,1025,1030,1035,1040,1045,1050,1055,1060,1065,1070,1075,1080,1085,1090,1095,1100,1105,1110,1115,1120,1125,1130,1135,1140,1145,1150,1155,1160,1165,1170,1175,1180,1185,1190,1195,1200,1205,1210,1215,1220,1225,1230,1235,1240,1245,1250,1255,1260,1265,1270,1275,1280,1285,1290,1295,1300,1305,1310,1315,1320,1325,1330,1335,1340,1345,1350,1355,1360,1365,1370,1375,1380,1385,1390,1395,1400,1405,1410,1415,1420,1425,1430,1435,1440,1445,1450,1455,1460,1465,1470,1475,1480,1485,1490,1495,1500,1505,1510,1515,1520,1525,1530,1535,1540,1545,1550,1555,1560,1565,1570,1575,1580,1585,1590,1595,1600,1605,1610,1615,1620,1625,1630,1635,1640,1645,1650,1655,1660,1665,1670,1675,1680,1685,1690,1695,1700,1705,1710,1715,1720,1725,1730,1735,1740,1745,1750,1755,1760,1765,1770,1775,1780,1785,1790,1795,1800,1805,1810,1815,1820,1825,1830,1835,1840,1845,1850,1855,1860,1865,1870,1875,1880,1885,1890,1895,1900,1905,1910,1915,1920,1925,1930,1935,1940,1945,1950,1955,1960,1965,1970,1975,1980,1985,1990,1995,2000,2005,2010,2015,2020,2025,2030,2035,2040,2045,2050,2055,2060,2065,2070,2075,2080,2085,2090,2095,2100,2105,2110,2115,2120,2125,2130,2135,2140,2145,2150,2155,2160,2165,2170,2175,2180,2185,2190,2195,2200,2205,2210,2215,2220,2225,2230,2235,2240,2245,2250,2255,2260,2265,2270,2275,2280,2285,2290,2295,2300,2305,2310,2315,2320,2325,2330,2335,2340,2345,2350,2355,2360,2365,2370,2375,2380,2385,2390,2395,2400,2405,2410,2415,2420,2425,2430,2435,2440,2445,2450,2455,2460,2465,2470,2475,2480,2485,2490,2495,2500,2505,2510,2515,2520,2525,2530,2535,2540,2545,2550,2555,2560,2565,2570,2575,2580,2585,2590,2595,2600,2605,2610,2615,2620,2625,2630,2635,2640,2645,2650,2655,2660,2665,2670,2675,2680,2685,2690,2695,2700,2705,2710,2715,2720,2725,2730,2735,2740,2745,2750,2755,2760,2765,2770,2775,2780,2785,2790,2795,2800,2805,2810,2815,2820,2825,2830,2835,2840,2845,2850,2855,2860,2865,2870,2875,2880,2885,2890,2895,2900,2905,2910,2915,2920,2925,2930,2935,2940,2945,2950,2955,2960,2965,2970,2975,2980,2985,2990,2995,3000,3005,3010,3015,3020,3025,3030,3035,3040,3045,3050,3055,3060,3065,3070,3075,3080,3085,3090,3095,3100,3105,3110,3115,3120,3125,3130,3135,3140,3145,3150,3155,3160,3165,3170,3175,3180,3185,3190,3195,3200,3205,3210,3215,3220,3225,3230,3235,3240,3245,3250,3255,3260,3265,3270,3275,3280,3285,3290,3295,3300,3305,3310,3315,3320,3325,3330,3335,3340,3345,3350,3355,3360,3365,3370,3375,3380,3385,3390,3395,3400,3405,3410,3415,3420,3425,3430,3435,3440,3445,3450,3455,3460,3465,3470,3475,3480,3485,3490,3495,3500,3505,3510,3515,3520,3525,3530,3535,3540,3545,3550,3555,3560,3565,3570,3575,3580,3585,3590,3595,3600,3605,3610,3615,3620,3625,3630,3635,3640,3645,3650,3655,3660,3665,3670,3675,3680,3685,3690,3695,3700,3705,3710,3715,3720,3725,3730,3735,3740,3745,3750,3755,3760,3765,3770,3775,3780,3785,3790,3795,3800,3805,3810,3815,3820,3825,3830,3835,3840,3845,3850,3855,3860,3865,3870,3875,3880,3885,3890,3895,3900,3905,3910,3915,3920,3925,3930,3935,3940,3945,3950,3955,3960,3965,3970,3975,3980,3985,3990,3995,4000,4005,4010,4015,4020,4025,4030,4035,4040,4045,4050,4055,4060,4065,4070,4075,4080,4085,4090,4095,4100,4105,4110,4115,4120,4125,4130,4135,4140,4145,4
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7364 MAP (CONFAC 11) ANALYSIS AND PROGRAMMING BY K.A.TOUPS,MAASID,11/1/63
110 YHIN=P12,K,MC}
120 PM=K,K,MDI=YMAX1200,200,175
175 YHAX=P12,M,DI
180 ME=K
200 CONTINUE
210 ME1=21-MH
220 ME1=1
225 GO 230 I=1,2
230 IF(I11745-260-250-240,240
240 MEJ,I1=1
245 IF(MJ,I11240,250,260
250 CONTINUE
260 MEJ,I1=1
265 IF(MJ,I11240,250,260
270 IF(MJ,I11240,250,260
275 IF(MJ,I11240,250,260
280 IF(MJ,I11240,250,260
285 IF(MJ,I11240,250,260
290 IF(MJ,I11240,250,260
295 IF(MJ,I11240,250,260
300 CONTINUE
305 INSTRUCTIONS COMPUTE THE POINTS OF INTERSECTION OF EACH
310 HORIZONTAL GRID LINE AND THE LINE SEGMENTS FORMING THE SURF BOUNDARY
315 COMPUTE THE VERTICAL INCREMENT
320 DY=YHAX-YMIN1/FL0AT(FN11)
325 CONTINUE
330 COMPUTE THE HORIZONTAL GRID LINES

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Figure 45. Subroutine MAP Listing  
(continued)

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Figure 45. Subroutine MAP Listing  
(continued)

73384 MAP (CONFAC II) ANALYSIS AND PROGRAMMING BY K.A.TOWNS,NAASID-11/1/63 11/07/73 PAGE 4

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C GO TO (NVL180,200,720
C NEXT MAPPING LINE AND NEXT BOUNDARY LINE SEGMENT
480 K=K+1
490 CONTINUE
500 CONTINUE
510 CONTINUE
520 MHT=MHT+1
530 AR=0
C COMPUTE THE MAPPING AREA
540 K=K+1
550 DX=X1(K,2)-X1(1,1)
560 AR=AR+DXL
570 AR=AR+DXL/2
580 AR=AR+DXL/2
590 RETURN
600 ENDD

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Figure 45. Subroutine MAP Listing  
(continued)

STORAGE NOT USED BY PROGRAM

DEC OCT  
510 00776  
14637 34455

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

ANAP 15169 35501	DEC OCT	AREA 21037 51113	DEC OCT	AREAX 21311 51023	DEC OCT	CI 2034 51116
C2 21745 52471	DEC OCT	C3 21795 52443	DEC OCT	CL 16140 37414	DEC OCT	DA 22134 53212
EN 15485 51516	DEC OCT	FA 13011 33245	DEC OCT	DF 13180 35512	DEC OCT	FA 14980 35721
INC 14649 34471	DEC OCT	FC 20976 50760	DEC OCT	KD 22154 53212	DEC OCT	KP 14492 36204
MR 20942 50716	DEC OCT	MSDU 14129 51401	DEC OCT	MSGL 16121 37371	DEC OCT	LP 16123 37373
NOA 22100 53124	DEC OCT	NOC 22112 53140	DEC OCT	NOL 21157 51245	DEC OCT	NGON 21114 53142
NOG 13189 35500	DEC OCT	ND 15494 36206	DEC OCT	NOT 22102 53126	DEC OCT	MHI 13184 35520
NS 21483 52275	DEC OCT	NSC 22123 51335	DEC OCT	NSD 22101 51126	DEC OCT	NSL 22217 63201
NSN 21269 51425	DEC OCT	NTITLE 21293 51455	DEC OCT	NVI 15184 35516	DEC OCT	NVL 15181 35515
NSP 14445 40075	DEC OCT	NSY 14445 40075	DEC OCT	NSY 14445 40075	DEC OCT	NSY 14445 40075
PA 14454 40106	DEC OCT	RA 14454 40106	DEC OCT	RY 20998 51006	DEC OCT	SI 22123 37372
SP 14445 40075	DEC OCT	TOA 22100 53124	DEC OCT	TOM 22114 53142	DEC OCT	INSIO 22101 53125
VA 15368 34010	DEC OCT	Y 14154 37432	DEC OCT	Z 15490 36202	DEC OCT	Z 14989 3555

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENTS

AR 509 00775	DEC OCT	DAL 508 00774	DEC OCT	MHI 507 00773	DEC OCT	11 506 00772
J 501 00765	DEC OCT	J 501 00765	DEC OCT	MN 499 00761	DEC OCT	MN 498 00762
PD 497 00761	DEC OCT	YMAX 496 00760	DEC OCT	YMIN 494 00757	DEC OCT	MR 495 00762

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC OCT	DEC OCT	DEC OCT	DEC OCT
11 509 00637	21 404 00635	31 400 00635	41 400 00635
A1102 404 00624	A1161 417 00441	A1162 432 00640	A1163 447 00677
C101 483 00743	C162 484 00744	C163 485 00745	C164 486 00746

Figure 16. Subroutine MAP Core Storage Listing







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C ZERO OUT COMPUTATIONAL ERROR
      F1=0.0
      F2=0.0
      F3=0.0
      F4=0.0
      F5=0.0
      F6=0.0
      F7=0.0
      F8=0.0
      F9=0.0
      F10=0.0
      F11=0.0
      F12=0.0
      F13=0.0
      F14=0.0
      F15=0.0
      F16=0.0
      F17=0.0
      F18=0.0
      F19=0.0
      F20=0.0
      F21=0.0
      F22=0.0
      F23=0.0
      F24=0.0
      F25=0.0
      F26=0.0
      F27=0.0
      F28=0.0
      F29=0.0
      F30=0.0
      F31=0.0
      F32=0.0
      F33=0.0
      F34=0.0
      F35=0.0
      F36=0.0
      F37=0.0
      F38=0.0
      F39=0.0
      F40=0.0
      F41=0.0
      F42=0.0
      F43=0.0
      F44=0.0
      F45=0.0
      F46=0.0
      F47=0.0
      F48=0.0
      F49=0.0
      F50=0.0
      F51=0.0
      F52=0.0
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      F54=0.0
      F55=0.0
      F56=0.0
      F57=0.0
      F58=0.0
      F59=0.0
      F60=0.0
      F61=0.0
      F62=0.0
      F63=0.0
      F64=0.0
      F65=0.0
      F66=0.0
      F67=0.0
      F68=0.0
      F69=0.0
      F70=0.0
      F71=0.0
      F72=0.0
      F73=0.0
      F74=0.0
      F75=0.0
      F76=0.0
      F77=0.0
      F78=0.0
      F79=0.0
      F80=0.0
      F81=0.0
      F82=0.0
      F83=0.0
      F84=0.0
      F85=0.0
      F86=0.0
      F87=0.0
      F88=0.0
      F89=0.0
      F90=0.0
      F91=0.0
      F92=0.0
      F93=0.0
      F94=0.0
      F95=0.0
      F96=0.0
      F97=0.0
      F98=0.0
      F99=0.0
      F100=0.0
      F101=0.0
      F102=0.0
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      F104=0.0
      F105=0.0
      F106=0.0
      F107=0.0
      F108=0.0
      F109=0.0
      F110=0.0
      F111=0.0
      F112=0.0
      F113=0.0
      F114=0.0
      F115=0.0
      F116=0.0
      F117=0.0
      F118=0.0
      F119=0.0
      F120=0.0
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      F123=0.0
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      F125=0.0
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      F127=0.0
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      F131=0.0
      F132=0.0
      F133=0.0
      F134=0.0
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      F164=0.0
      F165=0.0
      F166=0.0
      F167=0.0
      F168=0.0
      F169=0.0
      F170=0.0
      F171=0.0
      F172=0.0
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      F174=0.0
      F175=0.0
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      F177=0.0
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      F183=0.0
      F184=0.0
      F185=0.0
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Figure 47. Subroutine FACOR Listing (continued)

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905 PHII=PHI1+3.1415927
GO TO 900
C. COMPUTE THE COSINE PRODUCT OF VECTORS TO POINTS DEFINING LINE SEGMENT
910 F33=SQRT(F11*F22+*2)
C. COMPUTE THE COSINE OF ANGLE BETWEEN THE CIRCULAR SECTOR AND X-Y PLANE
C. IF COSINE IS POSITIVE, X=PRODUCT 1
C. IF COSINE IS NEGATIVE, X=PRODUCT 1
C. COMPUTE THE DOT PRODUCT SAME VECTORS
C. IF DOT PRODUCT IS POSITIVE, X=PRODUCT 1
C. COMPUTE THE ANGLE BETWEEN VECTORS IN RADIANS
910 AN=C3.1415927
IF (F33*F40+985.970)
GO TO 900
905 PHII=PHI1+1.5707963+C3G
GO TO 900
C. COMPUTE THE ANGLE BETWEEN VECTORS IN RADIANS
920 CONTINUE
C. A NEG. AREA RESULTS WHEN THE ORDER OF COMPUTATION REVERSES (THE BACKSIDE)
C. REVERSE THE ORDER OF COMPUTATION AND RECALCULATE THE AREA
C. RECALCULATE THE AREA AND RECALCULATE THE ANGLE
C. SURFACE WHICH SHOULD BE BUT IS NOT QUITE PLANNAR
903 PHII=PHI1+985.985+985
904 PHII=PHI1+11146.2831853
GO TO 900
C. IF A TAILORED PRINTOUT WAS REQUESTED, COMPUTE THE POINT FACTOR
910 I=IND(1971,984,971)
911 I=IND(1971,984,971)
912 I=IND(1971,984,971)
913 I=IND(1971,984,971)
914 I=IND(1971,984,971)
915 I=IND(1971,984,971)
916 I=IND(1971,984,971)
917 I=IND(1971,984,971)
918 I=IND(1971,984,971)
919 I=IND(1971,984,971)
920 F11=PHI1/20.2831853
C. IF THE COSINE OF THE ANGLE IS REACHED, USE THE MAP BOUNDARY VALUE
C. FOR THE POINT TO AVOID EARTH BUILDUP IN X
920 F11=PHI1/20.2831853
921 F11=PHI1/20.2831853
922 F11=PHI1/20.2831853
923 F11=PHI1/20.2831853
924 F11=PHI1/20.2831853
925 F11=PHI1/20.2831853
926 F11=PHI1/20.2831853
927 F11=PHI1/20.2831853
928 F11=PHI1/20.2831853
929 F11=PHI1/20.2831853
930 F11=PHI1/20.2831853
931 F11=PHI1/20.2831853
932 F11=PHI1/20.2831853
933 F11=PHI1/20.2831853
934 F11=PHI1/20.2831853
935 F11=PHI1/20.2831853
936 F11=PHI1/20.2831853
937 F11=PHI1/20.2831853
938 F11=PHI1/20.2831853
939 F11=PHI1/20.2831853
940 F11=PHI1/20.2831853
941 F11=PHI1/20.2831853
942 F11=PHI1/20.2831853
943 F11=PHI1/20.2831853
944 F11=PHI1/20.2831853
945 F11=PHI1/20.2831853
946 F11=PHI1/20.2831853
947 F11=PHI1/20.2831853
948 F11=PHI1/20.2831853
949 F11=PHI1/20.2831853
950 F11=PHI1/20.2831853
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960 F11=PHI1/20.2831853
961 F11=PHI1/20.2831853
962 F11=PHI1/20.2831853
963 F11=PHI1/20.2831853
964 F11=PHI1/20.2831853
965 F11=PHI1/20.2831853
966 F11=PHI1/20.2831853
967 F11=PHI1/20.2831853
968 F11=PHI1/20.2831853
969 F11=PHI1/20.2831853
970 F11=PHI1/20.2831853
971 F11=PHI1/20.2831853
972 F11=PHI1/20.2831853
973 F11=PHI1/20.2831853
974 F11=PHI1/20.2831853
975 F11=PHI1/20.2831853
976 F11=PHI1/20.2831853
977 F11=PHI1/20.2831853
978 F11=PHI1/20.2831853
979 F11=PHI1/20.2831853
980 F11=PHI1/20.2831853
981 F11=PHI1/20.2831853
982 F11=PHI1/20.2831853
983 F11=PHI1/20.2831853
984 F11=PHI1/20.2831853
985 F11=PHI1/20.2831853
986 F11=PHI1/20.2831853
987 F11=PHI1/20.2831853
988 F11=PHI1/20.2831853
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994 F11=PHI1/20.2831853
995 F11=PHI1/20.2831853
996 F11=PHI1/20.2831853
997 F11=PHI1/20.2831853
998 F11=PHI1/20.2831853
999 F11=PHI1/20.2831853

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Figure 47. Subroutine FACTOR Listing  
(continued)

73365 FACTORCONFACT III ANALYSIS AND PROGRAMMING BY K.A.L.O.U.P.S. HAASTO, 11/17/63 11/07/73 PAGE 4

```

974 CONTINUE
C DO 10 987
C MOVE THE CURVE THE POSITION OF THE POINT RELATIVE TO SURFACE 21 TO
C THE RIGHT AN INCREMENT AND CONTINUE
972 DO 975 J=1,ML
975 CALL MAP(J,JJ-DXIK)
987 CONTINUE
C INTEGRATE THE FUNCTION FH ALONG THE HORIZONTAL GRIC
988 DO 990 I=2,NMI
989 FV(I)=FV(I)+F(H(I)+F(H(ML))/2,1-DXIK)
990 CONTINUE
C INTEGRATE THE FUNCTION FV ALONG THE VERTICAL. DIVIDE BY 2 TO CONVERT
C FH TO AREA BY PI TO CONVERT M.I.D. TO REGULATION FACTOR, AND BY
C THE MAPPING AREA TO YIELD THE FORM FACTOR.
1000 F=0.500
1005 F=0.500
1010 F=0.500
1015 F=0.500
1020 F=0.500
1025 F=0.500
1030 F=0.500
1035 F=0.500
1040 F=0.500
1045 F=0.500
1050 F=0.500
1055 F=0.500
1060 F=0.500
1065 F=0.500
1070 F=0.500
1075 F=0.500
1080 F=0.500
1085 F=0.500
1090 F=0.500
1095 F=0.500
1100 F=0.500
1105 F=0.500
1110 F=0.500
1115 F=0.500
1120 F=0.500
1125 F=0.500
1130 F=0.500
1135 F=0.500
1140 F=0.500
1145 F=0.500
1150 F=0.500
1155 F=0.500
1160 F=0.500
1165 F=0.500
1170 F=0.500
1175 F=0.500
1180 F=0.500
1185 F=0.500
1190 F=0.500
1195 F=0.500
1200 F=0.500
1205 F=0.500
1210 F=0.500
1215 F=0.500
1220 F=0.500
1225 F=0.500
1230 F=0.500
1235 F=0.500
1240 F=0.500
1245 F=0.500
1250 F=0.500
1255 F=0.500
1260 F=0.500
1265 F=0.500
1270 F=0.500
1275 F=0.500
1280 F=0.500
1285 F=0.500
1290 F=0.500
1295 F=0.500
1300 F=0.500
1305 F=0.500
1310 F=0.500
1315 F=0.500
1320 F=0.500
1325 F=0.500
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1335 F=0.500
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1355 F=0.500
1360 F=0.500
1365 F=0.500
1370 F=0.500
1375 F=0.500
1380 F=0.500
1385 F=0.500
1390 F=0.500
1395 F=0.500
1400 F=0.500
1405 F=0.500
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1415 F=0.500
1420 F=0.500
1425 F=0.500
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1435 F=0.500
1440 F=0.500
1445 F=0.500
1450 F=0.500
1455 F=0.500
1460 F=0.500
1465 F=0.500
1470 F=0.500
1475 F=0.500
1480 F=0.500
1485 F=0.500
1490 F=0.500
1495 F=0.500
1500 F=0.500
1505 F=0.500
1510 F=0.500
1515 F=0.500
1520 F=0.500
1525 F=0.500
1530 F=0.500
1535 F=0.500
1540 F=0.500
1545 F=0.500
1550 F=0.500
1555 F=0.500
1560 F=0.500
1565 F=0.500
1570 F=0.500
1575 F=0.500
1580 F=0.500
1585 F=0.500
1590 F=0.500
1595 F=0.500
1600 F=0.500
1605 F=0.500
1610 F=0.500
1615 F=0.500
1620 F=0.500
1625 F=0.500
1630 F=0.500
1635 F=0.500
1640 F=0.500
1645 F=0.500
1650 F=0.500
1655 F=0.500
1660 F=0.500
1665 F=0.500
1670 F=0.500
1675 F=0.500
1680 F=0.500
1685 F=0.500
1690 F=0.500
1695 F=0.500
1700 F=0.500
1705 F=0.500
1710 F=0.500
1715 F=0.500
1720 F=0.500
1725 F=0.500
1730 F=0.500
1735 F=0.500
1740 F=0.500
1745 F=0.500
1750 F=0.500
1755 F=0.500
1760 F=0.500
1765 F=0.500
1770 F=0.500
1775 F=0.500
1780 F=0.500
1785 F=0.500
1790 F=0.500
1795 F=0.500
1800 F=0.500
1805 F=0.500
1810 F=0.500
1815 F=0.500
1820 F=0.500
1825 F=0.500
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1835 F=0.500
1840 F=0.500
1845 F=0.500
1850 F=0.500
1855 F=0.500
1860 F=0.500
1865 F=0.500
1870 F=0.500
1875 F=0.500
1880 F=0.500
1885 F=0.500
1890 F=0.500
1895 F=0.500
1900 F=0.500
1905 F=0.500
1910 F=0.500
1915 F=0.500
1920 F=0.500
1925 F=0.500
1930 F=0.500
1935 F=0.500
1940 F=0.500
1945 F=0.500
1950 F=0.500
1955 F=0.500
1960 F=0.500
1965 F=0.500
1970 F=0.500
1975 F=0.500
1980 F=0.500
1985 F=0.500
1990 F=0.500
1995 F=0.500
2000 RETURN
END

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Figure 47. Subroutine FACTOR Listing  
(continued)





[illegible]



36604000

35637900

Subroutine :  
(continued)

72386 SILFACONFAC II ANALYSIS AND PROGRAMMING BY N.A.TOUSS-NAASIO.11/1/73 11/08/85 PAGE 4

```

      DO 11700 K=1,4
      C PICKUP CONNECTING POINT K1 TO POINT J IN SURFACE ID
      C IF A2 IS ZERO, NO DATA IN THIS SPOT- CONTINUE
      C IF A2 IS NOT ZERO, UPDATE SURFACE ID TO 11700+11600
      C UPDATE NO OF CONNECTIONS COMPLET
      11600 K2=K2+1
      C UPDATE CONNECTING POINT NO TO TOTAL OF POINTS BEGINNING COMPOSITE SURFACE
      C UPDATING SURFACE ID TO NEXT COMPOSITE SURFACE
      C WITH NEW COMPOSITE SURFACE POINT NUMBER N.
      11700 K2=K2+1
      C LOAD TOTAL NO OF POINTS CONNECTING TO NEW POINT NO N.
      N=K2+1
      15000 K=K+1
      C SET CONNECTIONS PROCESSING FLAG TO NONZERO(ONLY ONE ENTRY REQD)
      K=K+1
      C START LOOP TO DETERMINE SILHOUETTE FROM LINE SEGMENTS PROJECTED ON Z=13000+100
      C PLANE AND COMPUTE POINT FACTOR FROM THIS SILHOUETTE.
      12100 UO=087 MM=1,NML
      12150 IF(FH(MH))GO TO 12150+12150
      12200 DSC=XK+Z*YSPZ
      U=SQRT(DSC)
      FH(MH)=U
      12300 IF(MH<1)GO TO 12300+986+12300
      12350 IF(MH<1)GO TO 12350+986+12350
      12350 BETA=SQRT(FASZES/ALPHA)
      FH(MH)=A*TAN(BETA)-PI+A TAN(BETA+D/(3+1.IN))-ALPHA+BETA/DSQ
      12400 FH(MH)=FH(MH)+FASZES/ALPHA
      GO TO 206
      C COMPUTE INTERCEPTS, SLOPES, ANGLES AND Y-INTERCEPTS
      12800 NLS=N-1
      SENSE=LIGH. 0
      C PICKUP NO. OF POINTS CONNECTING TO POINT I.
      NP=MH+1
    
```

Figure 49. Subroutine SILFAC Listing  
(continued)

```

DO 400 J=1,NP
C PICKUP A POINT CONNECTING TO I.
C THE SLOPE OF LINE SEGMENT FROM I TO J IS THE SAME AS J TO I. IF THE
C CONNECTING POINT IS NUMERICALLY LESS THAN POINT, THE SLOPE AND
C SLOPE OF LINE SEGMENT FROM I TO J IS THE SAME AS J TO I. IF THE
C IF NP IS GREATER THAN I, GO TO COMPUTE LINE SEGMENT PARAMETERS.
      IF1 NPI235-400,400
C SEARCH FOR MINIMUM DISTANCE FROM CONNECTIONS TO HPP.
      DO 240 M=1,1
      227 IF HPP(I,NPI)-I240,260,240
      228 IF HPP(I,NPI)-I240,260,240
      229 IF HPP(I,NPI)-I240,260,240
      230 IF HPP(I,NPI)-I240,260,240
      231 IF HPP(I,NPI)-I240,260,240
      232 IF HPP(I,NPI)-I240,260,240
      233 IF HPP(I,NPI)-I240,260,240
      234 IF HPP(I,NPI)-I240,260,240
      235 IF HPP(I,NPI)-I240,260,240
      236 IF HPP(I,NPI)-I240,260,240
      237 IF HPP(I,NPI)-I240,260,240
      238 IF HPP(I,NPI)-I240,260,240
      239 IF HPP(I,NPI)-I240,260,240
      240 IF HPP(I,NPI)-I240,260,240
      241 IF HPP(I,NPI)-I240,260,240
      242 IF HPP(I,NPI)-I240,260,240
      243 IF HPP(I,NPI)-I240,260,240
      244 IF HPP(I,NPI)-I240,260,240
      245 IF HPP(I,NPI)-I240,260,240
      246 IF HPP(I,NPI)-I240,260,240
      247 IF HPP(I,NPI)-I240,260,240
      248 IF HPP(I,NPI)-I240,260,240
      249 IF HPP(I,NPI)-I240,260,240
      250 IF HPP(I,NPI)-I240,260,240
      251 IF HPP(I,NPI)-I240,260,240
      252 IF HPP(I,NPI)-I240,260,240
      253 IF HPP(I,NPI)-I240,260,240
      254 IF HPP(I,NPI)-I240,260,240
      255 IF HPP(I,NPI)-I240,260,240
      256 IF HPP(I,NPI)-I240,260,240
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      274 IF HPP(I,NPI)-I240,260,240
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      312 IF HPP(I,NPI)-I240,260,240
      313 IF HPP(I,NPI)-I240,260,240
      314 IF HPP(I,NPI)-I240,260,240
      315 IF HPP(I,NPI)-I240,260,240
      316 IF HPP(I,NPI)-I240,260,240
      317 IF HPP(I,NPI)-I240,260,240
      318 IF HPP(I,NPI)-I240,260,240
      319 IF HPP(I,NPI)-I240,260,240
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      396 IF HPP(I,NPI)-I240,260,240
      397 IF HPP(I,NPI)-I240,260,240
      398 IF HPP(I,NPI)-I240,260,240
      399 IF HPP(I,NPI)-I240,260,240
      400 IF HPP(I,NPI)-I240,260,240

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C IF NOT CLASS B SURFACE, THE FOLLOWING LINE ELEMENTS ARE NOT NEEDED

Figure 49. Subroutine SIFAC Listing  
(continued)

73366 SILFACONFAC II:ANALYSIS AND PROGRAMMING BY K.A.T.O.PS.NAA:ID:11/7/63 11/04/63 PAGE 6

```

370 JFIMG1375,400,375
C COMPUTE INTERCEPT BASED ON PNT TO INCREASE COMPUTATIONAL ACCURACY
1270 JFIMG1375,400,375
1280 JFIMG1375,400,375
1290 JFIMG1375,400,375
1300 JFIMG1375,400,375
1310 JFIMG1375,400,375
1320 JFIMG1375,400,375
1330 JFIMG1375,400,375
1340 JFIMG1375,400,375
1350 JFIMG1375,400,375
1360 JFIMG1375,400,375
1370 JFIMG1375,400,375
1380 JFIMG1375,400,375
1390 JFIMG1375,400,375
1400 JFIMG1375,400,375
1410 JFIMG1375,400,375
1420 JFIMG1375,400,375
1430 JFIMG1375,400,375
1440 JFIMG1375,400,375
1450 JFIMG1375,400,375
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1470 JFIMG1375,400,375
1480 JFIMG1375,400,375
1490 JFIMG1375,400,375
1500 JFIMG1375,400,375
1510 JFIMG1375,400,375
1520 JFIMG1375,400,375
1530 JFIMG1375,400,375
1540 JFIMG1375,400,375
1550 JFIMG1375,400,375
1560 JFIMG1375,400,375
1570 JFIMG1375,400,375
1580 JFIMG1375,400,375
1590 JFIMG1375,400,375
1600 JFIMG1375,400,375
1610 JFIMG1375,400,375
1620 JFIMG1375,400,375
1630 JFIMG1375,400,375
1640 JFIMG1375,400,375
1650 JFIMG1375,400,375
1660 JFIMG1375,400,375
1670 JFIMG1375,400,375
1680 JFIMG1375,400,375
1690 JFIMG1375,400,375
1700 JFIMG1375,400,375
1710 JFIMG1375,400,375
1720 JFIMG1375,400,375
1730 JFIMG1375,400,375
1740 JFIMG1375,400,375
1750 JFIMG1375,400,375
1760 JFIMG1375,400,375
1770 JFIMG1375,400,375
1780 JFIMG1375,400,375
1790 JFIMG1375,400,375
1800 JFIMG1375,400,375
1810 JFIMG1375,400,375
1820 JFIMG1375,400,375
1830 JFIMG1375,400,375
1840 JFIMG1375,400,375
1850 JFIMG1375,400,375
1860 JFIMG1375,400,375
1870 JFIMG1375,400,375
1880 JFIMG1375,400,375
1890 JFIMG1375,400,375
1900 JFIMG1375,400,375
1910 JFIMG1375,400,375
1920 JFIMG1375,400,375
1930 JFIMG1375,400,375
1940 JFIMG1375,400,375
1950 JFIMG1375,400,375
1960 JFIMG1375,400,375
1970 JFIMG1375,400,375
1980 JFIMG1375,400,375
1990 JFIMG1375,400,375
2000 JFIMG1375,400,375

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Figure 49. Subroutine SILFAC Listing  
(continued)

72360 SILFAC(COMPAC III) ANALYSIS AND PROGRAMMING BY K.A. TOUPS, NASA ID: 11/1/63 11/03/63 PAGE 7

```

110 MLEP=NP
115 IF (SENSE LIGHT 2)
120 SENSE LIGHT 2
125 SENSE LIGHT 2
130 SENSE LIGHT 2
135 SENSE LIGHT 2
140 NP=NP+1
145 IF (NP=NP+1) NP
150 IF (SENSE LIGHT 1) 160, 180, 180
155 IF (SENSE LIGHT 2) 170, 190
160 SENSE LIGHT 3
165 SENSE LIGHT 3
170 J=J+1
175 IF (N=1190.175, 190)
180 GOTO 1200
185 GOTO 1200
190 M=MX+1
195 IF (M=MX)
200 CONTINUE
205 IF (SENSE LIGHT 3) 195, 835
210 IF (SENSE LIGHT 4) 195, 835
215 GOTO 140
220 CONTINUE
225 YIL(JR, NP)=1.
230 YIL(JR, NP)=YMIN-XIL
235 YIL(JR, NP)=YMIN
240 YIL(JR, NP)=YMIN
245 C M=NO. OF POINTS DEFINING SILHOUETTE
250 C XI= X-VALUE OF HEAD OF DEPARTURE VECTOR
255 C X2= X-VALUE OF BASE OF DEPARTURE VECTOR
260 C XI=XIL-1.
265 C X2=XIL-1.
270 C XI=XIL-1.
275 C XI=XIL-1.
280 C XI=XIL-1.
285 C XI=XIL-1.
290 C XI=XIL-1.
295 C XI=XIL-1.
300 C XI=XIL-1.
305 C XI=XIL-1.
310 C XI=XIL-1.
315 C XI=XIL-1.
320 C XI=XIL-1.
325 C XI=XIL-1.
330 C XI=XIL-1.
335 C XI=XIL-1.
340 C XI=XIL-1.
345 C XI=XIL-1.
350 C XI=XIL-1.
355 C XI=XIL-1.
360 C XI=XIL-1.
365 C XI=XIL-1.
370 C XI=XIL-1.
375 C XI=XIL-1.
380 C XI=XIL-1.
385 C XI=XIL-1.
390 C XI=XIL-1.
395 C XI=XIL-1.
400 C XI=XIL-1.
405 C XI=XIL-1.
410 C XI=XIL-1.
415 C XI=XIL-1.
420 C XI=XIL-1.
425 C XI=XIL-1.
430 C XI=XIL-1.
435 C XI=XIL-1.
440 C XI=XIL-1.
445 C XI=XIL-1.
450 C XI=XIL-1.
455 C XI=XIL-1.
460 C XI=XIL-1.
465 C XI=XIL-1.
470 C XI=XIL-1.
475 C XI=XIL-1.
480 C XI=XIL-1.
485 C XI=XIL-1.
490 C XI=XIL-1.
495 C XI=XIL-1.
500 C XI=XIL-1.
505 C XI=XIL-1.
510 C XI=XIL-1.
515 C XI=XIL-1.
520 C XI=XIL-1.
525 C XI=XIL-1.
530 C XI=XIL-1.
535 C XI=XIL-1.
540 C XI=XIL-1.
545 C XI=XIL-1.
550 C XI=XIL-1.
555 C XI=XIL-1.
560 C XI=XIL-1.
565 C XI=XIL-1.
570 C XI=XIL-1.
575 C XI=XIL-1.
580 C XI=XIL-1.
585 C XI=XIL-1.
590 C XI=XIL-1.
595 C XI=XIL-1.
600 C XI=XIL-1.
605 C XI=XIL-1.
610 C XI=XIL-1.
615 C XI=XIL-1.
620 C XI=XIL-1.
625 C XI=XIL-1.
630 C XI=XIL-1.
635 C XI=XIL-1.
640 C XI=XIL-1.
645 C XI=XIL-1.
650 C XI=XIL-1.
655 C XI=XIL-1.
660 C XI=XIL-1.
665 C XI=XIL-1.
670 C XI=XIL-1.
675 C XI=XIL-1.
680 C XI=XIL-1.
685 C XI=XIL-1.
690 C XI=XIL-1.
695 C XI=XIL-1.
700 C XI=XIL-1.
705 C XI=XIL-1.
710 C XI=XIL-1.
715 C XI=XIL-1.
720 C XI=XIL-1.
725 C XI=XIL-1.
730 C XI=XIL-1.
735 C XI=XIL-1.
740 C XI=XIL-1.
745 C XI=XIL-1.
750 C XI=XIL-1.
755 C XI=XIL-1.
760 C XI=XIL-1.
765 C XI=XIL-1.
770 C XI=XIL-1.
775 C XI=XIL-1.
780 C XI=XIL-1.
785 C XI=XIL-1.
790 C XI=XIL-1.
795 C XI=XIL-1.
800 C XI=XIL-1.
805 C XI=XIL-1.
810 C XI=XIL-1.
815 C XI=XIL-1.
820 C XI=XIL-1.
825 C XI=XIL-1.
830 C XI=XIL-1.
835 C XI=XIL-1.
840 C XI=XIL-1.
845 C XI=XIL-1.
850 C XI=XIL-1.
855 C XI=XIL-1.
860 C XI=XIL-1.
865 C XI=XIL-1.
870 C XI=XIL-1.
875 C XI=XIL-1.
880 C XI=XIL-1.
885 C XI=XIL-1.
890 C XI=XIL-1.
895 C XI=XIL-1.
900 C XI=XIL-1.
905 C XI=XIL-1.
910 C XI=XIL-1.
915 C XI=XIL-1.
920 C XI=XIL-1.
925 C XI=XIL-1.
930 C XI=XIL-1.
935 C XI=XIL-1.
940 C XI=XIL-1.
945 C XI=XIL-1.
950 C XI=XIL-1.
955 C XI=XIL-1.
960 C XI=XIL-1.
965 C XI=XIL-1.
970 C XI=XIL-1.
975 C XI=XIL-1.
980 C XI=XIL-1.
985 C XI=XIL-1.
990 C XI=XIL-1.
995 C XI=XIL-1.

```

Figure 49. Subroutine SILFAC Listing  
(continued)

[illegible]Subroutine SIFAC Listing  
(continued)

674	IFABSF5FVALJH,NPPI	-VALJ,11-7,599,9167+,-400,+400	36631000
675	XA=Z(NPP)		36631150
676	XA=V(NPP)		36631200
677	XA=V(LJ,1)-Y(LJH,NPPI)/CD		36631250
678	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631300
679	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631350
680	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631400
681	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631450
682	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631500
683	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631550
684	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631600
685	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631650
686	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631700
687	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631750
688	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631800
689	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631850
690	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631900
691	IFABSF5FAXI=-L-E-312400,+1400,+2500		36631950
692	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632000
693	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632050
694	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632100
695	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632150
696	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632200
697	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632250
698	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632300
699	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632350
700	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632400
701	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632450
702	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632500
703	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632550
704	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632600
705	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632650
706	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632700
707	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632750
708	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632800
709	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632850
710	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632900
711	IFABSF5FAXI=-L-E-312400,+1400,+2500		36632950
712	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633000
713	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633050
714	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633100
715	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633150
716	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633200
717	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633250
718	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633300
719	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633350
720	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633400
721	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633450
722	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633500
723	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633550
724	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633600
725	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633650
726	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633700
727	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633750
728	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633800
729	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633850
730	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633900
731	IFABSF5FAXI=-L-E-312400,+1400,+2500		36633950
732	IFABSF5FAXI=-L-E-312400,+1400,+2500		36634000
733	IFABSF5FAXI=-L-E-312400,+1400,+2500		36634050
734	IFABSF5FAXI=-L-E-312400,+1400,+2500		36634100
735	IFABSF5FAXI=-L-E-312400,+1400,+2500		36634150
736	IFABSF5FAXI=-L-E-312400,+1400,+2500		36634200
737	IFABSF5FAXI=-L-E-312400,+1400,+2500		36634250
738	IFABSF5FAXI=-L-E-312400,+1400,+2500		36634300
739	IFABSF5FAXI=-L-E-312400,+1400,+2500		36634350
740	IFABSF5FAXI=-L-E-312400,+1400,+2500		

Figure 49. Subroutine SIIFAC Listing  
(continued)



[illegible]

Figure 49. Subroutine SIFAC Listing  
(continued)

```

904 CONTINUE
902 IF (M305,803,805)
903 GO TO 835
805 M=1
      IF (M450,4550,4560)
806 X=X(NPP)
807 Y=Y(NPP)
808 IF (M450,810,2600)
809 IF (M450,810,810)
810 IF (M450,810,810)
811 IF (M450,810,810)
812 IF (M450,810,810)
813 IF (M450,810,810)
814 IF (M450,810,810)
815 IF (M450,810,810)
816 IF (M450,810,810)
817 IF (M450,810,810)
818 IF (M450,810,810)
819 IF (M450,810,810)
820 IF (M450,810,810)
821 IF (M450,810,810)
822 IF (M450,810,810)
823 IF (M450,810,810)
824 IF (M450,810,810)
825 IF (M450,810,810)
826 IF (M450,810,810)
827 IF (M450,810,810)
828 IF (M450,810,810)
829 IF (M450,810,810)
830 IF (M450,810,810)
831 IF (M450,810,810)
832 IF (M450,810,810)
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834 IF (M450,810,810)
835 IF (M450,810,810)
836 IF (M450,810,810)
837 IF (M450,810,810)
838 IF (M450,810,810)
839 IF (M450,810,810)
840 IF (M450,810,810)
841 IF (M450,810,810)
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864 IF (M450,810,810)
865 IF (M450,810,810)
866 IF (M450,810,810)
867 IF (M450,810,810)
868 IF (M450,810,810)
869 IF (M450,810,810)
870 IF (M450,810,810)
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874 IF (M450,810,810)
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937 IF (M450,810,810)
938 IF (M450,810,810)
939 IF (M450,810,810)
940 IF (M450,810,810)
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942 IF (M450,810,810)
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946 IF (M450,810,810)
947 IF (M450,810,810)
948 IF (M450,810,810)
949 IF (M450,810,810)
950 IF (M450,810,810)
951 IF (M450,810,810)
952 IF (M450,810,810)
953 IF (M450,810,810)
954 IF (M450,810,810)
955 IF (M450,810,810)
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959 IF (M450,810,810)
960 IF (M450,810,810)
961 IF (M450,810,810)
962 IF (M450,810,810)
963 IF (M450,810,810)
964 IF (M450,810,810)
965 IF (M450,810,810)
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967 IF (M450,810,810)
968 IF (M450,810,810)
969 IF (M450,810,810)
970 IF (M450,810,810)
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974 IF (M450,810,810)
975 IF (M450,810,810)
976 IF (M450,810,810)
977 IF (M450,810,810)
978 IF (M450,810,810)
979 IF (M450,810,810)
980 IF (M450,810,810)
981 IF (M450,810,810)
982 IF (M450,810,810)
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986 IF (M450,810,810)
987 IF (M450,810,810)
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992 IF (M450,810,810)
993 IF (M450,810,810)
994 IF (M450,810,810)
995 IF (M450,810,810)
996 IF (M450,810,810)
997 IF (M450,810,810)
998 IF (M450,810,810)
999 IF (M450,810,810)
1000 IF (M450,810,810)

```

Figure 49. Subroutine SILFAC Listing  
(continued)

[illegible]

Figure 49. Subroutine SIIFAC Listing  
(continued)





STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS			
DEC1	DEC1	DEC1	DEC1
Q11	3559 01017	NP	3519 04273
MJM	3559 01017	N5	3519 04273
XV	3259 04273	VV	3219 04271

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN DIMENSION, OR EQUIVALENCE STATEMENTS			
DEC1	DEC1	DEC1	DEC1
ALPHA	3311 04453	BETA	3351 04461
DELTA	3311 04453	DELTA	3351 04461
OMEGA	3311 04453	OMEGA	3351 04461
PHI	3311 04453	PHI	3351 04461
PSI	3311 04453	PSI	3351 04461
THETA	3311 04453	THETA	3351 04461
ZETA	3311 04453	ZETA	3351 04461
ETA	3311 04453	ETA	3351 04461
THETA	3311 04453	THETA	3351 04461
PHI	3311 04453	PHI	3351 04461
PSI	3311 04453	PSI	3351 04461
THETA	3311 04453	THETA	3351 04461
ZETA	3311 04453	ZETA	3351 04461
ETA	3311 04453	ETA	3351 04461
THETA	3311 04453	THETA	3351 04461
PHI	3311 04453	PHI	3351 04461
PSI	3311 04453	PSI	3351 04461
THETA	3311 04453	THETA	3351 04461
ZETA	3311 04453	ZETA	3351 04461
ETA	3311 04453	ETA	3351 04461
THETA	3311 04453	THETA	3351 04461
PHI	3311 04453	PHI	3351 04461
PSI	3311 04453	PSI	3351 04461
THETA	3311 04453	THETA	3351 04461
ZETA	3311 04453	ZETA	3351 04461
ETA	3311 04453	ETA	3351 04461
THETA	3311 04453	THETA	3351 04461
PHI	3311 04453	PHI	3351 04461
PSI	3311 04453	PSI	3351 04461
THETA	3311 04453	THETA	3351 04461
ZETA	3311 04453	ZETA	3351 04461
ETA	3311 04453	ETA	3351 04461
THETA	3311 04453	THETA	3351 04461
PHI	3311 04453	PHI	3351 04461
PSI	3311 04453	PSI	3351 04461
THETA	3311 04453	THETA	3351 04461
ZETA	3311 04453	ZETA	3351 04461
ETA	3311 04453	ETA	3351 04461
THETA	3311 04453	THETA	3351 04461
PHI	3311 04453	PHI	3351 04461
PSI	3311 04453	PSI	3351 04461
THETA	3311 04453	THETA	3351 04461
ZETA	3311 04453	ZETA	3351 04461
ETA	3311 04453	ETA	3351 04461
THETA	3311 04453	THETA	3351 04461
PHI	3311 04453	PHI	3351 04461
PSI	3311 04453	PSI	3351 04461
THETA	3311 04453	THETA	3351 04461
ZETA	3311 04453	ZETA	3351 04461
ETA	3311 04453	ETA	3351 04461
THETA	3311 04453	THETA	3351 04461
PHI	3311 04453	PHI	3351 04461
PSI	3311 04453	PSI	3351 04461
THETA	3311 04453	THETA	3351 04461
ZETA	3311 04453	ZETA	3351 04461
ETA	3311 04453	ETA	3351 04461
THETA	3311 04453	THETA	3351 04461
PHI	3311 04453	PHI	3351 04461
PSI	3311 04453	PSI	3351 04461
THETA	3311 04453	THETA	3351 04461
ZETA	3311 04453	ZETA	3351 04461
ETA	3311 04453	ETA	3351 04461
THETA	3311 04453	THETA	3351 04461
PHI	3311 04453	PHI	3351 04461
PSI	3311 04453	PSI	3351 04461
THETA	3311 04453	THETA	3351 04461
ZETA	3311 04453	ZETA	3351 04461
ETA	3311 04453	ETA	3351 04461
THETA	3311 04453	THETA	3351 04461

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IO 4383 04447	F52 2342 04440	F53 2341 04445	IO 2340 04444
IR 4385 04437	F51 2339 04436	JX 2335 04435	IR 2331 04434
KK 4331 04433	K 2330 04432	L 2329 04431	LT 2321 04430
LL 4333 04427	MEAR 2332 04426	NH 2321 04425	NO 2320 04420
NLP 4319 04417	AL 2318 04416	NLS 2317 04415	NOP 2311 04414
NPC 4313 04413	MPP 2314 04412	NPX 2313 04411	PSMR 2312 04410
PAK 2367 04403	RSOZ 2306 04402	SLR 2305 04401	TOL 2304 04400
TOL2 2303 04377	TOL3 2302 04376	TOL4 2301 04375	TOL 2300 04374
TOL2 2303 04377	VAR 2300 04374	XB 2299 04365	XT 2292 04364
XD 4291 04363	XA 2294 04362	XF 2289 04361	XG 2268 04360
XMIN 4287 04357	XM 2286 04356	XYMIN 2285 04352	Y 2266 04350
YSC 2279 04347	YMIN 2285 04352	YSPZ 2285 04352	

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

EFN	LOC	EFN	LOC	EFN	LOC
411UP	1999 04086	8145B	5000 04266	8145I	5010 04216
LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM					
UEC	QCT	UEC	QCT	UEC	QCT
11 2231 04267	21 2055 04067	31 2068 04024	61 2059 04021		
A11C2 2055 03643	A11C3 1868 03600	A11C4 1881 03615	A11C5 1994 03712		
A11C7 2005 04277	A11C8 2007 04274	A11C9 2010 04275	A11C0 2018 04276		
C1C5 2239 04277	C1C6 2240 04300	C1C7 2241 04301	C1C8 2242 04302		
C1C9 2243 04303	C1C0 2244 04304	C1C8 2245 04305	C1C0 2246 04306		
C1C0 2251 04313	C1C1 2252 04314	C1C2 2253 04315	C1C3 2254 04316		
C1C4 2255 04317	C1C5 2256 04320	C1C6 2257 04321	C1C7 2258 04322		
C1C8 2263 04322	C1C9 2264 04323	C1C0 2265 04324	C1C1 2266 04325		
C1C2 2267 04333	C1C3 2268 04334	C1C4 2269 04335	C1C5 2270 04336		
C1C6 2271 04337	C1C7 2272 04340	C1C8 2273 04341	C1C9 2274 04342		
C1C0 2275 04343	C1C1 2276 04344	C1C2 2277 04345	C1C3 2278 04346		

Figure 50. Subroutine SIFAC Core Storage Map  
(continued)

```

D11C5 303 00457 01114 351 00537 01132 712 01310 01121 738 01342
D112K 768 01400 01129 401 01441 0114K 1208 02270 01158 1441 02641
D112M 1451 04023 0115M 1250 03021 0115K 1383 03057 01166 1751 03127
D112P 1451 04023 0115M 1250 03021 0115K 1383 03057 01166 1751 03127
D12C 249 0441 0121C 402 00716 01111 505 00771 0111M 533 01025
D21P 543 01037 01223 601 01131 01224 609 01141 01225 618 01152
D22P 543 01037 01223 601 01131 01224 609 01141 01225 618 01152
D23V 107 01111 01245 1116 01134 0126K 1210 03272 0126M 1078 03096
D262 1691 01223 01266 1761 03361 01269 1766 03346 01280 1782 03366
D31M 1818 01705 0126V 1807 03350 01274 1921 03613 01275 1302 00456
D31M 1818 01705 0126V 1807 03350 01274 1921 03613 01275 1302 00456
D336K 1766 03340 01269 1765 03345 0136H 1837 03455 0136U 1889 03541
D3375 1945 03031 01376 1949 03635 0140E 130 00202 0140C 172 00224
D342 747 01553 0142E 644 01514 01431 907 01515 01433 911 01545
D44K 1335 04467 0145F 1485 02715 01451 1560 03030 0145A 1616 03120
D45K 1639 03136 0145K 1639 03136 0145J 1815 03427 01510 174 00504
D55K 1555 03027 0155K 1639 03136 0156J 1815 03427 0156J 1815 03427
D66P 286 0414 0162A 608 01140 0162J 746 01352 0162T 843 01513
D633 732 01644 0165P 1615 03117 0166V 1895 03547 01705 301 00455
D67 144 01360 01776 1948 01634 0177E 1888 03540 0177E 1888 03540
D775 144 01360 01776 1948 01634 0177E 1888 03540 0177E 1888 03540
E1M 467 02413 0177E 1888 03540 0177E 1888 03540 0177E 1888 03540
E1M 467 02413 0177E 1888 03540 0177E 1888 03540 0177E 1888 03540
E135 986 0426 0177E 1888 03540 0177E 1888 03540 0177E 1888 03540
E15P 4507 03107 0177E 1888 03540 0177E 1888 03540 0177E 1888 03540

```

## LOCATIONS OF NAMES IN TRANSFER VECTOR

```

A TAN DEC OCT DUMP DEC OCT DEC OCT
TIMEV 2 0002 0 0000 5 0005 1 00001
6 0006 3 0003

A TAN COUNTRY DUMP 3CAT TIMEV (FILE) (5PH)
ENTRY PRINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

```

Figure 50. Subroutine SIFAC Core Storage Map (continued)





Indicated by green arrow

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		2/14/74	PAGE 1
* 7090 FORTRAN INPUT-OUTPUT COMPATIBILITY ROUTINE CAUSES			
* 'READ N, LIST' TO BE EXECUTED AS 'READ INPUT TAPE			00000003.
* 'WRITE OUTPUT TAPE M2, N, LIST, AND PUNCH N, LIST'			00000004.
* TO BE EXECUTED AS 'WRITE OUTPUT TAPE M3, M, LIST'			00000005.
* WHEN N IS SYSTEM NUMBER OF INPUT TAPE AND			00000007.
* M2 AND M3 ARE LOGICAL TAPE NUMBERS			00000008.
* FOR PERIPHERAL INPUT, OUTPUT AND PUNCHING RESPECTIVELY.			00000010.
* WRITTEN BY G. W. GEORGE, NORTH AMERICAN AVIATION, INC.			00000011.
* SPACE AND INFORMATION SYSTEMS DIVISION, DOWNEY, CALIF.			00000013.
* ENTRY (CSH)			00000014.
* ENTRY (SPH)			00000015.
* ENTRY (SCH)			00000017.
TRANSFER VECTOR			
00000	74472623460	(TSH)	
00001	74472623460	(STH)	
00002	0560.00.0.00010	(CSH) CAL	00000018.
00003	0020.00.0.00000	(CSH) TRA	00000019.
00004	0020.00.0.00011	(SPH) CAL	00000020.
00005	0020.00.0.00011	(SCH) CAL	00000021.
00006	0550.00.0.00012	(SCH) CAL	00000022.
00007	0020.00.0.00001	TRA	00000023.
00008	0020.00.0.00000	M1	00000024.
00009	0020.00.0.00000	M2	00000025.
00010	0020.00.0.00000	M3	00000026.
00011	0.30016.0.00000	P1E	00000027.
00012	0.30016.0.00000	P2E	00000028.
00013	00005	P1N EQU	00000029.
00014	00005	P2N EQU	00000030.
00015	00016	NPUNCH EQU	00000031.
00016		END	00000032.

Figure 51. FAP Input-Output Compatibility Subroutine Listing

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POST PROCESSOR ASSEMBLY DATA  
13 IS THE FIRST LOCATION NOT USED BY THIS PROGRAM

REFERENCES TO USED SYMBOLS

10	M1	2
11	M2	4
12	M3	6
13	MIN	10
14	MOUT	11
15	MOUT	11
16	MOUT	11
17	MOUT	11
18	MOUT	11
19	MOUT	11
20	MOUT	11
21	MOUT	11
22	MOUT	11
23	MOUT	11
24	MOUT	11
25	MOUT	11
26	MOUT	11
27	MOUT	11
28	MOUT	11
29	MOUT	11
30	MOUT	11
31	MOUT	11
32	MOUT	11
33	MOUT	11
34	MOUT	11
35	MOUT	11
36	MOUT	11
37	MOUT	11
38	MOUT	11
39	MOUT	11
40	MOUT	11
41	MOUT	11
42	MOUT	11
43	MOUT	11
44	MOUT	11
45	MOUT	11
46	MOUT	11
47	MOUT	11
48	MOUT	11
49	MOUT	11
50	MOUT	11
51	MOUT	11
52	MOUT	11
53	MOUT	11
54	MOUT	11
55	MOUT	11
56	MOUT	11
57	MOUT	11
58	MOUT	11
59	MOUT	11
60	MOUT	11
61	MOUT	11
62	MOUT	11
63	MOUT	11
64	MOUT	11
65	MOUT	11
66	MOUT	11
67	MOUT	11
68	MOUT	11
69	MOUT	11
70	MOUT	11
71	MOUT	11
72	MOUT	11
73	MOUT	11
74	MOUT	11
75	MOUT	11
76	MOUT	11
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78	MOUT	11
79	MOUT	11
80	MOUT	11
81	MOUT	11
82	MOUT	11
83	MOUT	11
84	MOUT	11
85	MOUT	11
86	MOUT	11
87	MOUT	11
88	MOUT	11
89	MOUT	11
90	MOUT	11
91	MOUT	11
92	MOUT	11
93	MOUT	11
94	MOUT	11
95	MOUT	11
96	MOUT	11
97	MOUT	11
98	MOUT	11
99	MOUT	11
100	MOUT	11

NO ERROR IN ABOVE ASSEMBLY.

Figure S1. FAP Input-Output Compatibility Subroutine Listing  
(Continued)

Figure 52. Variable Format

[illegible]

Figure 52. Variable Format

## APPENDIX C

### COORDINATE TRANSFORMATION

#### PRIMARY TRANSFORMATION

As indicated in Section II, the surface coordinate transformation technique employed by the program does not require transformation parameters such as direction cosines, Euler angles and translation terms to be entered as input data to the program for transformation purposes. Instead, the  $x$ ,  $y$  and  $z$  coordinates of three points, not in a line, are given from the new origin, or to the new position of the surface. These data are then used to derive the rotational and translation terms required to transform the remaining surface data to the new origin or surface position.

The classical equations for transformation of rectangular coordinates in space are employed for both primary and auxiliary transformation. The new  $x$ ,  $y$  and  $z$  coordinates in terms of the old coordinates are:

$$x = x' \cos \alpha_1 + y' \cos \alpha_2 + z' \cos \alpha_3 + H \quad (1)$$

$$y = x' \cos \beta_1 + y' \cos \beta_2 + z' \cos \beta_3 + L \quad (2)$$

$$z = x' \cos \gamma_1 + y' \cos \gamma_2 + z' \cos \gamma_3 + K \quad (3)$$

Note that there are 9 unknown direction cosines and 3 translation terms, or a total of 12 unknowns. It is clear that the coordinates of four points from the new origin are required if these equations are to be used directly to determine the unknown parameters.

It can be shown, however, that the coordinates of three points (not in a line) are sufficient and necessary to fix the position of a surface in any rectangular coordinate system. It appears, therefore, that another point must be made available for solution of the above equations, or another technique developed which directly requires only three points. Investigation of the latter yielded a complex, difficult to program, solution. On the other hand, solution of the classical equations is straightforward, but requires the extra point (not in the plane of the other three). Rather than require the user to supply the extra point in data, it was decided to generate the point as a unit normal vector above the second point given in transformation data. This extra point must, of course, be generated in both old and new coordinate systems.

Figure 53 depicts a primary transformation of Surface A from the old (primed) to the new (unprimed) coordinate system. Note that the primary transformation shown affects only one surface, whereas both surfaces are involved in the auxiliary transformation, which will be discussed in more





detail later in this Appendix. The angles ( $\alpha$ ,  $\beta$  and  $\gamma$ ) shown in Equations 1, 2 and 3 are related in the following manner with the primed and unprimed coordinate axes shown in Figure 53:

$$\alpha_1 = \angle O'X'OX, \alpha_2 = \angle O'Y'OX, \alpha_3 = \angle O'Z'OX$$

$$\beta_1 = \angle O'X'OY, \beta_2 = \angle O'Y'OY, \beta_3 = \angle O'Z'OY$$

$$\gamma_1 = \angle O'X'OZ, \gamma_2 = \angle O'Y'OZ, \gamma_3 = \angle O'Z'OZ$$

Given the coordinates of points 2, 5 and 6 in Surface A, and the generated point U, from both the old and new coordinate systems, we may write four independent equations similar to Equation 1. Using Equation 2, the resulting set of equations in x is:

$$x_2 = x_2' \cos \alpha_1 + y_2' \cos \alpha_2 + z_2' \cos \alpha_3 + H \quad (4)$$

$$x_5 = x_5' \cos \alpha_1 + y_5' \cos \alpha_2 + z_5' \cos \alpha_3 + H \quad (5)$$

$$x_6 = x_6' \cos \alpha_1 + y_6' \cos \alpha_2 + z_6' \cos \alpha_3 + H \quad (6)$$

$$x_U = x_U' \cos \alpha_1 + y_U' \cos \alpha_2 + z_U' \cos \alpha_3 + H \quad (7)$$

We may similarly write two more sets of equations in y and z similar to Equations 2 and 3, for a total of twelve independent equations. Each set of four simultaneous equations is solved by Cramer's Rule (Reference 2) for the unknown direction cosines relating the old y' and z' axes to the new x, y and z axes.

For example, using the set developed above for Equation 1 (Equations 4, 5, 6 and 7), the coefficient determinant D is

$$D = \begin{vmatrix} x_2' & y_2' & z_2' & 1 \\ x_5' & y_5' & z_5' & 1 \\ x_6' & y_6' & z_6' & 1 \\ x_U' & y_U' & z_U' & 1 \end{vmatrix} \quad (8)$$

By Cramer's Rule, we successively replace the elements in each column of the set with the respective element on the left of each equation in the set. For example, the solution for  $\cos \alpha_2$  is:

$$\cos \alpha_2 = \frac{\begin{vmatrix} x_2' & x_2 & z_2' & 1 \\ x_5' & x_5 & z_5' & 1 \\ x_6' & x_6 & z_6' & 1 \\ x_U' & x_U & z_U' & 1 \end{vmatrix}}{D} \quad (9)$$

and similarly,

$$\cos \alpha_3 = \frac{\begin{vmatrix} x_2' & y_2' & x_2 & 1 \\ x_5' & y_5' & x_5 & 1 \\ x_6' & y_6' & x_6 & 1 \\ x_U' & y_U' & x_U & 1 \end{vmatrix}}{D} \quad (10)$$

The above process is repeated for the solution of  $\cos \beta_2$ ,  $\cos \beta_3$ ,  $\cos \gamma_2$ , and  $\cos \gamma_3$ , using the sets developed for  $y$  and  $z$ . The coefficient determinant is the same for all sets, because the coefficients of the unknowns in all sets are identical.

To increase computational efficiency, repeated factors in the expanded determinants are computed only once for each set. Also, considerable economy results in computing the unknown direction cosines  $\cos \alpha_1$ ,  $\cos \beta_1$ ,  $\cos \gamma_1$ , as the cross product of the corresponding direction cosines of the other ( $y$  and  $z$ ) axes:

$$\cos \alpha_1 = \cos \beta_2 \cos \gamma_3 - \cos \gamma_2 \cos \beta_3 \quad (11)$$

$$\cos \beta_1 = \cos \gamma_2 \cos \alpha_3 - \cos \alpha_2 \cos \gamma_3 \quad (12)$$

$$\cos \gamma_1 = \cos \alpha_2 \cos \beta_3 - \cos \beta_2 \cos \alpha_3 \quad (13)$$

The translation components  $H$ ,  $L$  and  $K$  are computed by substituting the coordinates of the point below point  $U$  in the surface to be transformed into Equations 1, 2 and 3, along with the known values of direction cosines. For the Surface A shown in Figure 53, using point 5,

$$H = x_5 - x_5' \cos \alpha_1 - y_5' \cos \alpha_2 - z_5' \cos \alpha_3 \quad (14)$$

$$L = y_5 - x_5' \cos \beta_1 - y_5' \cos \beta_2 - z_5' \cos \beta_3 \quad (15)$$

$$K = z_5 - x_5' \cos \gamma_1 - y_5' \cos \gamma_2 - z_5' \cos \gamma_3 \quad (16)$$

The program now transforms all point coordinates in Surface A from the old to the new system by direct substitution in Equations 1, 2 and 3.

The method outlined above will always perform the transformation desired, providing the three points selected are (1) sufficiently separated in space, (2) accurately computed, and (3) do not form a straight line in space. Because the fourth point U is always computed outside the plane of the other three, the coefficient determinant D can never be 0. Hence, by Cramer's Rule, a unique solution must always exist.

#### AUXILIARY TRANSFORMATION

An auxiliary transformation transforms the coordinates of both surfaces into the reference plane of a specified surface--the "Control" surface. In Figure 53, Surface A is the control surface; the auxiliary transformation depicted transforms both Surface A and B from the unprimed (old) system to the double-primed (new) system. In general, the origin O" in the control surface is always point 1 in the control surface coordinate array. It may not always be the first point entered in input surface data; if a bisection of the surface occurs, and the original point 1 is not seen by the other surface (assumed planar), then a new point 1 will be computed. The new point will be used as the origin O". The same processing occurs for internally generated surfaces. Only surfaces classed as plane surfaces may be control surfaces, i.e., Classes 1, 3, 4 and planar 6. For example, if both Surface A and B in Figure 53 are plane and bisect each other, two auxiliary transformations would occur to facilitate surface reconstruction. Actually, if Surface A were entered as Surface 1, the first auxiliary transformation to occur would be to point 1 in Surface B, rather than Surface A. This would not occur, however, if Surface A were not bisected by Surface B. In any case, the last transformation always is to point 1 in Surface 1, so that mapping and factor computation may proceed forthwith.

The processing of an auxiliary transformation differs from the primary transformation because unknowns may be more readily computed from available data. Equations 1, 2 and 3 are rewritten for the auxiliary old and new coordinate systems,

$$x'' = x \cos \alpha_1 + y \cos \alpha_2 + z \cos \alpha_3 + H'' \quad (17)$$

$$y'' = x \cos \beta_1 + y \cos \beta_2 + z \cos \beta_3 + L'' \quad (18)$$

$$z'' = x \cos \gamma_1 + y \cos \gamma_2 + z \cos \gamma_3 + K'' \quad (19)$$

The angles are defined as follows, referring to Figure 53:

$$\alpha_1 = \angle OXO''X'', \alpha_2 = \angle OYO''X'', \alpha_3 = \angle ZOZO''X''$$

$$\beta_1 = \angle OXO''Y'', \beta_2 = \angle OYO''Y'', \beta_3 = \angle ZOZO''Y''$$

$$\gamma_1 = \angle OXO''Z'', \gamma_2 = \angle OYO''Z'', \gamma_3 = \angle ZOZO''Z''$$

Because the  $O''X''$  axis in the new system is directed along the line segment formed by the first and second point in the control surface, the direction cosines related to that axis are readily computed.

The length of line  $\overline{12}$  in Surface A is

$$LS_{12} = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2},$$

and the direction cosines relating the new  $O''X''$  axis to the old  $OX$ ,  $OY$  and  $OZ$  axes are:

$$\cos \alpha_1 = (x_2 - x_1)/LS_{12} \quad (20)$$

$$\cos \alpha_2 = (y_2 - y_1)/LS_{12} \quad (21)$$

$$\cos \alpha_3 = (z_2 - z_1)/LS_{12} \quad (22)$$

Because the new  $O''Z''$  axis is directed along the surface unit orientation vector (point 0 above Surface A) the cosines relating that axis to the old  $OX$ ,  $OY$  and  $OZ$  axes are

$$\cos \gamma_1 = x_0 - x_1 \quad (23)$$

$$\cos \gamma_2 = y_0 - y_1 \quad (24)$$

$$\cos \gamma_3 = z_0 - z_1 \quad (25)$$

The remaining direction cosines are computed by cross products of the  $X''$  and  $Z''$  axis unit base vectors (direction cosines).

$$\cos \beta_1 = \cos \gamma_2 \cos \alpha_3 - \cos \alpha_2 \cos \gamma_3 \quad (26)$$

$$\cos \beta_2 = \cos \alpha_1 \cos \gamma_3 - \cos \gamma_1 \cos \alpha_3 \quad (27)$$

$$\cos \beta_3 = \cos \gamma_1 \cos \alpha_2 - \cos \alpha_1 \cos \gamma_2 \quad (28)$$

The unknown translation terms are determined from Equations 17, 18 and 19 for point 1 in Surface A ( $x_1^i = 0$ ,  $y_1^i = 0$ ,  $z_1^i = 0$ ).

$$H'' = -x_1 \cos \alpha_1 - y_1 \cos \alpha_2 - z_1 \cos \alpha_3 \quad (29)$$

$$L'' = -x_1 \cos \beta_1 - y_1 \cos \beta_2 - z_1 \cos \beta_3 \quad (30)$$

$$K'' = -x_1 \cos \gamma_1 - y_1 \cos \gamma_2 - z_1 \cos \gamma_3 \quad (31)$$

The program now transforms all coordinates in Surface A and Surface B to the new system by using Equations 17, 18 and 19.

# APPENDIX D

## COMPUTATION OF SURFACE AREA OF INTERNALLY GENERATED SURFACES

In Figure 54, View J-J shows a view of the surface of a right elliptical cone between the two arbitrary cross-sections indicated in the isometric sketch of the cone. Because the program internal surface generator uses the elliptical cross-section as the basic generating element, elemental surface areas such as  $ABCD$  in Figure 54 are trapezoids having, in general, unequal nonparallel sides. Also, because each elemental surface is developed by equal elliptical ~~parametric~~ angles, one need compute the area of only one elemental surface for each pair of cross-sections (providing, of course, the cross-sections are similar).

The plane area of trapezoid  $ABCD$  is

$$A_T = \frac{1}{2} h (L_1 + L_2). \quad (1)$$

$L_1$  and  $L_2$  are readily computed from the  $X, Y$  coordinates of points  $A, B, C$  and  $D$ :

$$L_1 = \sqrt{(X_C - X_A)^2 + (Y_C - Y_A)^2} \quad (2)$$

$$L_2 = \sqrt{(X_D - X_B)^2 + (Y_D - Y_B)^2} \quad (3)$$

The trapezoid height  $h$  is computed indirectly from the projected area  $A_p$  of the trapezoid on the  $XY$  plane in the following manner:

$$h = \sqrt{h_p^2 + Z^2} \quad (4)$$

where  $h_p$  is the projected length of trapezoid height  $h$ , and  $Z$  is the distance between cross-sections.

The projected area of  $ABCD$  is:

$$A_p = \frac{1}{2} h_p (L_1 + L_2). \quad (5)$$

Solving for  $h_p$  in Equation 5:

$$h_p = \frac{2 A_p}{(L_1 + L_2)} \quad (6)$$

The area  $A_p$  is computed from the trapezoid  $(X, Y)$  coordinates in the following manner:

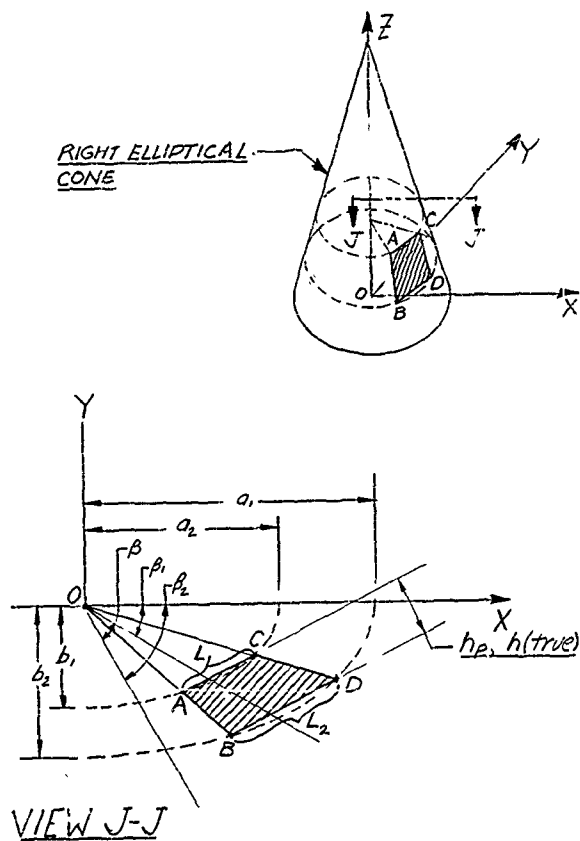


Figure 54. Surface Area Geometry of Internally Generated Polhedra

Noting triangles BOD and AOC

$$A_p = \text{Area } \triangle BOD - \text{Area } \triangle AOC \quad (7)$$

It is desirable for computational efficiency to compute  $A_p$  using known parameters. In this case,  $\sin \beta$  is known and is used. The parametric equations of the ellipse are:

$$x = a \cos \theta \quad (8)$$

$$y = b \sin \theta \quad (9)$$

where  $a$  is the semi-major axis,  $b$  is the semi-minor axis and  $\theta$  is the parametric angle. In Figure 54, angle  $\beta_1$  defines points A and B and angle  $\beta_2$  defines points C and D. Angle  $\beta = \beta_2 - \beta_1$ .

The area of triangle AOC can be computed by vector cross products,

$$A_{AOC} = \frac{1}{2} (X_A Y_C - X_C Y_A) \quad (10)$$

From Equations 8 and 9 for the parametric angles  $\beta_1$  and  $\beta_2$  defining points A and C,

$$X_A = a_1 \cos \beta_1, Y_A = b_1 \sin \beta_1 \quad (11)$$

$$X_C = a_1 \cos \beta_2, Y_C = b_1 \sin \beta_2 \quad (12)$$

Substituting Equations 11 and 12 in Equation 10,

$$A_{AOC} = \frac{1}{2} a_1 b_1 (\cos \beta_1 \sin \beta_2 - \cos \beta_2 \sin \beta_1)$$

$$A_{AOC} = \frac{1}{2} a_1 b_1 \sin (\beta_2 - \beta_1)$$

$$A_{AOC} = \frac{1}{2} a_1 b_1 \sin \beta \quad (13)$$

A similar derivation is developed to obtain the area of triangle BOD.

$$A_{BOD} = \frac{1}{2} a_2 b_2 \sin \beta \quad (14)$$

Substituting Equations 13 and 14 in Equation 7,

$$A_p = \frac{1}{2} \sin \beta (a_2 b_2 - a_1 b_1) \quad (15)$$

Substituting Equation 15 into Equation 6,

$$h_p = \frac{2 \left[ \frac{1}{2} \sin \beta (a_2 b_2 - a_1 b_1) \right]}{I_1 + I_2} \quad (16)$$

Substituting Equation 16 into Equation 4,

$$h = \sqrt{\left[ \frac{\sin \beta (a_2 b_2 - a_1 b_1)}{L_1 + L_2} \right]^2 + z^2} \quad (17)$$

Finally, substituting Equation 17 into Equation 1,

$$A_T = \frac{L_1 + L_2}{2} \sqrt{\left[ \frac{\sin \beta (a_2 b_2 - a_1 b_1)}{L_1 + L_2} \right]^2 + z^2}$$

Rearranging terms,

$$A_T = \frac{1}{2} \sqrt{[\sin \beta (a_2 b_2 - a_1 b_1)]^2 + [z (L_1 + L_2)]^2} \quad (18)$$

The total surface area is computed by repeated evaluation of Equation 18 for the particular surface generated.



# APPENDIX E

## DERIVATION OF CONFIGURATION FACTOR TO A SPHERE

The analytic solution of the configuration factor to a sphere depends upon the position of the sphere relative to the plane of Surface 1. This is clearly demonstrated geometrically by using the Nusselt unit sphere projection as shown in Figure 55. Three unique solutions are apparent from the five different sphere positions; Ib and IIIa represent "limit" values in each case. The unit sphere projections (crosshatched areas) shown in the lower part of Figure 55 correspond respectively to sphere positions (not to scale) depicted in the upper half. Case I results when the sphere is above (Ia) and/or touching (Ib) the plane of Surface 1. The locus on the Nusselt hemisphere base is an ellipse, and varies from a circle (when the sphere is vertically over the point O) to the single tangency position shown in Ib. When the sphere goes below the plane of Surface 1, the Case II locus appears, and is formed by the ellipse boundary on the left and the unit circle boundary on the right.

The locus projected on the unit sphere surface is a circle, in every case. The radius,  $b$ , of the circle becomes the semi-major axis of the projected ellipse. By similar triangles,

$$\frac{b}{1} = \frac{R}{D}$$

$$b = \frac{R}{D} \quad (1)$$

where  $D$  = distance from center of sphere to origin of unit sphere and  $R$  is the sphere radius. The semi-minor axis,  $a$ , of the ellipse is the projection on the unit circle of  $b$ ; again by similar triangles,

$$\frac{a}{b} = \frac{R}{D}$$

$$a = b \frac{R}{D} = \frac{R^2}{D^2}$$

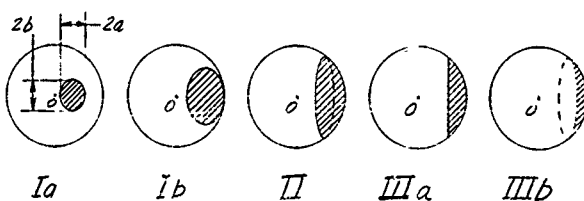
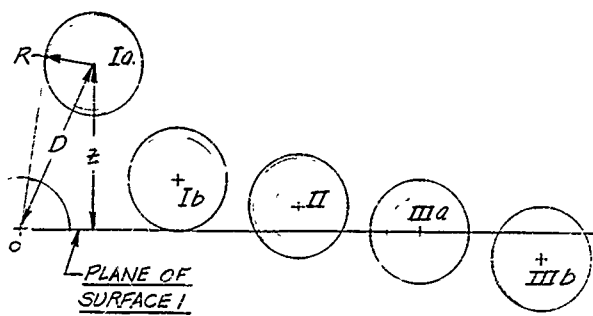
or

$$a = b \frac{R}{D} = \frac{R^2}{D^2} \quad (2)$$

The area of the ellipse is

$$A = \pi ab = \pi \frac{R^2}{D^2} \quad (3)$$

The configuration factor for Case I is the area of the ellipse divided by the area of the unit radius circle,



NUSSELT UNIT SPHERE PROJECTIONS  
(NOT TO ANY SCALE)

Figure 55. Areas Involved in Configuration Factor to Spheres

$$c_I = \frac{R^2 Z}{D^3}, \quad Z \geq R \quad (L)$$

NUSSELT UNIT  
CIRCLE

By inspection,

$$A_{ACB} = A_{AOB} - A_{CO'OB} - A_{CO'B} \quad (5)$$

Area AOB is a sector of the unit circle,  $R = 1$ ,

$$A_{AOB} = \frac{1}{2} R^2 \theta = \frac{1}{2} \theta \quad (6)$$

Given  $h$ , the distance between centers  $O$  and  $O'$ , and  $Y_C$ , the value of  $y$  at the tangency point between the ellipse and the circle, the area of the triangle  $OO'C$  is

$$A_{0103} = \frac{1}{2} = \bar{x}_c \quad (7)$$

The area CO'B is an elliptical sector defined by the parametric angle  $\phi$  at  $(x_c, y_c)$  the point of tangency,

$$A_{CO'B} = \frac{ab}{2} \phi \quad (8)$$

Inserting Equations 6, 7 and 8 into Equation 5,

$$A_{ACB} = \frac{1}{2} (\phi - by_c - ab\phi) \quad (9)$$

The unknowns  $b$ ,  $h$ ,  $y_c$  and  $\phi$  must be evaluated in terms of  $N$ ,  $Z$  and  $D$ . The tangency point  $x_c, y_c$  is determined as follows. The equation of the ellipse when translated a distance  $h$  in the  $x$  direction from the origin  $O$  is

$$\frac{(x-h)^2}{a^2} + \frac{y^2}{b^2} = 1 \quad (10)$$

The equation of the unit circle is

$$x^2 + y^2 = 1 \quad (11)$$

At the intersection point the slopes are equal. Taking the first derivative of Equation 10,

$$\frac{2}{a^2} (x-h) dx + \frac{2y}{b^2} dy = 0$$

Rearranging,

$$\frac{dy}{dx} = \frac{b^2}{2y} \left[ \frac{2}{a^2} (h-x) \right] = -\frac{b^2}{a^2} \frac{(h-x)}{y} \quad (12)$$

The slope at any point  $x, y$  on the circle is:

$$\frac{dy}{dx} = -\frac{x}{y} \quad (13)$$

Equating Equations 12 and 13,

$$\frac{b^2}{a^2} \frac{(h-x)}{y} = -\frac{x}{y}$$

Solving for  $h$ , at  $x = x_c$  and  $y = y_c$ ,

$$h = x_c \frac{(y_c^2 - a^2)}{b^2} \quad (14)$$

Substituting Equation 14 into Equation 10,

$$\frac{\left[ x_c - x_c \frac{(b^2 - a^2)}{b^2} \right]^2}{a^2} + \frac{y_c^2}{b^2} = 1$$

Reducing and rearranging terms, and solving simultaneously with Equation 11:

$$\left(\frac{a}{b}\right)^2 x_c^2 + y_c^2 = b^2 \quad (15)$$

$$x_c^2 + y_c^2 = 1$$

Subtracting Equation 11 from Equation 15,

$$x_c^2 \left[ \left(\frac{a}{b}\right)^2 - 1 \right] = b^2 - 1$$

Solving for  $x_c$ ,

$$x_c^2 = \frac{b^2 - 1}{\left(\frac{a}{b}\right)^2 - 1} \quad (16)$$

$$x_c = b \sqrt{\frac{1 - b^2}{b^2 - a^2}} \quad (17)$$

Solving for  $y_c$  in Equation 11,

$$y_c = \sqrt{1 - x_c^2} \quad (18)$$

Substituting Equation 1 and 2 into Equation 17,

$$x_c = \sqrt{\frac{R^2 - D^2}{Z^2 - D^2}} \quad (19)$$

Substituting Equation 1, 2 and 16 into Equation 18,

$$y_c = \sqrt{\frac{Z^2 - R^2}{Z^2 - D^2}} \quad (20)$$

The angle  $\phi$  may be defined as

$$\phi = \tan^{-1} \frac{y_c}{x_c} = \tan^{-1} \frac{y_c}{\sqrt{b^2 - y_c^2}} \quad (21)$$

Substituting Equation 1 and 20 into Equation 21,

$$\phi = \tan^{-1} \left[ \frac{D}{|Z|} \cdot \sqrt{\frac{Z^2 - R^2}{R^2 - D^2}} \right] \quad (22)$$

The angle  $\theta$  may be defined as

$$\theta = \tan^{-1} \frac{y_c}{x_c} \quad (23)$$

Substituting Equations 19 and 20 into Equation 23,

$$\theta = \tan^{-1} \sqrt{\frac{Z^2 - R^2}{R^2 - D^2}} \quad (24)$$

Substituting Equations 1, 2 and 19 into Equation 14,

$$h = \frac{D^2 - Z^2}{D^2} \sqrt{\frac{R^2 - D^2}{Z^2 - D^2}} \quad (25)$$

The parameter  $hy_c$  in Equation 9 is evaluated by multiplying Equations 20 and 25,

$$\begin{aligned} hy_c &= \left[ \frac{D^2 - Z^2}{D^2} \sqrt{\frac{R^2 - D^2}{Z^2 - D^2}} \right] \frac{Z^2 - R^2}{Z^2 - D^2} \\ hy_c &= \frac{\sqrt{D^2 - R^2} \cdot \sqrt{R^2 - Z^2}}{D^2} \\ hy_c &= \left( \frac{D^2 - R^2}{D^2} \right) \sqrt{\frac{R^2 - Z^2}{D^2 - R^2}} \end{aligned} \quad (26)$$

Let  $\alpha = D^2 - R^2$  (27)

and  $\beta = \sqrt{\frac{R^2 - Z^2}{\alpha}}$  (28)

Substituting Equations 27 and 28 into Equations 22, 24 and 26, respectively,

$$\phi = \tan^{-1} \left[ \frac{D}{2D} \beta \right] \quad (29)$$

$$\theta = \tan^{-1} \beta \quad (30)$$

and  $hy_c = \frac{\alpha \beta}{D^2}$  (31)

Finally, substitute Equations 29, 30 and 31 into 9; the actual area projected on the hemisphere base is twice Area ACB and is divided by the base area to yield the configuration factor.

$$C_{III} = \frac{1}{\pi} \left[ \left( \tan^{-1} \beta \right) - \frac{R^2 Z}{D^3} \left( \tan^{-1} \frac{\beta D}{|Z|} \right) - \frac{\beta}{Z} \right] \quad (2)$$

where

$$\alpha = D^2 - R^2$$

$$\beta = \sqrt{\frac{R^2 - Z^2}{\alpha}}, \quad Z \leq 0 \text{ and } Z^2 \leq R^2$$

By inspection of Figure 55, the projected area for Case II is the sum of the ellipse evaluated by the Case I formula and the crescent shaped area determined by the Case III formula,

$$C_{II} = C_I + C_{III}, \quad 0 < Z < R \quad (3)$$

In summary, referring to Figure 55,

$$C_I = \frac{R^2 Z}{D^3}, \quad Z \geq R$$

$$C_{III} = \frac{1}{\pi} \left[ \left( \tan^{-1} \beta \right) - \frac{R^2 Z}{D^3} \left( \tan^{-1} \frac{\beta D}{|Z|} \right) - \frac{\beta}{Z} \right]$$

where

$$\alpha = D^2 - R^2, \quad \beta = \sqrt{\frac{R^2 - Z^2}{\alpha}},$$

$$Z \leq 0, \quad Z^2 \leq R^2$$

$$C_{II} = C_I + C_{III}, \quad 0 < Z < R$$